

Wastewater Feasibility Study

ROMBAUER VINEYARDS # P19-00130-MOD Planning Commission Hearing Date 5 August 2020



ONSITE WASTEWATER DISPERSAL FEASIBILITY STUDY FOR ROMBAUER VINEYARDS WINERY 3522 SILVERADO TRAIL, NAPA COUNTY APN 021-410-025

As required by Napa County Planning, Building and Environmental Services (PBES) and at the request of Lynn S. Sletto, Esq., Bartelt Engineering has evaluated the feasibility of installing a new onsite sanitary wastewater treatment and dispersal system to serve the existing administration building, full crush winery, and tasting room located at 3522 Silverado Trail, St. Helena, CA 94574 to accommodate an increase in employee staffing levels and proposed changes to the hospitality marketing plan.

PROJECT DESCRIPTION

It is our understanding that Rombauer Vineyards Winery is proposing to increase the number of full time employees from 25 to 55 and to increase the number of part-time and seasonal employees from 9 to 26; while maintaining the existing wine production capacity at 450,000 gallons and the number of daily visitors at 400 as stated in the existing approved Use Permit (# P10-00039).

It is also our understanding that Rombauer Vineyards Winery would like to make the following changes to the approved marketing plan:

- Remove four (4) Wine Club Events per year with a maximum of 250 guests at each event
- Add five (5) Marketing Events per year with a maximum of 350 guests at each event
- Increase the number of Lunch/Dinner Event guests from forty (40) to sixty (60) guests per event.

All food served out of the tasting room "plating area" for special marketing events will be catered by an offsite company that will provide clean plates, utensils, etc. for dining and remove all dirty dishes, utensils, etc. for offsite cleaning. The small plates used for the daily food and wine pairings and wine glasses will be washed after each event using the tasting room glass dishwasher.



Table 1 summarizes the approved and proposed employee staffing plan:

TABLE 1: EMPLOYEE STAFFING PLAN SUMMARY					
Description	Арг	proved	Proposed		
	Frequency	Number of Employees	Frequency	Number of Employees	
Full-time Employees	Year-round	25	Year-round	55	
Part-time Employees	Year-round	0	Year-round	6	
Seasonal Employees	Daily during Harvest	9	Daily during Harvest	20	

Table 2 summarizes the approved and proposed marketing plan:

TABLE 2: MARKETING PLAN SUMMARY					
Description	Арр	proved	Proposed		
	Frequency	Number of Guests	Frequency	Number of Guests	
Private Tours & Tastings	daily	400 per day	daily	400 per day	
Food (cheese) & Wine Pairings ¹	10 per day	8 per pairing	10 per day	8 per pairing	
Marketing Events ²	1 per year	300 max	5 per year	350 max	
Wine Club Events	4 per year	250 max	Removed	Removed	
Wine Auction Event ^{1,3}	1 per year	40 max	1 per year	40 max	
Barrel Tasting Event ^{1,3}	1 per year	40 max	1 per year	40 max	
Lunch or Dinner Events ^{1,3}	4 per month	40 max per event	4 per month	60 max per event	

¹ Number of Guests per event are included in the maximum daily visitor count of 400.

² Event cannot be held the same day of tours & tasting, barrel tastings, lunch/dinner events, or auction related events; portable toilets are required for all events.

³ Events cannot be held on the same day with any other event, but can be held in conjunction with tours & tastings such that the combination is not to exceed a maximum daily visitor count of 400.

March 2019 Job No. 96-07



As part of our services, representatives from Bartelt Engineering have reviewed the operational methods for the winery with our Client, reviewed the parcel files at Napa County PBES, held conversations with Napa County PBES staff, performed a reconnaissance of the site to view existing conditions and conducted a site evaluation on November 8, 2018 to evaluate the feasibility of installing a new onsite sanitary wastewater dispersal system to serve the existing winery, offices, and tasting room.

This study prepared by Bartelt Engineering is provided to demonstrate that the proposed sanitary wastewater system improvements can feasibly be developed and that all sanitary wastewater can be adequately treated and dispersed onsite.

WASTEWATER FLOW CALCULATIONS

Existing Pressure Distribution Field Dispersal Capacity

Site evaluations were conducted on June 22, 1993 and May 29, 1996 by Napa Septic Tank Service and on November 4, 1998 by Bartelt Engineering. The site evaluation results showed useable soil up to 72 inches. The site evaluation conducted by Bartelt Engineering on November 4, 1998 was to verify subsurface soil conditions examined during an earlier site evaluation performed on May 29, 1996. Based on the finding of an acceptable percolation rate of 3 inches per hour at 48 inches below ground surface, a pressure distribution type wastewater disposal system was installed by Harold Smith & Sons in the summer of 1999.

- Site slope: 2% to 4%
- Soil Type: Sandy Clay Loam / Gravely Clay Loam / Gravely Loam
- Assigned Perc Rate: 3 inches/hr to 6 inches/hr, use 3 inches/hr Perc Rate = 3 inches/hour = 20 min/in
- From Table 3, Soil Hydraulic Loading Rates Based on Percolation Rates⁴: Converted perc rate = 0.657 gal/sf/day
- Total Existing Peak Estimated Wastewater Flow = 11,980 gpd* *(From September 1999 feasibility study prepared by Bartelt Engineering)
- Total lineal feet of pressure distribution lateral installed = 6,228 lf*
 *(From Rombauer Vineyards Septic System Design Record Drawing, dated October 1999 prepared by Bartelt Engineering)

An 18 inch deep trench was used for the pressure distributed leach lines which corresponds to 3 square feet of sidewall area per lineal foot of trench. Distribution lines were placed at grade to 3 inches below grade with 12 inches of imported fill and trench spoils placed over the trenches.

Minimum required length of trench⁴ =
$$\frac{11,980 \text{ gal/day}}{0.657 \text{ gal/sf/day}} \times \frac{1 \text{ lf}}{3 \text{ sf sidewall}} = 6,078 \text{ lf}$$

⁴ Referenced from Napa County Regulations for Design, Construction, and Installation of Alternative Sewage Treatment Systems, 2014.

Onsite Wastewater Dispersal Feasibility Study Rombauer Vineyards Winery



The dispersal capacity of the pressure distribution field can be calculated based on a total of 6,228 lf of leach line installed.

Pressure Distribution Dispersal Capacity =

(6,228 *lf of lateral*)
$$x \left(\frac{3 \text{ sf sidewall}}{1 \text{ lf of lateral}}\right) x (0.657 \text{ gal/sf/day}) = 12,275 \text{ gal/day}$$

The Use Permit Modification is not proposing any changes to wine production nor is it proposing improvements to the existing process wastewater system.

Daily Winery Sanitary Wastewater Flow

The sanitary wastewater generated in gallons per day (gpd) at the facility includes both full and part-time employees, daily tours, tastings and daily food and wine pairings and can be itemized as follows:

Employees:

 (55 full-time employees) x (15.0 gpd per employee) = 	825 gpd
 (6 part-time employees) x (15.0 gpd per employee) = 	90 gpd
• (20 seasonal (harvest) employees) x (15.0 gpd per employee) =	= 300 gpd
Private Tours and Tastings:	
• (400 guests/day) x (2.2 gal/guest for restroom) x (50% usage) =	= 440 gpd
• (400 wine glasses per day) x (2.4 gallons $\frac{5}{45}$ wine glasses) =	22± gpd
Food (cheese) and Wine Pairings:	
• (80 small plates per day) x (2.4 gallons ⁶ /25 small plates) =	8± gpd

Special Marketing Event Sanitary Wastewater Flow

The sanitary wastewater generated for each special marketing event can be itemized as follows:

Note: This feasibility study assumes that portable toilets, offsite meal preparation and catering services are utilized during the Marketing Events regardless of the season and that 30% of the event guests and all of the catering staff are assumed to use the winery restrooms during these events. The remainder of the event guests (70%) will utilize the portable toilets.

Marketing Events

- (350 guests) x (2.2 gal/guest for restroom usage) x (30% guest usage) = 231 gpd
- (20 outside catering staff) x (2.2 gal/staff for restroom usage) = 44 gpd
- Wine glasses are given to guests to take home

⁵ Glass Dishwasher water use is 2.4 gallons per cycle for 45 wine glasses per cycle; Hobart Dishmachine SR24.

⁶ Glass Dishwasher (small plates) water use is 2.4 gallon per cycle for 25 dishes per cycle; Hobart Dishmachine SR24.

Wine Auction Event (2-4 hours):

 (40 guests) x (2.2 gal/guest for restroom usage) = (5 outside catering staff) x (2.2 gal/staff for restroom usage) = (40 guests) x (4 wine glasses per guest) x (2.4 gallons⁵/45 glasses) = 	88 gpd 11 gpd 9± gpd
 Barrel Tasting Event (2-4 hours): (40 guests) x (2.2 gal/guest for restroom usage) = (5 outside catering staff) x (2.2 gal/staff for restroom usage) = (40 guests) x (1 wine glass per guest) x (2.4 gallons⁷/45 glasses) = 	88 gpd 11 gpd 3± gpd
 Lunch or Dinner Events (2-4 hours): (60 guests) x (2.2 gal/guest for restroom usage) = (5 outside catering staff) x (2.2 gal/staff for restroom usage) = (60 guests) x (4 glasses per guest) x (2.4 gallons⁷/45 glasses) = 	132 gpd 11 gpd 13± gpd

Total Harvest Season and Non-Harvest Season Peak Sanitary Wastewater Flow

The total proposed harvest season peak sanitary wastewater flow is the combination of the facilities employee and marketing events sanitary wastewater flows during the months of harvest. The total proposed non-harvest season peak sanitary wastewater flow is the combination of the facilities employee and marketing events sanitary wastewater flows during the months of non-harvest.

Table 3A uses the marketing schedule to calculate the sanitary wastewater flows generated by employees and guests during daily event sequences in harvest and non-harvest seasons. Wastewater flows in the same column indicate the events may occur on the same day.



⁷ Glass Dishwasher water use is 2.4 gallons per cycle for 45 wine glasses per cycle; Hobart Dishmachine SR24.



TABLE 3A: HARVEST	AND N	on -H a	rvest Se	ASON DA	ALY SANI	TARY WA	ASTEWA	ter Flov	VS	
]	Daily Oc	currenc	ce			
			Harves	st			N	on-Harv	vest	
Full-time Employees	825	825	825	825	825	825	825	825	825	825
Part-time Employees	90	90	90	90	90	90	90	90	90	90
Seasonal Employees	300	300	300	300	300					
Private Tours & Tastings ⁸	462		415	415	392	462		415	415	392
Food & Wine Pairings ⁹	8		8	8	8	8		8	8	8
Marketing Events ¹⁰		275					275			
Wine Auction Event ^{8, 11}			108					108		
Barrel Tasting Event ^{8, 11}				102					102	
Lunch / Dinner Events ^{8, 11}					156					156
Total Flow (gpd)	1,685	1,490	1,746	1,740	1,771	1,385	1,190	1,446	1,440	1,471

Table 3A shows that the greatest sanitary wastewater flow during the harvest and nonharvest seasons is generated during a typical staffing day with Tours/Tastings, Food & Wine Pairings, and Lunch or Dinner Events hosted at the winery.

Peak Sanitary Wastewater Flow

The peak sanitary wastewater flows during harvest and non-harvest periods is summarized in the following table:

TABLE 3B: HARVEST AND NON-HARVEST SEASON PEAK WASTEWATER SUMMARY				
Wastewater Source	Harvest Nor		Non-Harvest	
	(g	pd)	(gpd)	
Sanitary Wastewater	Employees	1,215	915	
	Hospitality	556	556	
Dispersal Field Capacity	1,771		1,471	

⁸ Number of Guests for Private Tours and Tastings is reduced when wine auction events, barrel tasting events and lunch/dinner events are held.

⁹ Number of Guests per event are included in the maximum daily visitor count of 400.

¹⁰ Event cannot be held the same day of tours & tasting, barrel tastings, lunch/dinner events, or wine auction related events; portable toilets are required for all events.

¹¹ Events cannot be held on the same day with any other event, but can be held in conjunction with tours & tastings such that the combination is not to exceed a maximum daily visitor count of 400.



WASTEWATER TREATMENT AND DISPERSAL METHODS

The proposed sanitary wastewater system is discussed further in the following sections. Refer to the associated Dispersal Field Exhibit prepared by Bartelt Engineering for location of the proposed primary and replacement dispersal areas.

Proposed Sanitary Wastewater Subsurface Drip Dispersal Field with Pretreatment

As summarized in Table 3B, the calculated dispersal field capacity is 1,771 gpd. This study proposes that the sanitary wastewater dispersal field be designed to have a peak daily flow of 2,500 gpd. The winery production facility, offices and tasting room sanitary wastewater would continue to gravity flow to a series of existing septic tanks. From the septic tanks, sanitary wastewater effluent will flow by gravity to a new recirculation/dose tank. From the recirculation/dose tank, stored effluent is pumped to a new Orenco AdvanTex AX Pretreatment System (or approved equal). Pretreated effluent is proposed to be dispersed through a subsurface drip field by means of a timed-dose pumping system.

Based on the site evaluation performed by Bartelt Engineering on November 8, 2018, suitable area is available onsite for a subsurface drip dispersal field. The primary dispersal area is proposed to be located near test pits #1 and #10 which has an observed depth of 48 inches with Clay Loam and Sandy Clay Loam soils. Napa County Standards require a minimum of 24 inches of acceptable soil below the bottom of the drip lines with a minimum of six (6) inches of acceptable soil cover material placed over the drip lines. For Clay Loam type soil, GeoFlow Incorporated recommends a soil hydraulic loading rate¹² of 0.60 gal/sf/day for pretreated effluent.

The minimum required primary area for the subsurface drip field is calculated below:

Subsurface Drip Field Area = $\frac{\text{Design Flow Rate}}{\text{Hydraulic Loading Rate}} = \frac{2,500 \text{ gallons per day}}{0.60 \text{ gallons/ft}^2/\text{day}} = 4,167 \text{ ft}^2$

Based on site slopes of 13% or less in the primary area, a two (2) foot spacing is recommended between driplines per Napa County Standards. The recommended drip field contains 42 driplines each $60\pm$ feet long. The total recommended primary area is 5,800± square feet.

Sanitary Wastewater 200% Replacement Area

The replacement area is proposed to be located near test pits #2 through #9 which had an observed depth of 36 to 70 inches with Clay Loam and Sandy Clay Loam soils. The same application rate (0.6 gal/sf/day) used for the primary area is used to size the 200% replacement area, as shown below:

Replacement area =
$$200\% \times \frac{2,500 \text{ gallons per day}}{0.60 \text{ gallons/ft}^2/\text{day}} = 8,333 \text{ ft}^2$$

¹² Referenced from *Table 1 Drip Loading Rates Considering Soils Structure* of The Subsurface Drip Dispersal and Reuse Design, Installation and Maintenance Guidelines prepared by GeoFlow Incorporated.



Based on site slopes of 13% or less in the replacement area, a two (2) foot spacing is recommended between driplines per Napa County Standards. The recommended replacement area is 11,700± square feet.

WASTEWATER TREATMENT TANK SIZING

<u>Septic Tank(s)</u>

The existing sanitary wastewater septic tank(s) are proposed to be utilized with the proposed improvements unless their existing condition is reported to be inadequate for continued use by a licensed contractor. Any new septic tank(s) will be sized to provide a minimum of three (3) days of hydraulic retention time during peak wastewater flows. Furthermore, the septic tank(s) will also be equipped with an effluent filter to aid in the reduction of Total Suspended Solids (TSS) and Biochemical Oxygen Demand (BOD) in the wastewater effluent stream.

Existing Septic and Sump Tanks

The existing septic and sump tanks are shown as follows:

Septic Tank Wastewater Source	Peak Flow (gpd)	Retention Time (days)	Existing Tankage Capacity (gallons)
Winery Sanitary	885	5.1	4,500
Administration Sanitary	330	4.5	1,500
Event Sanitary	556	8.1	4,500

Recirculation Tank

The proposed recirculation tank is sized to provide a minimum of one (1) day of hydraulic retention time during peak wastewater flows. Below is a summary of the recommended tank volume:

Tank Volume	= 1 day x 2,500 gallons
	= 2,500 gallons, 3,000 gallons recommended

Subsurface Drip Dosing Tank

The proposed dosing tank is sized to provide a minimum of a half (0.5) days of hydraulic retention time during peak wastewater flows. Below is a summary of the recommended tank volume:

Tank Volume	= 0.5 days x 2,500 gpd
	= 1,250 gallons, 1,500 gallons recommended

OPERATION AND MAINTENANCE

Per Napa County requirements, the sanitary wastewater system is classified as an Alternative Sewage Treatment Systems (ASTS) and therefore must have a Service Provider. The Service Provider would be assigned prior to operation and final approval of the installed wastewater system.

March 2019 Job No. 96-07



SUMMARY & CONCLUSIONS

Sanitary wastewater generated from the existing winery and hospitality building is anticipated to increase as a result of the proposed changes to the staff and marketing plan.

The project proposes to install a new subsurface drip dispersal field and pretreatment system to accommodate the increase in sanitary wastewater flows. This study demonstrates that all sanitary wastewater generated from the proposed increase in the number of employees and guests can feasibly be treated and dispersed onsite. Modifications to the approved wine production capacity and process wastewater system are not proposed as part of this Use Permit Modification.

Full design calculations and improvement plans will be completed after approval of the Use Permit Modification under consideration.

ATTACHMENTS

Dispersal Field Exhibit

Site Evaluation Report

REFERENCES

California Onsite Wastewater Association (COWA). "Pumping and Pressure Distribution Systems." May 1998.

Geoflow, Inc. Wastewater Design, Installation and Maintenance Guidelines. v1, 2007.

Napa County Department of Environmental Management. "Regulatons for Design, Construction, and Installation of Alternative Sewage Treatment Systems." October 22, 2014.

Telsco Industries. "Turf Irrigation Manual." By James A. Watkins. 1987.

- U.S. Department of Health, Education and Welfare, Public Health Service Publication. Manual of Septic-Tank Practice. 1967.
- U.S. Environmental Protection Agency. "Onsite Wastewater Treatment Systems Manual." February 2002.
- Napa County Planning, Building and Environmental Services, "Napa County Onsite Wastewater Treatment Systems (OWTS) Technical Standards." Final Draft.
- Orenco Systems, Incorprated. "AdvanTex Design Criteria for Commercial Treatment Systems". Rev.1.6. January 2016.

Napa County Department of Environmental Management

SITE EVALUATION REPORT

Please attach an 8.5" x 11" plot map showing the locations of all test pits triangulated from permanent landmarks or known property corners. The map must be drawn to scale and include a North arrow, surrounding geographic and topographic features, direction and % slope, distance to drainages, water bodies, potential areas for flooding, unstable landforms, existing or proposed roads, structures, utilities, domestic water supplies, wells, ponds, existing wastewater treatment systems and facilities.

Permit #: E18-00860

APN: 021-410-025

AFN. 021-410-023

Date:

(County Use Only) Reviewed by:

PLEASE PRINT OR TYPE ALL INFORMATION

Property Owner Koerner Rombauer Revocable Trust and Joan K. Rombauer Marital Trust B	□ New Construction □ Addition □ Remodel □ Relocation ⊠ Other:
Property Owner Mailing Address	Posidential # of Podroome: Design Flow: and
3522 Silverado Trail	D Residential - # of bedrooms. Design Flow . gpd
City State Zip	XI Commercial - Type: Winery
St. Helena, CA 94574	
Site Address/Location	Sanitary Waste: 2,500 gpd Process Waste: gpd
3522 Silverado Trail, St. Helena, CA	□ Other:
	Sanitary Waste: gpd Process Waste: gpd

Evaluation Conducted By:			
Company Name	Evaluator's Name		Signature (Civil Engineer, R.E.H.S., Geologist, Soil Scientist)
			DIIA
Bartelt Engineering	Richard Paxton, P.E.		Kichan Jufton
Mailing Address:			Telephone Number
1303 Jefferson Street, 200 B			(707) 258-1301
City	State	Zip	Date Evaluation Conducted
Napa	CA	94559	November 8, 2018

Primary Area See below	Expansion Area See below		
Acceptable Soil Depth: 54 & 48 in. Test pits #: 1 & 10	Acceptable Soil Depth: 36 to 70 in. Test pits #: 2, 3, 4, 5, 6, 7, 8 & 9		
Soil Application Rate (gal. /sq. ft. /day): 0.6	Soil Application Rate (gal. /sq. ft. /day): 0.6		
System Type(s) Recommended: Subsurface Drip	System Type(s) Recommended: Subsurface Drip		
Slope: 12% to 13%. Distance to nearest water source: 100+ feet	Slope: 7% to 14%. Distance to nearest water source: 100+ feet		
Hydrometer test performed? No \Box Yes \boxtimes (attach results)	Hydrometer test performed? No □ Yes ⊠ (attach results)		
Bulk Density test performed? No \boxtimes Yes \Box (attach results)	Bulk Density test performed? No ⊠ Yes □ (attach results)		
Groundwater Monitoring Performed? No ⊠ Yes □ (attach results)	Groundwater Monitoring Performed? No ⊠ Yes □ (attach results)		
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Site constraints/Recommendations:

A site evaluation was conducted on November 8, 2018 by Paul Bartelt, Rich Paxton, Christina Nicholson, Nick Warnock and Lucero Cervantes of Bartelt Engineering. Test pits were excavated by Taylor Bailey Construction using a 420 D CAT backhoe with a 24 inch bucket. Darrel Choate of Napa County Environmental Health visited the site to inspect soil conditions. Test pits # 1 through #11 showed suitable soil for the installation of an Alternative Sewage Treatment System (ASTS) Subsurface Drip dispersal field within the area tested with required reserve area.

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Horizon Depth (triches) Boundary Boundary %Rock Texture Structure Side Wall Ped Weit Pores Roots Mottlin (Mottlin Wall 0-30* C 30-50 CL M, SB SH VFRB SS, P MVF, CF MF, CC None 30-54* G 30-50 SCL M, SB S VFRB SS, P MVF, CF FF None 54-66 >50 Decomposing Rock Layer None Side Side/Side/Side/Side/Side/Side/Side/Side/		[1			Consistend	ce			
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0-24* C 30-50 SCL M, SB S VFRB SS, P FF MF None 24-64* G 30-50 CL M, SB S VFRB SS, P CF, CM, CC None 64-68 0-15 Decomposing Rock Layer None 64-68 0-15 Decomposing Rock Layer None Slope = 11%. Acceptable soil depth observed: 64 inches. Assigned soil application rate = STE 0.25 gal/sf/day for a Conventional – Standard System STE 0.35 gal/sf/day for ASTS PTE 0.50 gal/sf/day for ASTS Subsurface Drip = 0.6 gal/sf/day (per Napa County Soil Application Rates) Subsurface Drip = 0.6 gal/sf/day (per Napa County Soil Application Rates) Subsurface Drip = 0.6 gal/sf/day (per Napa County Soil Application Rates) Subsurface Drip = 0.6 gal/sf/day (per Napa County Soil Application Rates) Subsurface Drip = 0.6 gal/sf/day (per Napa County Soil Application Rates) Subsurface Drip = 0.6 gal/sf/day (per Napa County Soil Application Rates) Subsurface Drip = 0.6 gal/sf/day (per Napa County Soil Application Rates) Subsurface Drip = 0.6 gal/sf/day (per Napa County Soil Application Rates) Subsurface Drip = 0.6 gal/sf/day (per Napa County Soil Application Rates) 0 ogroundwater observed. *See attached Soil Texture Analysis by Bouyoucos Hydrometry Method prepared by RGH Consultants, Inc. dated November 28, 2018. est Pit # 3 Horizon Depth (Inches) Ped Wet Pores Roots Mottling	Horizon Depth (Inches)	Boundary	%Rock	Texture	Structure	Side Wall	Ped	e Wet	Pores	Roots	Mottling
24-64* G 30-50 CL M, SB S VFRB SS, P CF, CM, CC CC None 64-68 0-15 Decomposing Rock Layer None Slope = 11%. Acceptable soil depth observed: 64 inches. Assigned soil application rate = STE 0.25 gal/sf/day for a Conventional – Standard System STE 0.35 gal/sf/day for ASTS PTE 0.50 gal/sf/day for ASTS Subsurface Drip = 0.6 gal/sf/day (per Napa County Soil Application Rates) Subsurface Drip = 0.6 gal/sf/day (per recommended Geoflow Drip Loading Rates) Stefusal at 68 inches deep. Limiting condition found at 64 inches deep. log groundwater observed. *See attached Soil Texture Analysis by Bouyoucos Hydrometry Method prepared by RGH Consultants, Inc. dated November 28, 2018. Yers Pores Roots Mottling Yest Pit # 3 3 Consistence Pores Roots Mottling	0-24*	С	30-50	SCL	M, SB	S	VFRB	SS, P	FF	MF	None
64-68 0-15 Decomposing Rock Layer None Slope = 11%. Acceptable soil depth observed: 64 inches. Assigned soil application rate = STE 0.25 gal/sf/day for a Conventional – Standard System STE 0.35 gal/sf/day for ASTS PTE 0.50 gal/sf/day for ASTS Subsurface Drip = 0.6 gal/sf/day (per Napa County Soil Application Rates) Subsurface Drip = 0.6 gal/sf/day (per recommended Geoflow Drip Loading Rates) None Refusal at 68 inches deep. Limiting condition found at 64 inches deep. See attached Soil Texture Analysis by Bouyoucos Hydrometry Method prepared by RGH Consultants, Inc. dated November 28, 2018. Texture Consistence Horizon Depth (Inches) Boundary %Rock Texture Structure Consistence Pores Roots Mottling	24-64*	G	30-50	CL	M, SB	S	VFRB	SS, P	CF, CM, CC	сс	None
Slope = 11%. Acceptable soil depth observed: 64 inches. Assigned soil application rate = STE 0.25 gal/sf/day for a Conventional – Standard System STE 0.35 gal/sf/day for ASTS PTE 0.50 gal/sf/day for ASTS Subsurface Drip = 0.6 gal/sf/day (per Napa County Soil Application Rates) Subsurface Drip = 0.6 gal/sf/day (per recommended Geoflow Drip Loading Rates) Subsurface Drip = 0.6 gal/sf/day (per recommended Geoflow Drip Loading Rates) Refusal at 68 inches deep. Io groundwater observed. *See attached Soil Texture Analysis by Bouyoucos Hydrometry Method prepared by RGH Consultants, Inc. dated November 28, 2018. Test Pit # 3 Horizon Depth (Inches) Boundary %Rock Texture Structure Stide Ped Wet Pores Roots Mottling	64-68		0-15			Decomp	bosing Roc	k Layer			None
Consultants, Inc. dated November 28, 2018. Test Pit # 3 Horizon Depth (Inches) Boundary %Rock Texture Structure Consistence Wall Vet Pores Roots Mottling	Slope = 11 Assigned s Refusal at No ground	 %. Acceptal soil applicatio 68 inches de water observ 	ole soil dep n rate = S S P S ep. Limitir ed. *See a	oth observed: TE 0.25 gal/s TE 0.35 gal/s TE 0.50 gal/s TE 0.50 gal/s ubsurface Displays ubsurface Displays to condition f ttached Soil	64 inches. of/day for a Co of/day for AST of/day for AST of/day for AST of/day for AST of/day for AST of/day for AST ound at 64 inc Texture Analy	onventiona FS FS f/day (per l f/day (per l ches deep /sis by Bou	I – Standar Napa Coun recomment	rd System ity Soil App ded Geoflo rdrometry N	blication Rate w Drip Loadir ∕lethod prepa	s) ng Rates) red by RGH	
Depth (Inches) Wall Wall	Consultant Test Pit # Horizon	s, Inc. dated	November %Rock	28, 2018.	Structure	(Consistence	2	Pores	Roots	Mottling
	Depth (Inches)	Doundary				Wall	Ped	vvet			N

None 0-54 н 30-30 >50 54-67 Decomposing Rock Layer None Slope = 10%. Acceptable soil depth observed: 54 inches. Assigned soil application rate = STE 0.33 gal/sf/day for a Conventional – Standard System STE 0.50 gal/sf/day for ASTS PTE 0.75 gal/sf/day for ASTS Subsurface Drip = 0.7 gal/sf/day (per Napa County Soil Application Rates) Subsurface Drip = 0.6 gal/sf/day (per recommended Geoflow Drip Loading Rates) No refusal at 67 inches deep. Limiting condition found at 54 inches deep. No Groundwater observed.

Test Pit # 4

Horizon	Duri					Consisten	ce			
Depth (Inches)	Boundary	%Rock	Iexture	Structure	Side Wall	Ped	Wet	Pores	Roots	Mottling
0-25	А	30-50	SCL	M, SB	S	FRB	SS, P	CF, CM	FF, FM	None
25-54	С	30-50	SCL	M, SB	SH	FRB	SS, P	CF, CM	FF, FM	None
54-58		0-15	С	М	VH	VF	N/A	CF	None	None
No refusal No ground	at 58 inches o water observe	PT Su Su deep. Limiti ed.	E 0.50 gais E 0.75 gal/s bsurface Dr bsurface Dr ng conditior	sf/day for AST sf/day for AST ip = 0.7 gal/sf ip = 0.6 gal/sf found at 54 i	S S /day (per /day (per nches dee	Napa Cour recommen ep.	nty Soil App ded Geoflo	plication Rate ow Drip Loadi	es) ng Rates)	
				normed	(Consistence	9	1		
Horizon Depth (Inches)	Boundary	%Rock	Texture	Structure	Side Wall	Ped	Wet	Pores	Roots	Mottling
0-36*	С	30-50	SCL	M, SB	SH	VFRB	SS, P	MVF, CF	CF, FC, FM	None
36-48		>50	SCL		D	ecomposin	ig Rock La	yer		None
Slope = 9% Assigned s No refusal No groundy Consultants	5. Acceptable oil application at 48 inches d vater observer s, Inc. dated N	soil depth rate = Ins ST PT Sul Sul eep. Limitir d. *See atta lovember 2	observed: 3 ufficient soil E 0.50 gal/s E 0.75 gal/s osurface Dri osurface Dri osurface Dri ng condition ached Soil T 8, 2018.	36 inches. depth for a C f/day for AST f/day for AST p = 0.7 gal/sf/ p = 0.6 gal/sf/ found at 36 ir exture Analys	onvention S S /day (per N /day (per r nches dee sis by Bou	al – Standa Vapa Coun ecommenc p. youcos Hyo	ard System ty Soil App led Geoflo drometry N	n Dication Rate: w Drip Loadir /lethod prepa	s) ng Rates) red by RGH	
est Pit #	6	* Hydrome	eter Test Pe	formed						
	I I				C	onsistence				

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Horizon			·	<u> </u>	CONSISTENCE		_			
Depth	Boundary	%ROCK	Texture	Structure	Side	Ped	Wet	Pores	Roots	Mottling
(Inches)					Wall					
0-27*	С	30-50	SCL	S, SB	SH	FRB	S, P	CF	FF	None
27-53*	G	30-50	L	M, SB	S	FRB	S, P	FVF, FF	FF, FC, FM	None
53-66*		0-15	SCL	M, SB	SH	VFRB	SS, P	CVF	FM	None
Slope = 13	%. Acceptat	ole soil dep	th observed:	66 inches.				L	1	
Assigned s	oil applicatio	n rate = S	ΓE 0.33 gal/s	f/day for a Co	onventiona	l – Standar	d System			
		S	TE 0.50 gal/s	f/day for AST	TS I					
		P.	TE 0.75 gal/s	f/day for AST	-S					
		S	ubsurface Dr	ip = 0.6 gal/st	f/day (per l	Vapa Coun	ty Soil App	lication Rate	s)	
	Subsurface Drip = 0.6 gal/sf/day (per recommended Geoflow Drip Loading Rates)									
No refusal at 66 inches deep.										
No ground	No groundwater observed. *See attached Soil Texture Analysis by Bouyoucos Hydrometry Method prepared by RGH									
Consultant	Consultants, Inc. dated November 28, 2018.									

Test Pit #

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	Horizon Boundany				(Consistenc	е			Mottling
Depth (Inches)	Boundary	%Rock	Texture	Structure	Side Wall	Ped	Wet	Pores	Roots	wottling
0-52	G	30-50	SCL	M, SB	SH	VFRB	SS, P	MF, CF, MVF	FF, CM, FC	None
52-66		30-50	SCL	M, SB	SH, H	FRB	SS, P	MF, MVF	None	None
Slope = 89 Assigned s	Slope = 8%. Acceptable soil depth observed: 66 inches. Assigned soil application rate = STE 0.33 gal/sf/day for a Conventional – Standard System STE 0.50 gal/sf/day for ASTS PTE 0.75 gal/sf/day for ASTS Subsurface Drip = 0.7 gal/sf/day (per Napa County Soil Application Rates) Subsurface Drip = 0.6 gal/sf/day (per recommended Geoflow Drip Loading Rates)									
No refusal No ground	No refusal at 66 inches deep. No groundwater observed.									

Test Pit # 8

Horizon Boundan		dan & Rock Texture Structure	(Consistenc	е			Mottling		
Depth (Inches)	Boundary	%Rock	Texture	Structure	Side Wall	Ped	Wet	Pores	Roots	Mottling
0-36	С	30-50	SCL	M, SB	SH	FRB	SS, P	FF	FF	None
36-54	G	15-30	SCL	M, SB	SH	FRB	SS, P	CVF, CF	FF	None
54-70		15-30	SCL	M, SB	SH	FRB	SS, P	CVF, CF	FF	None
Slope = 13 Assigned s	Slope = 13%. Acceptable soil depth observed: 70 inches. Assigned soil application rate = STE 0.33 gal/sf/day for a Conventional – Standard System STE 0.50 gal/sf/day for ASTS PTE 0.75 gal/sf/day for ASTS Subsurface Drip = 0.7 gal/sf/day (per Napa County Soil Application Rates) Subsurface Drip = 0.6 gal/sf/day (per recommended Geoflow Drip Loading Rates)									
No refusal No ground	No refusal at 70 inches deep. No groundwater observed.									

Test Pit #

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* Hydrometer Test Performed

11					C	Consistenc	е				
Depth (Inches)	Boundary	%Rock	Texture	Structure	Side Wall	Ped	Wet	Pores	Roots	Mottling	
0-50*	G	30-50	SCL	M, SB	SH, H	FRB	SS, P	MF, MVF	FC, CM, MF, MVF	None	
50-66		>50		Decomposing Rock Layer							
Slope = 7%	Slope = 7%. Acceptable soil depth observed: 50 inches.										
Assigned a	soil applicatio	n rate = In	sufficient soi	l depth for a 0	Convention	al – Stand	ard System	ו			
		S	TE 0.50 gal/s	sf/day for AST	rs To						
		Р	TE 0.75 gal/s	sf/day for AST	S						
		S	ubsurface Dr	ip = 0.7 gal/s	f/day (per N	Vapa Cour	nty Soil App	olication Rate	s)		
	Subsurface Drip = 0.6 gal/sf/day (per recommended Geoflow Drip Loading Rates)										
No refusal	No refusal at 66 inches deep. Limiting condition found at 50 inches deep.										
No ground	water observ	ed. [:] See at	ttached Soil	Fexture Analy	sis by Bou	youcos Hy	drometry N	/lethod prepa	red by RGH		
Consultant	Consultants, Inc. dated November 28, 2018.										

Test Pit #

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Horizon					(Consistenc	e	_		
Depth (Inches)	Boundary	%Rock	Texture	Structure	Side Wall	Ped	Wet	Pores	Roots	Mottling
0-26*	С	30-50	CL	M, SB	Н	FRB	SS, P	MF, CM	MF, MVF, FM	None
26-48*	G	30-50	SCL	M, SB	Н	FRB	SS, P	MF, MVF	None	None
48-56		>50	50 Granite/Decomposing Rock Layer							
Slope = 13 Assigned s	Slope = 13%. Acceptable soil depth observed: 48 inches. Assigned soil application rate = Insufficient soil depth for a Conventional – Standard System STE 0.35 gal/sf/day for ASTS PTE 0.50 gal/sf/day for ASTS Subsurface Drip = 0.6 gal/sf/day (per Napa County Soil Application Rates) Subsurface Drip = 0.6 gal/sf/day (per recommended Geoflow Drip Loading Rates)									
No refusal No ground Consultant	No refusal at 56 inches deep. Limiting condition found at 48 inches deep. No groundwater observed. *See attached Soil Texture Analysis by Bouyoucos Hydrometry Method prepared by RGH Consultants, Inc. dated November 28, 2018.									
1										

Test Pit #											
Horizon					(Consistenc	е				
Depth (Inches)	Boundary	%Rock	Texture	Structure	Side Wall	Ped	Wet	Pores	Roots	Mottling	
0-40	С	15-30	SCL	CL M, SB SH, H FRB SS, P MF, FM, MF, MVF MVF, CM							
40-54	С	0-15		Massive Clay None							
54-66		>50		Decomposing Rock Layer None							
Slope = 20 Assigned s	Slope = 20%. Acceptable soil depth observed: 40 inches. Assigned soil application rate = Insufficient soil depth for a Conventional – Standard System STE 0.50 gal/sf/day for ASTS PTE 0.75 gal/sf/day for ASTS Subsurface Drip = 0.7 gal/sf/day (per Napa County Soil Application Rates) Subsurface Drip = 0.6 gal/sf/day (per recommended Geoflow Drip Loading Rates)										
No refusal No ground	No refusal at 66 inches deep. Limiting condition found at 40 inches deep. No groundwater observed.										

Table of Abbreviations

				Consistence				
Boundary	Texture	Structure	Side Wall	Ped	Wet	Pores	Roots	Mottling
A=Abrupt <1" C=Clear 1"-2.5" G=Gradual 2.5"-5" D=Difuse >5"	S=Sand LS=Loamy Sand SL=Sandy Loam SCL=Sandy Clay Loam SC=Sandy Clay CL=Clay Loam L=Loam C=Clay SiC=Silty Clay SiC=Silty Clay SiL=Silt Loam Si=Silt	W=Weak M=Moderate S=Strong G=Granular PL=Platy Pr=Prismatic C=Columnar AB=Angular Blocky SB=Subangular Blocky M=Massive C=Cemented	L=Loose S=Soft SH=Slighty Hard H=Hard VH=Very Hard ExH=Extremely Hard	L=Loose VFRB=Very Friable FRB=Friable F=Firm VF=Very Firm ExF=Extremely Firm	NS=NonSticky SS=Slightly Sticky S=Sticky VS=Very Sticky NP=NonPlastic SP=Slightly Plastic P=Plastic VP=Very Plastic	Quantity: F=Few C=Common M=Many Size: VF=Very Fine F=Fine M=Medium C=Coarse	Quantity: F=Few C=Common M=Many Size: VF=Very Fine F=Fine M=Medium C=Coarse VC=Very Course	Quantity: F=Few C=Common M=Many Size: F=Fine M=Medium C=Coarse VC=Very Course ExC=Extremely Coarse Contrast: Ft=Faint D=Distinct P=Prominent

Attach additional sheets as needed

.

Conventional Sewage Treatment System Soil Application Rates

TEXTURE	STR	UCTURE	APPLICATION RATE (Gal/ft²/day)		
	Shape	Grade	STE		
Coarse Sand, Sand, Loamy Coarse Sand	Single grain	Structureless	Prohibited		
	Massive	Structureless	Prohibited		
Sandy Loam, Loamy Sand	Platy	Weak, mod, strong	Prohibited		
	Prismatic,	Weak	0.33		
	blocky, granular	Moderate, strong	0.5		
	Massive	Structureless	Prohibited		
Loam, Silt Loam, Sandy Clay Loam, Fine	Platy	Weak, mod, strong	Prohibited		
Sandy Loam	Prismatic,	Weak	0.25		
	blocky, granular	Moderate, Strong	0.33		
	Massive	Structureless	Prohibited		
Clav Loam	Platy	Weak, moderate, strong	Prohibited		
	Prismatic	Weak, moderate	0.25		
	blocky, granular	Strong	0.33		
	Massive	Structureless	Prohibited		
Condu Clou City Cloud com	Platy	Weak, moderate, strong	Prohibited		
Sandy Clay, Silly Clay Loam	Prismatic blocky	Weak, moderate	Prohibited		
	granular	Strong	0.25		
	Massive	Structureless	Prohibited		
Clay, Silty Clay	Platy	Weak, moderate, strong	Prohibited		
Sidy, Sity Sidy	Prismatic, blocky,	Weak	Prohibited		
	granular	Moderate, strong	Prohibited		

CONVENTIONAL SEWAGE TREATMENT SYSTEM SOIL APPLICATION RATES BASED ON PERCOLATION RATES							
Percolation Rate (mpi)	Application Rate (STE)						
< 5 MPI	Prohibited						
5 to 10 MPI	0.5						
10-20 MPI	0.33						
20-60 MPI	0.25						
> 60 MPI	Prohibited						

Alternative Sewage Treatment System Soil Application Rates

TEXTURE	ST	TRUCTURE	APPLICATION RATE (Gal/ft ² /day)		
	Shape	Grade	STE ¹	PTE ^{1,2}	
Coarse Sand, Sand, Loamy Coarse Sand	Single grain	Structureless	1.0	1.2	
Fine Sand, Loamy Fine Sand	Single grain Structureless		0.6	1.0	
	Massive	Structureless	0.35	0.5	
	Platy	Weak	0.35	0.5	
Sandy Loam, Loamy Sand	Prismatic blocky	Weak	0.5	0.75	
	granular	Moderate, Strong	0.8	1.0	
	Massive	Structureless			
Loam, Silt Loam, Sandy Clay	Platy	Weak, moderate, strong			
Loam, Fine Sandy Loam	Prismatic, blocky,	Weak, moderate	0.5	0.75	
	granular	Strong	0.8	1.0	
	Massive	Structureless			
Sandy Clay, Silty Clay Loam,	Platy	Weak, moderate, strong			
Clay Loam	Prismatic, blocky,	Weak, moderate	0.35	0.5	
	granular	Strong	0.6	0.75	
	Massive	Structureless			
Clay, Silty Clay	Platy	Weak, moderate, strong			
Oldy, Olity Oldy	Prismatic, blocky,	Weak			
	granular	Moderate, strong	0.2	0.25	

1. See Table 1 in the Design, Construction and Installation of Alternative Sewage Treatment Systems.

2. A higher application rate for pretreated effluent may only be used when pretreatment is not used for one foot of vertical separation credit.

MINIMUM SURFACE AREA GUIDELINES TO DISPOSE OF 100 GPD OF SECONDARY TREATED EFFLUENT FOR SUBSURFACE DRIP DISPERSAL SYSTEMS

		Soil Absorp	otion Rates			
Soil Class	Soil Type	Est. Soil Perc. Rate minutes/inch	Hydraulic Conductivity inches/hour	- Design Application Rate (Gal/ft²/day)	Sq. ft./100 gallons per day	
I	Coarse sand	1 – 5	>2	1.400	71.5	
I	Fine sand	5-10	1.5 – 2	1.200	83.3	
11	Sandy loam	10 – 20	1.0 - 1.5	1.000	100.0	
11	Loam	20 - 30	0.75 – 1.0	0.700	143.0	
	Clay loam	30 – 45	0.5 - 0.75	0.600	167.0	
111	Silt - clay loam	45 - 60	0.3 - 0.5	0.400	250.0	
IV	Clay non-swell	60 - 90	0.2 - 0.3	0.200	500.0	
IV	Clay - swell	90 – 120	0.1 - 0.2	0.100	1000.0	

1. For design purpose, the "Soil Type" category to be used in the above table shall be based on the most restrictive soil type encountered within two feet below the bottom of the drip line.

2. Dispersal field area calculation: Total square feet area of dispersal field = Design flow divided by loading rate.

TABLE 1

DRIP LOADING RATES CONSIDERING SOIL STRUCTURE.

Table 1 is taken from the State of Wisconsin code and was prepared by Jerry Tyler. Provided for guidelines and budgeting purposes. Refer to your local regulations and qualified soil scientists to determine best loading rates.

Course sand or coarserN/A1.60.4Loamy coarse sandN/A1.40.3SandN/A1.20.3Loamy sandWeak to strong1.20.3Loamy sandMassive0.70.2Fine sandModerate to strong0.90.3Fine sandModerate to strong0.90.3Loamy fine sandModerate to strong0.90.3Loamy fine sandModerate to strong0.60.2Very fine sandN/A0.60.2Sandy loamModerate to strong0.90.3Loamy fine sandN/A0.60.2Sandy loamModerate to strong0.90.2Sandy loamModerate to strong0.90.2Sandy loamWeak, weak platy0.60.2LoamModerate to strong0.80.2LoamModerate to strong0.80.2LoamModerate to strong0.80.2LoamModerate to strong0.80.2LoamModerate to strong0.60.2Silt loamModerate to strong0.60.2	Soil Textures	Soil Structure	Maximum Monthly Average BOD ₅ <30mg/L TSS<30mg/L (gallons/ft ² /day)	Maximum Monthly Average BOD ₅ >30mg/L TSS>30mg/L (gallons/ft ² /day)
Loamy coarse sand N/A 1.4 0.3 Sand N/A 1.2 0.3 Loamy sand Weak to strong 1.2 0.3 Loamy sand Massive 0.7 0.2 Fine sand Moderate to strong 0.9 0.3 Fine sand Massive or weak 0.6 0.2 Loamy fine sand Massive or weak 0.6 0.2 Loamy fine sand Massive or weak 0.6 0.2 Very fine sand M/A 0.6 0.2 Sandy loam Moderate to strong 0.9 0.2 Sandy loam Moderate to strong 0.9 0.2 Sandy loam Moderate to strong 0.6 0.2 Loam Moderate to strong 0.8 0.2 Loam Moderate to strong 0.8 0.2 Loam Moderate to strong 0.6 0.2 Loam Moderate to strong 0.6 0.2 Silt loam Moderate to strong 0.6 0.2	Course sand or coarser	N/A	1.6	0.4
SandN/A1.20.3Loamy sandWeak to strong1.20.3Loamy sandMassive0.70.2Fine sandModerate to strong0.90.3Fine sandMassive or weak0.60.2Loamy fine sandModerate to strong0.90.3Loamy fine sandModerate to strong0.90.3Loamy fine sandMassive or weak0.60.2Very fine sandN/A0.60.2Sandy loamModerate to strong0.90.2Sandy loamModerate to strong0.90.2Sandy loamModerate to strong0.80.2Loamy loamModerate to strong0.80.2LoamModerate to strong0.80.2LoamModerate to strong0.80.2Silt loamModerate to strong0.60.2Silt loamModerate to strong0.60.2Sandy clay loamModerate to strong0.60.2 <td>Loamy coarse sand</td> <td>N/A</td> <td>1.4</td> <td>0.3</td>	Loamy coarse sand	N/A	1.4	0.3
Loamy sandWeak to strong1.20.3Loamy sandMassive0.70.2Fine sandModerate to strong0.90.3Fine sandMassive or weak0.60.2Loamy fine sandModerate to strong0.90.3Loamy fine sandMassive or weak0.60.2Very fine sandN/A0.60.2Sandy loamModerate to strong0.90.2Sandy loamModerate to strong0.90.2Sandy loamModerate to strong0.90.2Sandy loamMassive0.50.1LoamModerate to strong0.80.2LoamModerate to strong0.80.2LoamModerate to strong0.80.2LoamMassive0.50.1LoamModerate to strong0.80.2LoamMassive0.50.1Silt loamModerate to strong0.80.2Silt loamModerate to strong0.80.2Sandy clay loamModerate to strong0.60.2Sandy clay loamModerate to strong0.60.2Sandy clay loamModerate to strong0.60.2Sandy clay loamModerate to strong0.60.2Clay loamModerate to strong0.60.2Sandy clay loamModerate to strong0.60.2Silt planModerate to strong0.60.2Silt planMassive0.00.	Sand	N/A	1.2	0.3
Loamy sandMassive0.70.2Fine sandModerate to strong0.90.3Fine sandMassive or weak0.60.2Loamy fine sandModerate to strong0.90.3Loamy fine sandMassive or weak0.60.2Very fine sandN/A0.60.2Loamy very fine sandN/A0.60.2Sandy loamModerate to strong0.90.2Sandy loamModerate to strong0.90.2Sandy loamModerate to strong0.80.2LoamModerate to strong0.80.2LoamModerate to strong0.80.2LoamModerate to strong0.80.2LoamModerate to strong0.80.2LoamModerate to strong0.80.2Silt loamModerate to strong0.80.2Silt loamModerate to strong0.60.2Sandy clay loamModerate to strong0.60.2Sandy clay loamModerate to strong0.60.2Sandy clay loamModerate to strong0.60.2Clay loamModerate to strong0.60.2Clay loamModerate to strong0.60.2Silty clay loamModerate to strong0.60.2Silty clay loamModerate to strong0.60.2Silty clay loamModerate to strong0.60.2Silty clay loamModerate to strong0.60.2	Loamy sand	Weak to strong	1.2	0.3
Fine sandModerate to strong0.90.3Fine sandMassive or weak0.60.2Loamy fine sandModerate to strong0.90.3Loamy fine sandMassive or weak0.60.2Very fine sandM/A0.60.2Loamy very fine sandN/A0.60.2Sandy loamModerate to strong0.90.2Sandy loamWeak, weak platy0.60.2Sandy loamModerate to strong0.80.2LoamModerate to strong0.80.2LoamModerate to strong0.80.2LoamModerate to strong0.80.2LoamModerate to strong0.80.2Silt loamModerate to strong0.80.2Silt loamModerate to strong0.60.2Sandy clay loamModerate to strong0.60.2Silt y clay loamModerate to strong0.60.2Silty clay loamModerate to strong0.60.2Silty clay loamModerate to strong0.60.2Silty clay loamModerate to strong0.60.2Silty clay loamModerate to strong0.30.1Silty clay loamModerate to strong <td>Loamy sand</td> <td>Massive</td> <td>0.7</td> <td>0.2</td>	Loamy sand	Massive	0.7	0.2
Fine sandMassive or weak0.60.2Loamy fine sandModerate to strong0.90.3Loamy fine sandMassive or weak0.60.2Very fine sandN/A0.60.2Loamy very fine sandN/A0.60.2Sandy loamModerate to strong0.90.2Sandy loamWeak, weak platy0.60.2Sandy loamModerate to strong0.80.2LoamModerate to strong0.80.2LoamModerate to strong0.80.2LoamModerate to strong0.80.2LoamModerate to strong0.80.2LoamModerate to strong0.80.2Silt loamModerate to strong0.80.2Silt loamModerate to strong0.60.2Sandy clay loamModerate to strong0.60.2Sandy clay loamModerate to strong0.60.2Sandy clay loamModerate to strong0.60.2Sandy clay loamModerate to strong0.60.2Clay loamModerate to strong0.60.2Silt y clay loamModerate to strong0.30.1Silt y clay loamMassive0.0	Fine sand	Moderate to strong	0.9	0.3
Loamy fine sand Moderate to strong 0.9 0.3 Loamy fine sand Massive or weak 0.6 0.2 Very fine sand N/A 0.6 0.2 Loamy very fine sand N/A 0.6 0.2 Sandy loam Moderate to strong 0.9 0.2 Sandy loam Weak, weak platy 0.6 0.2 Sandy loam Weak, weak platy 0.6 0.2 Loam Moderate to strong 0.8 0.2 Silt loam Moderate to strong 0.8 0.2 Silt loam Moderate to strong 0.6 0.2 Sandy clay loam Moderate to strong 0.6 0.2 Sandy clay loam Moderate to strong 0.6 0.2 Clay loam Moderate to strong	Fine sand	Massive or weak	0.6	0.2
Loamy fine sandMassive or weak0.60.2Very fine sandN/A0.60.2Loamy very fine sandN/A0.60.2Sandy loamModerate to strong0.90.2Sandy loamWeak, weak platy0.60.2Sandy loamWeak, weak platy0.60.2LoamModerate to strong0.80.2LoamModerate to strong0.80.2LoamModerate to strong0.80.2LoamModerate to strong0.80.2LoamModerate to strong0.80.2LoamModerate to strong0.80.2Silt loamModerate to strong0.80.2Silt loamModerate to strong0.60.2Sandy clay loamModerate to strong0.60.2Sandy clay loamModerate to strong0.60.2Sandy clay loamModerate to strong0.60.2Sandy clay loamModerate to strong0.60.2Clay loamModerate to strong0.60.2Silty clay loamModerate to strong0.3 <td< td=""><td>Loamy fine sand</td><td>Moderate to strong</td><td>0.9</td><td>0.3</td></td<>	Loamy fine sand	Moderate to strong	0.9	0.3
Very fine sandN/A0.60.2Loamy very fine sandN/A0.60.2Sandy loamModerate to strong0.90.2Sandy loamWeak, weak platy0.60.2Sandy loamMassive0.50.1LoamModerate to strong0.80.2LoamWeak, weak platy0.60.2LoamModerate to strong0.80.2LoamMassive0.50.1Silt loamModerate to strong0.80.2Silt loamModerate to strong0.80.2Silt loamModerate to strong0.60.2Sandy clay loamModerate to strong0.60.2Sandy clay loamModerate to strong0.60.2Sandy clay loamModerate to strong0.60.2Sandy clay loamMassive0.00.0Clay loamModerate to strong0.60.2Silt y loamMassive0.00.0Silty clay loamMassive0.00.0Silty clay loamMassive0.00.0Silty clay loamMassive0.00.0Silty clay loamMassive0.00.0Silty clay loamMassive0.00.0Silty clay loamMassive to weak0.00.0Silty clay loamMassive to weak0.00.0Silty clay loamMassive to weak0.00.0Sinty clayMassive to weak0.00.0 <td>Loamy fine sand</td> <td>Massive or weak</td> <td>0.6</td> <td>0.2</td>	Loamy fine sand	Massive or weak	0.6	0.2
Loamy very fine sandN/A0.60.2Sandy loamModerate to strong0.90.2Sandy loamWeak, weak platy0.60.2Sandy loamMassive0.50.1LoamModerate to strong0.80.2LoamWeak, weak platy0.60.2LoamModerate to strong0.80.2LoamMassive0.50.1Silt loamModerate to strong0.80.2Silt loamModerate to strong0.80.2Silt loamModerate to strong0.80.2Silt loamModerate to strong0.60.2Sandy clay loamModerate to strong0.60.2Clay loamModerate to strong0.60.2Silty clay loamModerate to strong0.30.1Silty clay loamMassive0.00.0Sandy clayModerate to strong0.30.1Silty clay loamMassive to weak0.00.0 <td>Very fine sand</td> <td>N/A</td> <td>0.6</td> <td>0.2</td>	Very fine sand	N/A	0.6	0.2
Sandy loamModerate to strong0.90.2Sandy loamWeak, weak platy0.60.2Sandy loamMassive0.50.1LoamModerate to strong0.80.2LoamWeak, weak platy0.60.2LoamMassive0.50.1Silt loamModerate to strong0.80.2Silt loamModerate to strong0.80.2Silt loamModerate to strong0.80.2Silt loamModerate to strong0.60.2Sandy clay loamModerate to strong0.60.2Clay loamModerate to strong0.60.2Silty clay loamModerate to strong0.30.1Silty clay loamMassive0.00.0Sandy clayMassive to weak0.00.0ClayModerate to strong0.30.1Sandy clayMassive to weak0.00.0<	Loamy very fine sand	N/A	0.6	0.2
Sandy loam Weak, weak platy 0.6 0.2 Sandy loam Massive 0.5 0.1 Loam Moderate to strong 0.8 0.2 Loam Weak, weak platy 0.6 0.2 Loam Weak, weak platy 0.6 0.2 Loam Massive 0.5 0.1 Silt loam Moderate to strong 0.8 0.2 Silt loam Weak, weak platy 0.3 0.1 Silt loam Moderate to strong 0.6 0.2 Sandy clay loam Moderate to strong 0.6 0.2 Sandy clay loam Moderate to strong 0.6 0.2 Sandy clay loam Measive 0.0 0.0 Clay loam Moderate to strong 0.6 0.2 Clay loam Moderate to strong 0.6 0.2 Silt clay loam Moderate to strong 0.6 0.2 Silty clay loam Moderate to strong 0.6 0.2 Silty clay loam Moderate to strong	Sandy loam	Moderate to strong	0.9	0.2
Sandy loamMassive0.50.1LoamModerate to strong0.80.2LoamWeak, weak platy0.60.2LoamMassive0.50.1Silt loamModerate to strong0.80.2Silt loamModerate to strong0.80.2Silt loamModerate to strong0.80.2Silt loamModerate to strong0.10.1Silt loamModerate to strong0.60.2Sandy clay loamModerate to strong0.60.2Sandy clay loamMeak, weak platy0.30.1Sandy clay loamModerate to strong0.60.2Clay loamModerate to strong0.60.2Clay loamModerate to strong0.60.2Silty clay loamModerate to strong0.60.2Silty clay loamMassive0.00.0Silty clay loamModerate to strong0.60.2Silty clay loamModerate to strong0.60.2Silty clay loamModerate to strong0.60.2Silty clay loamMassive0.00.0Sandy clayMassive0.00.0Sandy clayMassive to weak0.00.0Sandy clayMassive to weak0.00.0Sandy clayMassive to weak0.00.0ClayModerate to strong0.30.1Sandy clayMassive to weak0.00.0	Sandy loam	Weak, weak platy	0.6	0.2
LoamModerate to strong0.80.2LoamWeak, weak platy0.60.2LoamMassive0.50.1Silt loamModerate to strong0.80.2Silt loamWeak, weak platy0.30.1Silt loamMederate to strong0.60.2Silt loamModerate to strong0.60.2Sandy clay loamModerate to strong0.60.2Sandy clay loamWeak, weak platy0.30.1Sandy clay loamMederate to strong0.60.2Clay loamModerate to strong0.60.2Clay loamModerate to strong0.60.2Clay loamModerate to strong0.60.2Silty clay loamMassive0.00.0Sandy clayModerate to strong0.30.1Sandy clayMassive to weak0.00.0ClayModerate to strong0.30.1ClayModerate to strong0.30.1ClayModerate to strong0.30.1ClayModerate to strong0.30.1ClayModerate to strong0.30.1ClayMode	Sandy loam	Massive	0.5	0.1
LoamWeak, weak platy0.60.2LoamMassive0.50.1Silt loamModerate to strong0.80.2Silt loamWeak, weak platy0.30.1Silt loamMassive0.20.0Sandy clay loamModerate to strong0.60.2Sandy clay loamModerate to strong0.60.2Sandy clay loamModerate to strong0.60.2Sandy clay loamMassive0.00.0Clay loamModerate to strong0.60.2Clay loamModerate to strong0.60.2Silt clay loamModerate to strong0.60.2Clay loamModerate to strong0.60.2Silty clay loamMassive0.00.0Sandy clayModerate to strong0.30.1Sandy clayMassive to weak0.00.0ClayModerate to strong0.30.1ClayModerate to strong0.30.1	Loam	Moderate to strong	0.8	0.2
LoamMassive0.50.1Silt loamModerate to strong0.80.2Silt loamWeak, weak platy0.30.1Silt loamMassive0.20.0Sandy clay loamModerate to strong0.60.2Sandy clay loamWeak, weak platy0.30.1Sandy clay loamWeak, weak platy0.30.1Sandy clay loamModerate to strong0.60.2Clay loamModerate to strong0.60.2Clay loamModerate to strong0.60.2Clay loamModerate to strong0.60.2Silty clay loamMassive0.00.0Sandy clayModerate to strong0.30.1Sandy clayModerate to strong0.30.1Sandy clayMassive to weak0.00.0ClayModerate to strong0.30.1ClayMassive to weak0.00.0	Loam	Weak, weak platy	0.6	0.2
Silt loamModerate to strong0.80.2Silt loamWeak, weak platy0.30.1Silt loamMassive0.20.0Sandy clay loamModerate to strong0.60.2Sandy clay loamWeak, weak platy0.30.1Sandy clay loamWeak, weak platy0.30.1Sandy clay loamModerate to strong0.60.2Clay loamModerate to strong0.60.2Clay loamModerate to strong0.60.2Clay loamModerate to strong0.60.2Silty clay loamModerate to strong0.30.1Silty clay loamMassive0.00.0Sandy clayModerate to strong0.30.1Sandy clayModerate to strong0.30.1Sandy clayMassive to weak0.00.0ClayModerate to strong0.30.1ClayMassive to weak0.00.0	Loam	Massive	0.5	0.1
Silt loamWeak, weak platy0.30.1Silt loamMassive0.20.0Sandy clay loamModerate to strong0.60.2Sandy clay loamWeak, weak platy0.30.1Sandy clay loamMassive0.00.0Clay loamModerate to strong0.60.2Clay loamModerate to strong0.60.2Clay loamModerate to strong0.60.2Clay loamModerate to strong0.60.2Silty clay loamModerate to strong0.30.1Silty clay loamMassive0.00.0Sandy clayModerate to strong0.30.1Sandy clayMassive to weak0.00.0ClayModerate to strong0.30.1ClayModerate to strong0.30.1	Silt loam	Moderate to strong	0.8	0.2
Silt loamMassive0.20.0Sandy clay loamModerate to strong0.60.2Sandy clay loamWeak, weak platy0.30.1Sandy clay loamMassive0.00.0Clay loamModerate to strong0.60.2Clay loamModerate to strong0.60.2Clay loamWeak, weak platy0.30.1Clay loamMeak, weak platy0.30.1Clay loamModerate to strong0.60.2Silty clay loamModerate to strong0.60.2Silty clay loamModerate to strong0.60.2Silty clay loamMeak, weak platy0.30.1Silty clay loamMeak, weak platy0.30.1Silty clay loamMassive0.00.0Sandy clayModerate to strong0.30.1Sandy clayMassive to weak0.00.0ClayModerate to strong0.30.1ClayMassive to weak0.00.0	Silt loam	Weak, weak platy	0.3	0.1
Sandy clay loamModerate to strong0.60.2Sandy clay loamWeak, weak platy0.30.1Sandy clay loamMassive0.00.0Clay loamModerate to strong0.60.2Clay loamWeak, weak platy0.30.1Clay loamWeak, weak platy0.30.1Clay loamModerate to strong0.60.2Silty clay loamModerate to strong0.60.2Silty clay loamModerate to strong0.60.2Silty clay loamWeak, weak platy0.30.1Silty clay loamMassive0.00.0Sandy clayModerate to strong0.30.1Sandy clayModerate to strong0.30.1ClayModerate to strong0.30.1ClayMassive to weak0.00.0ClayMassive to weak0.00.0	Silt loam	Massive	0.2	0.0
Sandy clay loamWeak, weak platy0.30.1Sandy clay loamMassive0.00.0Clay loamModerate to strong0.60.2Clay loamWeak, weak platy0.30.1Clay loamMassive0.00.0Silty clay loamModerate to strong0.60.2Silty clay loamModerate to strong0.60.2Silty clay loamModerate to strong0.60.2Silty clay loamMeak, weak platy0.30.1Silty clay loamMassive0.00.0Sandy clayModerate to strong0.30.1Sandy clayMassive to weak0.00.0ClayModerate to strong0.30.1ClayMassive to weak0.00.0	Sandy clay loam	Moderate to strong	0.6	0.2
Sandy clay loamMassive0.00.0Clay loamModerate to strong0.60.2Clay loamWeak, weak platy0.30.1Clay loamMassive0.00.0Silty clay loamModerate to strong0.60.2Silty clay loamWeak, weak platy0.30.1Silty clay loamWeak, weak platy0.30.1Silty clay loamMassive0.00.0Sandy clayModerate to strong0.30.1Sandy clayMassive to weak0.00.0ClayModerate to strong0.30.1ClayMassive to weak0.00.0	Sandy clay loam	Weak, weak platy	0.3	0.1
Clay loamModerate to strong0.60.2Clay loamWeak, weak platy0.30.1Clay loamMassive0.00.0Silty clay loamModerate to strong0.60.2Silty clay loamWeak, weak platy0.30.1Silty clay loamMassive0.00.0Silty clay loamMassive0.00.0Sandy clayModerate to strong0.30.1Sandy clayMassive to weak0.00.0ClayModerate to strong0.30.1ClayMassive to weak0.00.0	Sandy clay loam	Massive	0.0	0.0
Clay loamWeak, weak platy0.30.1Clay loamMassive0.00.0Silty clay loamModerate to strong0.60.2Silty clay loamWeak, weak platy0.30.1Silty clay loamMassive0.00.0Sandy clayModerate to strong0.30.1Sandy clayMassive to weak0.00.0ClayModerate to strong0.30.1ClayMassive to weak0.00.0	Clay loam	Moderate to strong	0.6	0.2
Clay loamMassive0.00.0Silty clay loamModerate to strong0.60.2Silty clay loamWeak, weak platy0.30.1Silty clay loamMassive0.00.0Sandy clayModerate to strong0.30.1Sandy clayMassive to weak0.00.0ClayModerate to strong0.30.1ClayMassive to weak0.00.0	Clay loam	Weak, weak platy		0.1
Silty clay loamModerate to strong0.60.2Silty clay loamWeak, weak platy0.30.1Silty clay loamMassive0.00.0Sandy clayModerate to strong0.30.1Sandy clayMassive to weak0.00.0ClayModerate to strong0.30.1ClayMassive to weak0.00.0	Clay loam	Massive	0.0	0.0
Silty clay loamWeak, weak platy0.30.1Silty clay loamMassive0.00.0Sandy clayModerate to strong0.30.1Sandy clayMassive to weak0.00.0ClayModerate to strong0.30.1ClayMassive to weak0.00.0	Silty clay loam	Moderate to strong	0.6	0.2
Silty clay loamMassive0.00.0Sandy clayModerate to strong0.30.1Sandy clayMassive to weak0.00.0ClayModerate to strong0.30.1ClayMassive to weak0.00.0	Silty clay loam	Weak, weak platy	0.3	0.1
Sandy clayModerate to strong0.30.1Sandy clayMassive to weak0.00.0ClayModerate to strong0.30.1ClayMassive to weak0.00.0	Silty clay loam	Massive	0.0	0.0
Sandy ClayMassive to weak0.00.0ClayModerate to strong0.30.1ClayMassive to weak0.00.0	Sandy clay	Moderate to strong	0.3	0.1
ClayModerate to strong0.50.1ClayMassive to weak0.00.0	Sandy clay	Iviassive to weak	0.0	0.0
	Clay	Massime to strong	0.5	0.1
Silty clay Moderate to strong 0.3 0.1	Silty clay	Moderate to strong		0.0
Silty clay Massive to weak 0.0 0.0	Silty clay	Massive to weak	0.0	0.0



Santa Rosa Office 1305 North Dutton Ave. Santa Rosa, CA 95401 P: 707-544-1072 F: 707-544-1082

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Middletown Office

P.O. Box 652 Middletown, CA 95461 P: 707-987-4602 F: 707-987-4603

Bouyoucos Hydrometer

Client:	Bartelt Engineering	Sampled:	Not Stated
Project:	Rombauer	Received:	11/13/2018
Project #:	9147.79	Reported:	11/28/2018
Client Project #:	96-07		

Sample Number	TP-1	TP-1	TP-2	TP-2	TP-5	TP-6	TP-6	TP-6
Depth	Hor. 1	Hor. 2	Hor. 1	Hor. 2	Hor. 1	Hor. 1	Hor. 2	Hor. 3
A. Oven Dry Wt.	50.0	50.0	50.0	50.0	50.0	50.0	50.0	50.0
B. Starting Time (hr:min)	10:00	9:58	9:56	9:54	9:52	9:50	9:48	14:54
C. Temp. @ 40 sec. (F)	65.2	65.2	65.2	65.2	65.2	65.2	65.2	64.3
D. Hydro Reading @ 40 sec.	37.0	33.5	30.0	35.5	31.0	36.0	33.0	28.5
E. Comp. Correction	-6.5	-6.5	-6.5	-6.5	-6.5	-6.5	-6.5	-6.6
F. True Density @ 40 sec.								
(D-E)	30.5	27.0	23.5	29.0	24.5	29.5	26.5	21.9
G. Temp. @ 2 hrs. (F)	65.0	65.0	65.0	65.0	65.0	65.0	65.0	64.9
H. Hydro Reading @ 2 hrs.	22.5	20.0	17.0	22.0	17.0	21.0	17.5	17.0
I. Comp. Correction	-6.5	-6.5	-6.5	-6.5	-6.5	-6.5	-6.5	-6.5
J. True Density @ 2 hrs. (H-I)	16.0	13.5	10.5	15.5	10.5	14.5	11.0	10.5
K. % Sand=100-((F/A) x 100)	39.0	46.0	53.0	42.0	51.0	41.0	47.0	56.2
L. % Clay= ((J/A) x 100)	32.0	27.0	21.0	31.0	21.0	29.0	22.0	21.0
M. % Silt= 100-(K+L)	29.0	27.0	26.0	27.0	28.0	30.0	31.0	22.8
N. % Retained #10=	25.7	20.9	27.4	14.3	· 30.6	25.2	12.6	9.4
Dry Wt. Before Wash + Tare	922.5	953.3	979.7	1137.0	1269.0	1431.9	1345.0	1049.2
Dry Wt. After Wash + Tare	311.8	279.6	341.6	249.5	459.8	438.2	256.1	188.8
Dry Wt. Passing #10	610.7	673.7	638.1	887.5	809.2	993.7	1088.9	860.4
Tare Weight	100.6	101.1	100.3	101.9	102.5	103.0	98.9	100.0
Dry Wt. Before Wash	821.9	852.2	879.4	1035.1	1166.5	1328.9	1246.1	949.2
% Passing #10	74.3	79.1	72.6	85.7	69.4	74.8	87.4	90.6
% #10	25.7	20.9	27.4	14.3	30.6	25.2	12.6	9.4



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Bouyoucos Hydrometer

Project #:	Ba	Rombauer 9147.79	ering		Sampled: Received: Reported:	Not 11/13 11/13	5tated 3/2018 8/2018	
Client Project #:		96-07						
Sample Number	TP-9	TP-10	TP-10	Ι				
Depth	Hor. 1	Hor. 1	Hor. 2					
A. Oven Dry Wt.	50.0	50.0	50.0					
B. Starting Time (hr:min)	14:52	14:50	14:48					
C. Temp. @ 40 sec. (F)	64.3	64.3	64.3					
D. Hydro Reading @ 40 sec.	33.5	39.0	34.5					
E. Comp. Correction	-6.6	-6.6	-6.6					
F. True Density @ 40 sec.								
(D-E)	26.9	32.4	27.9					
G. Temp. @ 2 hrs. (F)	64.9	64.9	64.9					
H. Hydro Reading @ 2 hrs.	18.5	24.0	19.5					
I. Comp. Correction	-6.5	-6.5	-6.5					
J. True Density @ 2 hrs. (H-I)	12.0	17.5	13.0			ж. Т		
K. % Sand=100-((F/A) x 100)	46.2	35.2	44.2					
L. % Clay= ((J/A) x 100)	24.0	35.0	26.0					
M. % Silt= 100-(K+L)	29.8	29.8	29.8					
N. % Retained #10=	26.3	36.4	25.4					
			3					
Dry Wt. Before Wash + Tare	1131.4	1476.1	1194.0					
Dry Wt. After Wash + Tare	373.6	602.0	380.6					
Dry Wt. Passing #10	757.8	874.1	813.4					
Tare Weight	103.4	101.7	103.4					
Dry Wt. Before Wash	1028.0	1374.4	1090.6					
% Passing #10	73.7	63.6	74.6					
% #10	26.3	36.4	25.4					



INSTRUCTIONS:

- I. PLOT TEXTURE ON TRIANGLE BASED ON PERCENT SAND, SILT AND CLAY AS DETERMINED BY HYDROMETER ANALYSIS.
- 2. ADJUST FOR COARSE FRAGMENTS BY MOVING THE PLOTTED POINT IN THE SAND DIRECTION AN ADDITIONAL 2% FOR EACH 10% (BY VOLUME) OF FRAGMENTS GREATER THAN 2mm IN DIAMETER.
- 3. ADJUST FOR COMPACTNESS OF SOIL BY MOVING THE PLOTTED POINT IN THE CLAY DIRECTION AN ADDITIONAL 15% FOR SOILS HAVING A BULK-DENSITY GREATER THAN 1.7gm/cc.

NOTE:

FOR SOILS FALLING IN SAND, LOAMY SAND OR SANDY LOAM CLASSIFICATION, A BULK DENSITY ANALYSIS WILL GENERALLY NOT AFFECT SUITABILITY AND ANALYSIS IS NOT NECESSARY.



	Rombauer Vineyards 3522 Silverado Trail Napa, CA 94574				
I	APN 021-410-025				
	Job No. 96-07 December 2018				



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Rombauer Vineyards 3522 Silverado Trail Napa, CA 94574 APN 021-410-025 lob No. 96-07 December 2018



November 28, 2018

Project:RombauerProject #:9147.79Client Project #:96-07

Bartelt Engineering 1303 Jefferson Street, Ste. 200B Napa, CA 94559 Sampled: Not Stated Received: 11/13/2018 Reported: 11/28/2018

Subject: Laboratory Test Results Soil Texture Analysis by Bouyoucos Hydrometry Method

Dear Mr. Bartelt:

This letter transmits the results of our laboratory testing performed for the subject project. We performed a Soil Texture Analysis by the Bouyoucos Hydrometery Method with the following results:

	TP-1
Size/Density	Horizon 1
+ #10 Sieve	25.7%
Sand	39.0%
Clay	32.0%
Silt	29.0%
Db g/cc	

We trust this provides the information required at this time. Should you have further questions, please call.

Regards,

RGH GEOTECHNICAL



November 28, 2018

Project:	Rombauer
Project #:	9147.79
Client Project #:	96-07

Bartelt Engineering 1303 Jefferson Street, Ste. 200B Napa, CA 94559

Subject: Laboratory Test Results Soil Texture Analysis by Bouyoucos Hydrometry Method

Dear Mr. Bartelt:

This letter transmits the results of our laboratory testing performed for the subject project. We performed a Soil Texture Analysis by the Bouyoucos Hydrometery Method with the following results:

	TP-1
Size/Density	Horizon 2
+ #10 Sieve	20.9%
Sand	46.0%
Clay	27.0%
Silt	27.0%
Db g/cc	

We trust this provides the information required at this time. Should you have further questions, please call.

Regards,

RGH GEOTECHNICAL

Sean Flinn Laboratory Technician



November 28, 2018

Project:	Rombauer
Project #:	9147.79
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Dear Mr. Bartelt:

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	TP-2
Size/Density	Horizon 1
+ #10 Sieve	27.4%
Sand	53.0%
Clay	21.0%
Silt	26.0%
Db g/cc	

We trust this provides the information required at this time. Should you have further questions, please call.

Regards,

RGH GEOTECHNICAL

Sean Flinn Laboratory Technician



November 28, 2018

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Project #:	9147.79
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Dear Mr. Bartelt:

This letter transmits the results of our laboratory testing performed for the subject project. We performed a Soil Texture Analysis by the Bouyoucos Hydrometery Method with the following results:

	TP-2
Size/Density	Horizon 2
+ #10 Sieve	14.3%
Sand	42.0%
Clay	31.0%
Silt	27.0%
Db g/cc	

We trust this provides the information required at this time. Should you have further questions, please call.

Regards,

RGH GEOTECHNICAL

Sean Flinn Laboratory Technician



November 28, 2018

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Dear Mr. Bartelt:

This letter transmits the results of our laboratory testing performed for the subject project. We performed a Soil Texture Analysis by the Bouyoucos Hydrometery Method with the following results:

	TP-5
Size/Density	Horizon 1
+ #10 Sieve	30.6%
Sand	51.0%
Clay	21.0%
Silt	28.0%
Db g/cc	

We trust this provides the information required at this time. Should you have further questions, please call.

Regards,

RGH GEOTECHNICAL

Sean Flinn Laboratory Technician

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Dear Mr. Bartelt:

This letter transmits the results of our laboratory testing performed for the subject project. We performed a Soil Texture Analysis by the Bouyoucos Hydrometery Method with the following results:

	TP-6
Size/Density	Horizon 1
+ #10 Sieve	25.2%
Sand	41.0%
Clay	29.0%
Silt	30.0%
Db g/cc	as 15

We trust this provides the information required at this time. Should you have further questions, please call.

Regards,

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	TP-6
Size/Density	Horizon 2
+ #10 Sieve	12.6%
Sand	47.0%
Clay	22.0%
Silt	31.0%
Db g/cc	

We trust this provides the information required at this time. Should you have further questions, please call.

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Dear Mr. Bartelt:

This letter transmits the results of our laboratory testing performed for the subject project. We performed a Soil Texture Analysis by the Bouyoucos Hydrometery Method with the following results:

	TP-6
Size/Density	Horizon 3
+ #10 Sieve	9.4%
Sand	56.2%
Clay	21.0%
Silt	22.8%
Db g/cc	

We trust this provides the information required at this time. Should you have further questions, please call.

Regards,

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November 28, 2018

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Dear Mr. Bartelt:

This letter transmits the results of our laboratory testing performed for the subject project. We performed a Soil Texture Analysis by the Bouyoucos Hydrometery Method with the following results:

	TP-9
Size/Density	Horizon 1
+ #10 Sieve	26.3%
Sand	46.2%
Clay	24.0%
Silt	29.8%
Db g/cc	A 10

We trust this provides the information required at this time. Should you have further questions, please call.

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Dear Mr. Bartelt:

This letter transmits the results of our laboratory testing performed for the subject project. We performed a Soil Texture Analysis by the Bouyoucos Hydrometery Method with the following results:

	TP-10
Size/Density	Horizon 1
+ #10 Sieve	36.4%
Sand	35.2%
Clay	35.0%
Silt	29.8%
Db g/cc	

We trust this provides the information required at this time. Should you have further questions, please call.

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Dear Mr. Bartelt:

This letter transmits the results of our laboratory testing performed for the subject project. We performed a Soil Texture Analysis by the Bouyoucos Hydrometery Method with the following results:

	TP-10
Size/Density	Horizon 2
+ #10 Sieve	25.4%
Sand	44.2%
Clay	26.0%
Silt	29.8%
Db g/cc	

We trust this provides the information required at this time. Should you have further questions, please call.

Regards,

RGH GEOTECHNICAL

Sean Flinn Laboratory Technician





NO SCALE

Rombauer Vineyards 3522 Silverado Trail St. Helena, CA 94574 APN 021-410-025 Job No. 96-07 November 2018 Sheet 1 of 2





TEST PIT LOCATION MAP

SCALE: |" = 40'

TEST PIT EXPLORATION NOTES:

I. 🖶 REPRESENTS TEST PIT LOCATION.

2. TEST PITS TP-I THRU TP-II WERE EXCAVATED BY TAYLOR BAILEY CONSTRUCTION ON NOVEMBER 8, 2018 AND WITNESSED BY A REPRESENTATIVE FROM BARTELT ENGINEERING AND NAPA COUNTY ENVIRONMENTAL HEALTH.

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Rombauer Vineyards 3522 Silverado Trail St. Helena, CA 94574 APN 021-410-025 Job No. 96-07 November 2018 Sheet 2 of 2

