# ZINFANDEL LANE / SILVERADO TRAIL INTERSECTION TRAFFIC ANALYSIS 

UPDATED TRAFFIC STUDY FOR THE PROPOSED
RAYMOND VINEYARDS WINERY
USE PERMIT MODIFICATION \#P11-00156

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# ZINFANDEL LANE / SILVERADO TRAIL INTERSECTION TRAFFIC ANALYSIS 

## RAYMOND VINEYARDS WINERY USE PERMIT MODIFICATION \#P11-00156

## INTRODUCTION / SUMMARY

Traffic conditions were evaluated at the Zinfandel Lane/Silverado Trail intersection for the proposed Raymond Winery use permit modification (P11-00156). This analysis supplements the traffic study which was conducted for the proposed use permit modification (Updated Traffic Study for the Proposed Raymond Vineyards Winery Use Permit Modification P11-00156, April 5, 2013) which evaluated two other intersections. The originally proposed use permit modification evaluated in the report (and subsequently the current smaller request) would not result in a significant impact based on the County standards of significance (with the provision that a left turn lane would be installed on Zinfandel Lane at the project access intersection.)

This analysis of the Zinfandel Lane/Silverado Trail intersection found that the original proposed use permit would add vehicular traffic above "without project" conditions, but within the standards of significance based on the County standards. The eastbound Zinfandel Lane approach operates at LOS ‘ $F$ ’ for existing, near term, and long term scenarios without the project and would continue to do so with the project with eastbound vehicle queues increasing by one to two vehicle during the peak hours. The northbound Silverado Trail left turn movement would operate at LOS 'A’-‘B' conditions, with slight increases in delays. The original permit request was calculated to add 14-26 peak hour trips above existing volumes to the intersection. The current proposal is calculated to add 10-18 peak hour trips to the Zinfandel Lane/Silverado Trail intersection.

## SETTING

A traffic study prepared for the Castellucci Winery located at the east end of Zinfandel Lane evaluated the Zinfandel Lane/Silverado Trail intersection. ${ }^{1}$ The traffic volumes from that study were utilized for the "without project" conditions of this analysis. The Raymond Winery proposed use permit volumes were added to the Castellucci report volumes to evaluate "with project" conditions. In order to remain consistent with the traffic report conducted for the Raymond Winery, this analysis has evaluated the original proposed use permit modification (consisting of 500 daily visitors, 90 employees, and average annual wine production of $1,500,000$ gallons). The use permit modification has been reduced and no longer includes changes to the current use permit visitation level ( 400 daily visitors) and no change in production levels ( 900,000 peak annual gallons). Therefore, the current use modification request would generate fewer vehicle trips and all of the findings of this analysis address conditions associated with the current proposal's reduced size.

Silverado Trail is a two lane through route oriented in a north-south direction along the eastern side of the Napa Valley. In the project vicinity it consists of 12 -foot travel lanes with striped shoulder areas marked as Class 2 bicycle lanes. The posted speed limit is 55 mph near Zinfandel Lane.

Zinfandel Lane east of the Raymond Winery to Silverado Trail consists of two twelve foot wide lanes with $1-4$ foot wide striped shoulder areas. It is flat and straight until curving at the Napa River 700 west of Silverado Trail where there is a bridge (approximately 100 feet long) with narrower 9 -foot travel lanes then continues straight to Zinfandel Lane. The posted speed limit is 45 mph with yellow warning 35 mph speed limit signs through the curved segment.

[^0]The Zinfandel Lane/Silverado Trail intersection has a single lane approach on Zinfandel Lane which is stop sign controlled. Northbound Silverado Trail has a separate left turn lane pocket on the approach to the intersection. A private driveway is located on the east side of the intersection.

## Napa County Significance Criteria

The County of Napa's significance criteria has been based on a review of the Napa County Transportation \& Planning Agency and Napa County General Plan documentation on roadway and intersection operations. Specifically, the Circulation Element of the County's General Plan outlines the following significance criteria specific to operations:

- The County shall seek to maintain an arterial Level of Service D or better on all county roadways, except where maintaining this desired level of service would require the installation of more travel lanes than shown on the Circulation Map.
- The County shall seek to maintain a Level of Service D or better at all signalized intersections, except where the level of service already exceeds this standard (i.e. Level of Service E or F) and where increased intersection capacity is not feasible without substantial additional right-of-way.
- No single level of service standard is appropriate for un-signalized intersections, which shall be evaluated on a case-by-case basis to determine if signal warrants are met.

Further significance criteria are based on County and CEQA guidelines and apply mainly to intersection operation and access. A significant impact occurs if project traffic would result in the following:

- Cause an increase in traffic which is substantial in relation to existing traffic load and capacity of the street system (i.e. result in a substantial increase in either the number of vehicle trips, the volume capacity ratio on roads, or congestion at intersections);
- Exceed either individually or cumulatively, an LOS standard established by the county congestion management agency for designated roads or highways;
- Result in a change of traffic patterns, including either an increase in traffic levels or a change in location that results in substantial safety risks;
- Substantially increase hazards due to a design feature (e.g. sharp curves or dangerous intersections) or incompatible uses (e.g. farm equipment);
- Result in inadequate emergency vehicle access;
- Project site or internal circulation on the site is not adequate to accommodate pedestrians and bicycles.


## EXISTING TRAFFIC CONDITIONS

The Castellucci report conducted peak hour counts at the Zinfandel Lane/Silverado Trail intersection in June 2013 and daily volume counts on Zinfandel Lane in August, 2013. The Castellucci Winery report found daily volumes on Zinfandel Lane near Silverado Trail averaged 3,512 vehicles. Volume data for Silverado Trail available from Napa County identifies volumes north and south of Zinfandel Lane are equal to ten times the peak hour volumes. Applied to the 2013 intersection counts results in 15,150 two-way weekday average daily trips north of Zinfandel Lane and 15,650 daily trips to the south. Weekend volumes equate to 13,710 daily trips to the north and 14,020 trips to the south of Zinfandel Lane. The average daily volumes on Silverado Trail are equivalent to LOS 'D' conditions (13,800-22,300 ADT) based on Napa County LOS volume thresholds.

The calculated peak hour intersection levels of service are provided in Table 1. The Zinfandel Lane/Silverado Trail intersection has calculated existing peak hour operating conditions of LOS ' $F$ ' (delays in excess of 50 seconds) for the eastbound Zinfandel Lane approach during the weekday and Saturday peak hours. The Silverado Trail northbound left turn movement operates at LOS ‘A’-'B' (9.4-10.7 seconds delay) during peak hours.

## NEAR TERM TRAFFIC CONDITIONS

For the Near Term conditions, the "Year 2018 With Castellucci Project" volumes from the Castellucci report were used. The volumes are based on traffic model projections from the Napa County General Plan and reflect an eight percent increase from existing volumes. Future lane geometries and controls at the Zinfandel Lane/Silverado Trail intersection were unchanged from existing conditions. (However, a left turn lane on eastbound Zinfandel Lane is proposed at the Castellucci Winery access.)

Silverado Trail would be expected to have daily volumes of 16,360-16,900 weekday trips and 13,250-13,260 Saturday daily trips. The volumes would continue to reflect LOS ' $D$ ' conditions based on the volume thresholds.

The Zinfandel Lane/Silverado Trail intersection would continue to operate at LOS ' F ' for the eastbound Zinfandel Lane approach and the northbound left turn movement would continue to operate at LOS 'A'-'B' (9.6-11.3 seconds of delay) during the weekday and Saturday peak hours.

## Signalization Warrants

The volumes were compared with the California Manual on Uniform Traffic Control Devices "peak hour" signal warrants. The peak hour volume warrant is one of several warrants available to determine if installation of a traffic signal may be appropriate. The Zinfandel Lane/Silverado Trail intersection would qualify for signalization under existing, near term, and long term Year 2030 cumulative "without project" conditions. With signalization, the intersection would operate at LOS ‘B' or better during all evaluated timeframes.

## TRAFFIC CONDITIONS WITH PROPOSED USE PERMIT

The total winery trips with the original proposed use permit as calculated in the Raymond Winery traffic report were distributed with $30 \%$ to/from the east on Zinfandel Lane to Silverado Trail. The project trips at the Zinfandel Lane/Silverado Trail intersection were distributed in proportion to the background turning volumes. For weekdays, this resulted in $40 \%$ of the trips to/from the north and $60 \%$ to/from the south on Silverado Trail, while the Saturday distribution resulted in $50 \%$ of the trips equally to the north and to the south.

With the originally proposed use permit, the project trips would add 33 weekday daily and 74 Saturday daily trips above existing volumes to Zinfandel Lane east of the winery. On Silverado Trail, approximately 13 daily weekday and 37 Saturday daily trips would be added north of Zinfandel Lane and 20 weekday daily and 37 Saturday daily trips would be added south of the intersection. The reduced permit application, which excludes the visitation and production increase components, now represents an increase of 23 weekday daily and 51 Saturday daily volumes on Zinfandel Lane east of the Winery. The revised permit would add approximately 9 weekday and 25 Saturday daily trips on Silverado Trail north of Zinfandel Lane and 14 weekday and 26 Saturday daily trips on Silverado Trail south of the intersection.

The originally proposed permit would add 14 weekday peak hour trips and 26 Saturday peak hour trips to the Zinfandel Lane/Silverado Trail intersection above existing volumes. The revised permit would add 10 weekday and 18 Saturday peak hour trips above existing volumes. The roadway LOS on Silverado Trail would remain unchanged for existing, near term and long term with project conditions, continuing to operate at LOS 'D' conditions. Zinfandel Lane would continue to operate at LOS ' C ' conditions.

The peak hour conditions with the original proposed use permit were evaluated for the Zinfandel Lane/Silverado Trail intersection (level of service conditions are shown in Table 1). The levels of service for "with project" conditions would remain unchanged from "without project" conditions. The eastbound Zinfandel Lane approach would continue to operate at LOS ' $F$ ' with longer delays compared to "without project" conditions and the northbound left turn would operate at LOS 'A'-‘B' with delay increases, if any, of approximately one second compared to "without project" conditions.

The calculated vehicle queues indicate vehicle queues would increase by one to two vehicles at the eastbound Zinfandel Lane approach during Friday and Saturday peak hours. There are no calculated increases in queues for the northbound left turn lane approach on Silverado Trail.

It is noted that the calculated increases are based on the visitation numbers used in the original permit application, but the ratio of surveyed visitation to the current permit level is lower than the levels used for the trip rate calculations, indicating actual volume increases may be less than calculated during typical conditions.

## Signalization Warrants

The volumes were compared with the California Manual on Uniform Traffic Control Devices "peak hour" signal warrants. The peak hour volume warrant is one of several warrants available to determine if installation of a traffic signal may be appropriate. The Zinfandel Lane/Silverado Trail intersection qualifies for signalization for all "without project" conditions and would qualify for signalization under existing, near term, and long term cumulative "with project" conditions. With signalization, the intersection would operate at LOS ' B ' or better during all evaluated periods.

## CUMULATIVE CONDITIONS

The long term cumulative volumes were based on the County's General Plan transportation model forecasts as provided in the Circulation Element for future Year 2030 conditions. The growth projections translated into a 25 percent growth in traffic on Zinfandel Lane and 28 percent growth in traffic on Silverado Trail from the Year 2013 volumes.

The volume projections equate to daily volumes on Silverado Trail of 19,390-20,030 two-way trips to the north and to the south of Zinfandel Lane, respectively. The volumes would continue to equate to LOS 'D' conditions based on the volume thresholds. Conditions would operate at LOS 'C' on Zinfandel Lane.

The cumulative volumes indicate the eastbound approach to the Zinfandel Lane/Silverado Trail intersection would continue to operate at LOS ' $F$ ' with increased delays at peak times of the day and with longer peak periods during the day.

As noted in the Raymond Winery traffic study, the County has identified mitigation policies for potential long term traffic volume increases outlined in the Napa County General Plan. The policies include street network improvements, potential development of a traffic impact fee, and reduction of vehicle trips through alternative transportation and trip reducing policies. As stated in the report, the winery would provide bicycle racks and an electric vehicle charging station. It is our understanding a travel demand management program with trip reduction strategies would be provided to winery employees. If, for example, the measures result in $25 \%$ of employees ridesharing, daily and peak hour trips would be reduced by $20 \%-26 \%$.

Although no significant impacts were found based on the County standards at this intersection, the findings/recommendations in the Raymond Winery traffic analysis would remain applicable; notably the construction of a left turn lane on Zinfandel Lane at the Wheeler Lane project access (proposed for installation as part of the use permit modification) which would mitigate the left turn lane operating conditions at the winery access intersection.

TABLE 1
ZINFANDEL LANE / SILVERADO TRAIL

## EXISTING AND EXISTING + PROJECT PEAK HOUR INTERSECTION OPERATIONS LEVEL OF SERVICE (LOS) AND SECONDS OF DELAY

| Zinfandel Lane / Silverado Trail Unsignalized (minor street stop) | Weekday PM Peak Hour |  | Saturday Afternoon Peak Hour |  |
| :---: | :---: | :---: | :---: | :---: |
|  | $\begin{gathered} \text { Existing } \\ \text { LOS Delay } \\ \hline \end{gathered}$ | $\begin{gathered} \hline \text { Existing + } \\ \text { Project } \\ \text { LOS Delay } \\ \hline \end{gathered}$ | $\begin{gathered} \text { Existing } \\ \text { LOS Delay } \\ \hline \end{gathered}$ | $\begin{gathered} \text { Existing + } \\ \text { Project } \\ \text { LOS Delay } \\ \hline \end{gathered}$ |
| Zinfandel Lane eastbound approach | F >50" | F > 50" | F > 50, | F > 50, |
| Silverado Trail northbound approach | B 10.7" | B 10.7" | A 9.4" | A 9.5" |
| Silverado Trail southbound approach | A <1" | A <1, | A <1" | A <1" |

EXISTING AND EXISTING + CURRENT USE PERMIT PEAK HOUR INTERSECTION OPERATIONS LEVEL OF SERVICE (LOS) AND SECONDS OF DELAY

| Zinfandel Lane / Silverado Trail Unsignalized (minor street stop) | Weekday PM Peak Hour |  | Saturday Afternoon Peak Hour |  |
| :---: | :---: | :---: | :---: | :---: |
|  | Existing <br> LOS Delay | Existing + Current Use Permit LOS Delay | Existing <br> LOS Delay | Existing + Current Use Permit LOS Delay |
| Zinfandel Lane eastbound approach | F >50" | F > 50" | F >50" | F >50" |
| Silverado Trail northbound approach | B 10.7" | B 10.7" | A 9.4" | A 9.4" |
| Silverado Trail southbound approach | A <1" | A <1, | A <1" | A <1" |

## NEAR TERM AND NEAR TERM + PROJECT PEAK HOUR INTERSECTION OPERATIONS LEVEL OF SERVICE (LOS) AND SECONDS OF DELAY

| Zinfandel Lane / Silverado Trail Unsignalized (minor street stop) | Weekday PM Peak Hour |  | Saturday Afternoon Peak Hour |  |
| :---: | :---: | :---: | :---: | :---: |
|  | Near Term <br> LOS Delay | Near Term + Project LOS Delay | Near Term <br> LOS Delay | Near Term + Project LOS Delay |
| Zinfandel Lane eastbound approach Silverado Trail northbound approach Silverado Trail southbound approach | $\begin{array}{cc} \mathrm{F} & >50 " \\ \mathrm{~B} & 11.3 " \\ \mathrm{~A} & <1 " \end{array}$ | $\begin{array}{lr} \mathrm{F} & >50 " \prime \\ \mathrm{~B} & 11.3^{\prime \prime} \\ \mathrm{A} & <1 \end{array}$ | $\begin{array}{lr} \mathrm{F} & >50 \prime \prime \\ \mathrm{~A} & 9.6^{\prime \prime} \\ \mathrm{A} & <1^{\prime \prime} \end{array}$ | $\begin{array}{cc} \mathrm{F} & >50 " \\ \mathrm{~A} & 9.7 \prime \prime \\ \mathrm{~A} & <1 " \end{array}$ |

Based on Highway Capacity Manual (HCM) 2000, Operations methodology for stop-sign controlled (unsignalized) intersections using Synchro-Simtraffic software. Intersection calculation yields an LOS and vehicle delay in seconds.

## APPENDIX

Zinfandel Lane/Silverado Trail Traffic Analysis Raymond Vineyards Winery Use Permit Modification \# P11-00156

- Level of Service Definitions
- Level of Service Calculations
- Peak Hour Signal Warrants

TABLE A-1
LEVEL-OF-SERVICE CRITERIA FOR INTERSECTIONS

| LEVEL OF SERVICE | Type of Flow | Delay | Maneuverability | Control Delay (SECONDS/VEHICLE) |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Signalized | UnSIGNALIZED | All-Way Stop |
| A | Stable Flow | Very slight delay. Progression is very favorable, with most vehicles arriving during the green phase not stopping at all. | Turning movements are easily made, and nearly all drivers find freedom of operation. | $\begin{gathered} \leq 10.0 \text { secs. } \\ \leq 0.60 \mathrm{v} / \mathrm{c} \end{gathered}$ | $\leq 10.0$ | $\leq 10.0$ |
| B | Stable Flow | Good progression and/or short cycle lengths. More vehicles stop than for LOS A, causing higher levels of average delay. | Vehicle platoons are formed. Many drivers begin to feel somewhat restricted $\dagger$ within groups of vehicles. | $\begin{aligned} & >10 \text { and } \leq 20.0 \\ & \text { secs. } \\ & 0.61-0.70 \mathrm{v} / \mathrm{c} \end{aligned}$ | $>10$ and $\leq 15.0$ | $>10$ and $\leq 15.0$ |
| C | Stable Flow | Higher delays resulting from fair progression and/or longer cycle lengths. Individual cycle failures may begin to appear at this level. The number of vehicles stopping is significant, although many still pass through the intersection without stopping. | Back-ups may develop behind turning vehicles. Most drivers feel somewhat restricted | $\begin{aligned} & >20 \text { and } \leq 35.0 \\ & \text { secs. } \\ & 0.71-0.80 \mathrm{v} / \mathrm{c} \end{aligned}$ | $>15$ and $\leq 25.0$ | >15 and $\leq 25.0$ |
| D | Approaching Unstable Flow | The influence of congestion becomes more noticeable. Longer delays may result from some combination of unfavorable progression, long cycle lengths, or high volume-to-capacity ratios. Many vehicles stop, and the proportion of vehicles of stopping declines. Individual cycle failures are noticeable. | Maneuverability is severely limited during short periods due to temporary back-ups. | $\begin{aligned} & >35 \text { and } \leq 55.0 \\ & \text { secs. } \\ & 0.81-0.90 \mathrm{v} / \mathrm{c} \end{aligned}$ | $>25$ and $\leq 35.0$ | >25 and $\leq 35.0$ |
| E | Unstable Flow | Generally considered to be the limit of acceptable delay. Indicative of poor progression, long cycle lengths, and high volume-to-capacity ratios. Individual cycle failures are frequent occurrences. | There are typically long queues of vehicles waiting upstream of the intersection. | $\begin{aligned} & >55 \text { and } \leq 80.0 \\ & \text { secs. } \\ & 0.91-1.00 \mathrm{v} / \mathrm{c} \end{aligned}$ | $>35$ and $\leq 50.0$ | >35 and $\leq 50.0$ |
| F | Forced Flow | Generally considered to be unacceptable to most drivers. Often occurs with over saturation. May also occur at high volume-to-capacity ratios. There are many individual cycle failures. Poor progression and long cycle lengths may also be major contributing factors. | Jammed conditions. Back-ups from other locations restrict or prevent movement. Volumes may vary widely, depending principally on the downstream back-up conditions. | $\begin{aligned} & >80.0 \text { secs. } \\ & >1.00 \mathrm{v} / \mathrm{c} \end{aligned}$ | > 50.0 | > 50.0 |

References: 1. Highway Capacity Manual, Fourth Edition, Transportation Research Board, 2000, Contra Costa Transportation Authority (CCTA), Technical Procedures Update, Final, July 9, 2006. For the purposes of this study, CCTA intersection methodology has been used for signalized intersections yielding an LOS and v/c ratio.

|  | $\rangle$ |  |  |  |  |  | 4 | $\dagger$ | P |  | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | \$ |  |  | ¢ |  | \% | $\hat{F}$ |  |  | ${ }_{*}$ |  |
| Sign Control |  | Stop |  |  | Stop |  |  | Free |  |  | Free |  |
| Grade |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Volume (veh/h) | 84 | 1 | 130 | 0 | 0 | 1 | 50 | 578 | 0 | 1 | 916 | 42 |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 1.00 | 0.95 | 0.95 |
| Hourly flow rate (vph) | 88 | 1 | 137 | 0 | 0 | 1 | 53 | 608 | 0 | 1 | 964 | 44 |
| Pedestrians |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Width (ft) |  |  |  |  |  |  |  |  |  |  |  |  |
| Walking Speed (ft/s) |  |  |  |  |  |  |  |  |  |  |  |  |
| Percent Blockage |  |  |  |  |  |  |  |  |  |  |  |  |
| Right turn flare (veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Median type |  | None |  |  | None |  |  |  |  |  |  |  |
| Median storage veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Upstream signal (ft) |  |  |  |  |  |  |  |  |  |  |  |  |
| pX, platoon unblocked |  |  |  |  |  |  |  |  |  |  |  |  |
| vC , conflicting volume | 1703 | 1702 | 986 | 1839 | 1724 | 608 | 1008 |  |  | 608 |  |  |
| $\mathrm{vC1}$, stage 1 conf vol |  |  |  |  |  |  |  |  |  |  |  |  |
| $\mathrm{vC2}$, stage 2 conf vol |  |  |  |  |  |  |  |  |  |  |  |  |
| vCu, unblocked vol | 1703 | 1702 | 986 | 1839 | 1724 | 608 | 1008 |  |  | 608 |  |  |
| tC, single (s) | 7.1 | 6.5 | 6.2 | 7.1 | 6.5 | 6.2 | 4.1 |  |  | 4.1 |  |  |
| $\mathrm{tC}, 2$ stage (s) |  |  |  |  |  |  |  |  |  |  |  |  |
| tF (s) | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 | 2.2 |  |  | 2.2 |  |  |
| p0 queue free \% | 0 | 99 | 54 | 100 | 100 | 100 | 92 |  |  | 100 |  |  |
| cM capacity (veh/h) | 67 | 85 | 301 | 29 | 82 | 495 | 687 |  |  | 970 |  |  |
| Direction, Lane \# | EB 1 | WB 1 | NB 1 | NB 2 | SB 1 |  |  |  |  |  |  |  |
| Volume Total | 226 | 1 | 53 | 608 | 1009 |  |  |  |  |  |  |  |
| Volume Left | 88 | 0 | 53 | 0 | 1 |  |  |  |  |  |  |  |
| Volume Right | 137 | 1 | 0 | 0 | 44 |  |  |  |  |  |  |  |
| cSH | 127 | 495 | 687 | 1700 | 970 |  |  |  |  |  |  |  |
| Volume to Capacity | 1.78 | 0.00 | 0.08 | 0.36 | 0.00 |  |  |  |  |  |  |  |
| Queue Length 95th (ft) | 433 | 0 | 6 | 0 | 0 |  |  |  |  |  |  |  |
| Control Delay (s) | 442.1 | 12.3 | 10.7 | 0.0 | 0.0 |  |  |  |  |  |  |  |
| Lane LOS | F | B | B |  | A |  |  |  |  |  |  |  |
| Approach Delay (s) | 442.1 | 12.3 | 0.8 |  | 0.0 |  |  |  |  |  |  |  |
| Approach LOS | F | B |  |  |  |  |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 53.0 |  |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 77.6\% | ICU Level of Service |  |  |  |  | D |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |  |


|  | $\rangle$ |  |  |  |  |  | 4 | 4 | 7 |  | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | \$ |  |  | \$ |  | 7 | $\uparrow$ |  |  | $\uparrow$ |  |
| Sign Control |  | Stop |  |  | Stop |  |  | Free |  |  | Free |  |
| Grade |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Volume (veh/h) | 97 | 1 | 83 | 2 | 0 | 0 | 76 | 559 | 1 | 0 | 605 | 54 |
| Peak Hour Factor | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 |
| Hourly flow rate (vph) | 103 | 1 | 88 | 2 | 0 | 0 | 81 | 595 | 1 | 0 | 644 | 57 |
| Pedestrians |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Width (ft) |  |  |  |  |  |  |  |  |  |  |  |  |
| Walking Speed (ft/s) |  |  |  |  |  |  |  |  |  |  |  |  |
| Percent Blockage |  |  |  |  |  |  |  |  |  |  |  |  |
| Right turn flare (veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Median type |  | None |  |  | None |  |  |  |  |  |  |  |
| Median storage veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Upstream signal (ft) |  |  |  |  |  |  |  |  |  |  |  |  |
| pX, platoon unblocked |  |  |  |  |  |  |  |  |  |  |  |  |
| vC , conflicting volume | 1429 | 1430 | 672 | 1518 | 1458 | 595 | 701 |  |  | 596 |  |  |
| vC1, stage 1 conf vol |  |  |  |  |  |  |  |  |  |  |  |  |
| vC2, stage 2 conf vol |  |  |  |  |  |  |  |  |  |  |  |  |
| vCu, unblocked vol | 1429 | 1430 | 672 | 1518 | 1458 | 595 | 701 |  |  | 596 |  |  |
| tC, single (s) | 7.1 | 6.5 | 6.2 | 7.1 | 6.5 | 6.2 | 4.1 |  |  | 4.1 |  |  |
| tC, 2 stage (s) |  |  |  |  |  |  |  |  |  |  |  |  |
| tF (s) | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 | 2.2 |  |  | 2.2 |  |  |
| p0 queue free \% | 1 | 99 | 81 | 97 | 100 | 100 | 91 |  |  | 100 |  |  |
| cM capacity (veh/h) | 105 | 122 | 456 | 73 | 118 | 504 | 896 |  |  | 981 |  |  |
| Direction, Lane \# | EB 1 | WB 1 | NB 1 | NB 2 | SB 1 |  |  |  |  |  |  |  |
| Volume Total | 193 | 2 | 81 | 596 | 701 |  |  |  |  |  |  |  |
| Volume Left | 103 | 2 | 81 | 0 | 0 |  |  |  |  |  |  |  |
| Volume Right | 88 | 0 | 0 | 1 | 57 |  |  |  |  |  |  |  |
| cSH | 162 | 73 | 896 | 1700 | 981 |  |  |  |  |  |  |  |
| Volume to Capacity | 1.19 | 0.03 | 0.09 | 0.35 | 0.00 |  |  |  |  |  |  |  |
| Queue Length 95th (ft) | 265 | 2 | 7 | 0 | 0 |  |  |  |  |  |  |  |
| Control Delay (s) | 186.2 | 56.0 | 9.4 | 0.0 | 0.0 |  |  |  |  |  |  |  |
| Lane LOS | F | F | A |  |  |  |  |  |  |  |  |  |
| Approach Delay (s) | 186.2 | 56.0 | 1.1 |  | 0.0 |  |  |  |  |  |  |  |
| Approach LOS | F | F |  |  |  |  |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 23.4 |  |  |  |  |  |  |  |  |  |
| Intersection Capacity U | ilization |  | 79.2\% | ICU Level of Service |  |  |  |  | D |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |  |










| Both 1 Lane Approaches |  | 2 or more Lane and One Lane Approaches |  | Both 2 or more Lane Approaches |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Major Street Total of Both Approaches | Minor Street High Volume Approach | Major Street Total of Both Approaches | Minor Street High Volume Approach | Major Street Total of Both Approaches | Minor Street High Volume Approach |
| 370 | 280 |  |  |  |  |
| 400 | 270 | 460 | 297 | 430 | 410 |
| 500 | 215 | 500 | 290 | 500 | 380 |
| 600 | 185 | 600 | 230 | 600 | 310 |
| 700 | 140 | 700 | 198 | 700 | 265 |
| 800 | 115 | 800 | 170 | 800 | 210 |
| 900 | 99 | 900 | 125 | 900 | 180 |
| 1000 | 85 | 1000 | 105 | 1000 | 140 |
| 1100 | 75 | 1100 | 90 | 1100 | 110 |
| 1200 | 75 | 1200 | 75 | 1150 | 100 |
| 1300 | 75 | 1300 | 75 | 1300 | 100 |

* Note: Values in Table are approximate, actual curves based upon 2nd order polynomial equation

$\star$ NOTE:
100 VPH APPLIES AS THE LOWER THRESHOLD VOLUME FOR MINOR STREET APPROACH WITH TWO OR MORE LANES AND 75 VPH APPLIES AS THE LOWER THRESHOLD VOLUME FOR A MINOR STREET APPROACHING WITH ONE LANE.

Intersection:
Scenario:
Minor St. Volume:
Major St. Volume:
Warrant Met?:

Silverado Trail / Zinfandel Lane
Existing Weekday Peak Hour Conditions
215
1587
Yes

| Both 1 Lane Approaches |  | 2 or more Lane and One Lane Approaches |  | Both 2 or more Lane Approaches |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Major Street Total of Both Approaches | Minor Street High Volume Approach | Major Street Total of Both Approaches | Minor Street High Volume Approach | Major Street Total of Both Approaches | Minor Street High Volume Approach |
| 370 | 280 |  |  |  |  |
| 400 | 270 | 460 | 297 | 430 | 410 |
| 500 | 215 | 500 | 290 | 500 | 380 |
| 600 | 185 | 600 | 230 | 600 | 310 |
| 700 | 140 | 700 | 198 | 700 | 265 |
| 800 | 115 | 800 | 170 | 800 | 210 |
| 900 | 99 | 900 | 125 | 900 | 180 |
| 1000 | 85 | 1000 | 105 | 1000 | 140 |
| 1100 | 75 | 1100 | 90 | 1100 | 110 |
| 1200 | 75 | 1200 | 75 | 1150 | 100 |
| 1300 | 75 | 1300 | 75 | 1300 | 100 |

* Note: Values in Table are approximate, actual curves based upon 2nd order polynomial equation


3 NOTE:
100 VPH APPLIES AS THE LOWER THRESHOLD VOLUME FOR MINOR STREET APPROACH WITH TWO OR MORE LANES AND 75 VPH APPLIES AS THE LOWER THRESHOLD VOLUME FOR A MINOR STREET APPROACHING WITH ONE LANE.

Intersection:
Scenario:
Minor St. Volume:
Major St. Volume:
Warrant Met?:

Silverado Trail / Zinfandel Lane
Existing Saturday Peak Hour Conditions 181
1295
Yes

| Both 1 Lane Approaches |  | 2 or more Lane and One Lane Approaches |  | Both 2 or more Lane Approaches           <br> Major Street Total of <br> Both Approaches           <br> Minor Street High <br> Volume Approach       Major Street Total of <br> Both Approaches Minor Street High <br> Volume Approach Major Street Total of <br> Both Approaches Volume Approach <br> 370          $\quad 280$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: |

* Note: Values in Table are approximate, actual curves based upon 2nd order polynomial equation

$\star$ NOTE:
100 VPH APPLIES AS THE LOWER THRESHOLD VOLUME FOR MINOR STREET APPROACH WITH TWO OR MORE LANES AND 75 VPH APPLIES AS THE LOWER THRESHOLD VOLUME FOR A MINOR STREET APPROACHING WITH ONE LANE.

Intersection:
Scenario:
Minor St. Volume:
Major St. Volume:
Warrant Met?:

Silverado Trail / Zinfandel Lane
Existing With Current Use Permit Weekday Peak Hour Conditions
218
1588
Yes

| Both 1 Lane Approaches |  | 2 or more Lane and One Lane Approaches |  | Both 2 or more Lane Approaches |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Major Street Total of Both Approaches | Minor Street High Volume Approach | Major Street Total of Both Approaches | Minor Street High Volume Approach | Major Street Total of Both Approaches | Minor Street High Volume Approach |
| 370 | 280 |  |  |  |  |
| 400 | 270 | 460 | 297 | 430 | 410 |
| 500 | 215 | 500 | 290 | 500 | 380 |
| 600 | 185 | 600 | 230 | 600 | 310 |
| 700 | 140 | 700 | 198 | 700 | 265 |
| 800 | 115 | 800 | 170 | 800 | 210 |
| 900 | 99 | 900 | 125 | 900 | 180 |
| 1000 | 85 | 1000 | 105 | 1000 | 140 |
| 1100 | 75 | 1100 | 90 | 1100 | 110 |
| 1200 | 75 | 1200 | 75 | 1150 | 100 |
| 1300 | 75 | 1300 | 75 | 1300 | 100 |

* Note: Values in Table are approximate, actual curves based upon 2nd order polynomial equation


3 NOTE:
100 VPH APPLIES AS THE LOWER THRESHOLD VOLUME FOR MINOR STREET APPROACH WITH TWO OR MORE LANES AND 75 VPH APPLIES AS THE LOWER THRESHOLD VOLUME FOR A MINOR STREET APPROACHING WITH ONE LANE.

Intersection:
Scenario:
Minor St. Volume:
Major St. Volume:
Warrant Met?:

Silverado Trail / Zinfandel Lane
Existing With Current Use Permit Saturday Peak Hour Conditions 193
1301
Yes

| Both 1 Lane Approaches |  | 2 or more Lane and One Lane Approaches |  | Both 2 or more Lane Approaches |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Major Street Total of Both Approaches | Minor Street High Volume Approach | Major Street Total of Both Approaches | Minor Street High Volume Approach | Major Street Total of Both Approaches | Minor Street High Volume Approach |
| 370 | 280 |  |  |  |  |
| 400 | 270 | 460 | 297 | 430 | 410 |
| 500 | 215 | 500 | 290 | 500 | 380 |
| 600 | 185 | 600 | 230 | 600 | 310 |
| 700 | 140 | 700 | 198 | 700 | 265 |
| 800 | 115 | 800 | 170 | 800 | 210 |
| 900 | 99 | 900 | 125 | 900 | 180 |
| 1000 | 85 | 1000 | 105 | 1000 | 140 |
| 1100 | 75 | 1100 | 90 | 1100 | 110 |
| 1200 | 75 | 1200 | 75 | 1150 | 100 |
| 1300 | 75 | 1300 | 75 | 1300 | 100 |

* Note: Values in Table are approximate, actual curves based upon 2nd order polynomial equation


3 NOTE:
100 VPH APPLIES AS THE LOWER THRESHOLD VOLUME FOR MINOR STREET APPROACH WITH TWO OR MORE LANES AND 75 VPH APPLIES AS THE LOWER THRESHOLD VOLUME FOR A MINOR STREET APPROACHING WITH ONE LANE.

Intersection:
Scenario:
Minor St. Volume:
Major St. Volume:
Warrant Met?:

Silverado Trail / Zinfandel Lane
Existing Plus Project Weekday Peak Hour Conditions
226
1590
Yes

| Both 1 Lane Approaches |  | 2 or more Lane and One Lane Approaches |  | Both 2 or more Lane Approaches           <br> Major Street Total of <br> Both Approaches           <br> Minor Street High <br> Volume Approach       Major Street Total of <br> Both Approaches Minor Street High <br> Volume Approach Major Street Total of <br> Both Approaches Volume Approach <br> 370          $\quad 280$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: |

* Note: Values in Table are approximate, actual curves based upon 2nd order polynomial equation

$\star$ NOTE:
100 VPH APPLIES AS THE LOWER THRESHOLD VOLUME FOR MINOR STREET APPROACH WITH TWO OR MORE LANES AND 75 VPH APPLIES AS THE LOWER THRESHOLD VOLUME FOR A MINOR STREET APPROACHING WITH ONE LANE.

Intersection:
Scenario:
Minor St. Volume:
Major St. Volume:
Warrant Met?:

Silverado Trail / Zinfandel Lane
Existing Plus Project Saturday Peak Hour Conditions 198
1304
Yes

| Both 1 Lane Approaches |  | 2 or more Lane and One Lane Approaches |  | Both 2 or more Lane Approaches |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Major Street Total of Both Approaches | Minor Street High Volume Approach | Major Street Total of Both Approaches | Minor Street High Volume Approach | Major Street Total of Both Approaches | Minor Street High Volume Approach |
| 370 | 280 |  |  |  |  |
| 400 | 270 | 460 | 297 | 430 | 410 |
| 500 | 215 | 500 | 290 | 500 | 380 |
| 600 | 185 | 600 | 230 | 600 | 310 |
| 700 | 140 | 700 | 198 | 700 | 265 |
| 800 | 115 | 800 | 170 | 800 | 210 |
| 900 | 99 | 900 | 125 | 900 | 180 |
| 1000 | 85 | 1000 | 105 | 1000 | 140 |
| 1100 | 75 | 1100 | 90 | 1100 | 110 |
| 1200 | 75 | 1200 | 75 | 1150 | 100 |
| 1300 | 75 | 1300 | 75 | 1300 | 100 |

* Note: Values in Table are approximate, actual curves based upon 2nd order polynomial equation


3 NOTE:
100 VPH APPLIES AS THE LOWER THRESHOLD VOLUME FOR MINOR STREET APPROACH WITH TWO OR MORE LANES AND 75 VPH APPLIES AS THE LOWER THRESHOLD VOLUME FOR A MINOR STREET APPROACHING WITH ONE LANE.

Intersection:
Scenario:
Minor St. Volume:
Major St. Volume:
Warrant Met?:

Silverado Trail / Zinfandel Lane
Near Term (Existing + Approved Developments) Weekday Peak Hour Conditions 225
1713
Yes

| Both 1 Lane Approaches |  | 2 or more Lane and One Lane Approaches |  | Both 2 or more Lane Approaches |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Major Street Total of Both Approaches | Minor Street High Volume Approach | Major Street Total of Both Approaches | Minor Street High Volume Approach | Major Street Total of Both Approaches | Minor Street High Volume Approach |
| 370 | 280 |  |  |  |  |
| 400 | 270 | 460 | 297 | 430 | 410 |
| 500 | 215 | 500 | 290 | 500 | 380 |
| 600 | 185 | 600 | 230 | 600 | 310 |
| 700 | 140 | 700 | 198 | 700 | 265 |
| 800 | 115 | 800 | 170 | 800 | 210 |
| 900 | 99 | 900 | 125 | 900 | 180 |
| 1000 | 85 | 1000 | 105 | 1000 | 140 |
| 1100 | 75 | 1100 | 90 | 1100 | 110 |
| 1200 | 75 | 1200 | 75 | 1150 | 100 |
| 1300 | 75 | 1300 | 75 | 1300 | 100 |

* Note: Values in Table are approximate, actual curves based upon 2nd order polynomial equation

$\star$ NOTE:
100 VPH APPLIES AS THE LOWER THRESHOLD VOLUME FOR MINOR STREET APPROACH WITH TWO OR MORE LANES AND 75 VPH APPLIES AS THE LOWER THRESHOLD VOLUME FOR A MINOR STREET APPROACHING WITH ONE LANE.

Intersection:
Scenario:
Minor St. Volume:
Major St. Volume:
Warrant Met?:

Silverado Trail / Zinfandel Lane
Near Term (Existing + Approved Developments) Saturday Peak Hour Conditions 181
1397
Yes

| Both 1 Lane Approaches |  | 2 or more Lane and One Lane Approaches |  | Both 2 or more Lane Approaches |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Major Street Total of Both Approaches | Minor Street High Volume Approach | Major Street Total of Both Approaches | Minor Street High Volume Approach | Major Street Total of Both Approaches | Minor Street High Volume Approach |
| 370 | 280 |  |  |  |  |
| 400 | 270 | 460 | 297 | 430 | 410 |
| 500 | 215 | 500 | 290 | 500 | 380 |
| 600 | 185 | 600 | 230 | 600 | 310 |
| 700 | 140 | 700 | 198 | 700 | 265 |
| 800 | 115 | 800 | 170 | 800 | 210 |
| 900 | 99 | 900 | 125 | 900 | 180 |
| 1000 | 85 | 1000 | 105 | 1000 | 140 |
| 1100 | 75 | 1100 | 90 | 1100 | 110 |
| 1200 | 75 | 1200 | 75 | 1150 | 100 |
| 1300 | 75 | 1300 | 75 | 1300 | 100 |

* Note: Values in Table are approximate, actual curves based upon 2nd order polynomial equation

$\star$ NOTE:
100 VPH APPLIES AS THE LOWER THRESHOLD VOLUME FOR MINOR STREET APPROACH WITH TWO OR MORE LANES AND 75 VPH APPLIES AS THE LOWER THRESHOLD VOLUME FOR A MINOR STREET APPROACHING WITH ONE LANE.

Intersection:
Scenario:
Minor St. Volume:
Major St. Volume:
Warrant Met?:

Silverado Trail / Zinfandel Lane
Near Term (Existing + Approved Developments) Plus Project Weekday Peak Hour Conditions 236
1716
Yes

| Both 1 Lane Approaches |  | 2 or more Lane and One Lane Approaches |  | Both 2 or more Lane Approaches |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Major Street Total of Both Approaches | Minor Street High Volume Approach | Major Street Total of Both Approaches | Minor Street High Volume Approach | Major Street Total of Both Approaches | Minor Street High Volume Approach |
| 370 | 280 |  |  |  |  |
| 400 | 270 | 460 | 297 | 430 | 410 |
| 500 | 215 | 500 | 290 | 500 | 380 |
| 600 | 185 | 600 | 230 | 600 | 310 |
| 700 | 140 | 700 | 198 | 700 | 265 |
| 800 | 115 | 800 | 170 | 800 | 210 |
| 900 | 99 | 900 | 125 | 900 | 180 |
| 1000 | 85 | 1000 | 105 | 1000 | 140 |
| 1100 | 75 | 1100 | 90 | 1100 | 110 |
| 1200 | 75 | 1200 | 75 | 1150 | 100 |
| 1300 | 75 | 1300 | 75 | 1300 | 100 |

* Note: Values in Table are approximate, actual curves based upon 2nd order polynomial equation


4 NOTE:
100 VPH APPLIES AS THE LOWER THRESHOLD VOLUME FOR MINOR STREET APPROACH WITH TWO OR MORE LANES AND 75 VPH APPLIES AS THE LOWER THRESHOLD VOLUME FOR A MINOR STREET APPROACHING WITH ONE LANE.

| Intersection: | Silverado Trail / Zinfandel Lane |
| :--- | :--- |
| Scenario: | Near Term (Existing + Approved Developments) Plus Project Saturday Peak Hour Conditions |
| Minor St. Volume: | 198 |
| Major St. Volume: | 1406 |
| Warrant Met?: | Yes |




Analysis Period (min)
15
c Critical Lane Group

|  | $\stackrel{ }{*}$ |  |  |  |  |  | 4 | $\dagger$ | 7 |  | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | $\uparrow$ |  |  | $\uparrow$ |  | \% | F |  |  | $\uparrow$ |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) |  | 4.0 |  |  | 4.0 |  | 4.0 | 4.0 |  |  | 4.0 |  |
| Lane Util. Factor |  | 1.00 |  |  | 1.00 |  | 1.00 | 1.00 |  |  | 1.00 |  |
| Frpb, ped/bikes |  | 0.98 |  |  | 0.97 |  | 1.00 | 1.00 |  |  | 1.00 |  |
| Flpb, ped/bikes |  | 1.00 |  |  | 1.00 |  | 1.00 | 1.00 |  |  | 1.00 |  |
| Frt |  | 0.92 |  |  | 0.86 |  | 1.00 | 1.00 |  |  | 0.99 |  |
| Flt Protected |  | 0.98 |  |  | 1.00 |  | 0.95 | 1.00 |  |  | 1.00 |  |
| Satd. Flow (prot) |  | 1634 |  |  | 1562 |  | 1770 | 1863 |  |  | 1850 |  |
| Flt Permitted |  | 0.87 |  |  | 1.00 |  | 0.29 | 1.00 |  |  | 1.00 |  |
| Satd. Flow (perm) |  | 1453 |  |  | 1562 |  | 537 | 1863 |  |  | 1849 |  |
| Volume (vph) | 85 | 1 | 132 | 0 | 0 | 1 | 50 | 578 | 0 | 1 | 916 | 43 |
| Peak-hour factor, PHF | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 1.00 | 0.95 | 0.95 |
| Adj. Flow (vph) | 89 | 1 | 139 | 0 | 0 | 1 | 53 | 608 | 0 | 1 | 964 | 45 |
| RTOR Reduction (vph) | 0 | 104 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 2 | 0 |
| Lane Group Flow (vph) | 0 | 125 | 0 | 0 | 0 | 0 | 53 | 608 | 0 | 0 | 1008 | 0 |
| Confl. Bikes (\#/hr) |  |  | 5 |  |  | 5 |  |  | 5 |  |  | 5 |
| Heavy Vehicles (\%) | 4\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% |
| Turn Type | Perm |  |  | Perm |  |  | Perm |  |  | Perm |  |  |
| Protected Phases |  | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |  |
| Actuated Green, G (s) |  | 9.9 |  |  | 9.9 |  | 38.4 | 38.4 |  |  | 38.4 |  |
| Effective Green, g (s) |  | 9.9 |  |  | 9.9 |  | 38.4 | 38.4 |  |  | 38.4 |  |
| Actuated g/C Ratio |  | 0.18 |  |  | 0.18 |  | 0.68 | 0.68 |  |  | 0.68 |  |
| Clearance Time (s) |  | 4.0 |  |  | 4.0 |  | 4.0 | 4.0 |  |  | 4.0 |  |
| Vehicle Extension (s) |  | 3.0 |  |  | 3.0 |  | 3.0 | 3.0 |  |  | 3.0 |  |
| Lane Grp Cap (vph) |  | 256 |  |  | 275 |  | 366 | 1271 |  |  | 1261 |  |
| v/s Ratio Prot |  |  |  |  | 0.00 |  |  | 0.33 |  |  |  |  |
| v/s Ratio Perm |  | c0.09 |  |  |  |  | 0.10 |  |  |  | c0.54 |  |
| v/c Ratio |  | 0.49 |  |  | 0.00 |  | 0.14 | 0.48 |  |  | 0.80 |  |
| Uniform Delay, d1 |  | 20.9 |  |  | 19.1 |  | 3.2 | 4.2 |  |  | 6.3 |  |
| Progression Factor |  | 1.00 |  |  | 1.00 |  | 1.00 | 1.00 |  |  | 1.00 |  |
| Incremental Delay, d2 |  | 1.5 |  |  | 0.0 |  | 0.2 | 0.3 |  |  | 3.6 |  |
| Delay (s) |  | 22.4 |  |  | 19.1 |  | 3.3 | 4.5 |  |  | 9.9 |  |
| Level of Service |  | C |  |  | B |  | A | A |  |  | A |  |
| Approach Delay (s) |  | 22.4 |  |  | 19.1 |  |  | 4.4 |  |  | 9.9 |  |
| Approach LOS |  | C |  |  | B |  |  | A |  |  | A |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM Average Control Delay |  |  | 9.5 |  | HCM Le | el of S | rvice |  | A |  |  |  |
| HCM Volume to Capacity ratio |  |  | 0.74 |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length (s) |  |  | 56.3 |  | Sum of | st time |  |  | 8.0 |  |  |  |
| Intersection Capacity Utilization |  |  | 77.8\% |  | ICU Lev | of Ser | vice |  | D |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |  |
| c Critical Lane Group |  |  |  |  |  |  |  |  |  |  |  |  |



Analysis Period (min)
15
c Critical Lane Group

|  | $\stackrel{ }{*}$ |  |  |  |  |  | 4 | $\dagger$ | 7 |  | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | $\uparrow$ |  |  | $\uparrow$ |  | \% | F |  |  | ¢ |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) |  | 4.0 |  |  | 4.0 |  | 4.0 | 4.0 |  |  | 4.0 |  |
| Lane Util. Factor |  | 1.00 |  |  | 1.00 |  | 1.00 | 1.00 |  |  | 1.00 |  |
| Frpb, ped/bikes |  | 0.98 |  |  | 0.97 |  | 1.00 | 1.00 |  |  | 1.00 |  |
| Flpb, ped/bikes |  | 1.00 |  |  | 1.00 |  | 1.00 | 1.00 |  |  | 1.00 |  |
| Frt |  | 0.92 |  |  | 0.86 |  | 1.00 | 1.00 |  |  | 0.99 |  |
| Flt Protected |  | 0.98 |  |  | 1.00 |  | 0.95 | 1.00 |  |  | 1.00 |  |
| Satd. Flow (prot) |  | 1635 |  |  | 1563 |  | 1770 | 1863 |  |  | 1849 |  |
| Flt Permitted |  | 0.87 |  |  | 1.00 |  | 0.29 | 1.00 |  |  | 1.00 |  |
| Satd. Flow (perm) |  | 1453 |  |  | 1563 |  | 534 | 1863 |  |  | 1849 |  |
| Volume (vph) | 88 | 1 | 137 | 0 | 0 | 1 | 51 | 578 | 0 | 1 | 916 | 44 |
| Peak-hour factor, PHF | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 1.00 | 0.95 | 0.95 |
| Adj. Flow (vph) | 93 | 1 | 144 | 0 | 0 | 1 | 54 | 608 | 0 | 1 | 964 | 46 |
| RTOR Reduction (vph) | 0 | 102 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 2 | 0 |
| Lane Group Flow (vph) | 0 | 136 | 0 | 0 | 0 | 0 | 54 | 608 | 0 | 0 | 1009 | 0 |
| Confl. Bikes (\#/hr) |  |  | 5 |  |  | 5 |  |  | 5 |  |  | 5 |
| Heavy Vehicles (\%) | 4\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% |
| Turn Type | Perm |  |  | Perm |  |  | Perm |  |  | Perm |  |  |
| Protected Phases |  | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |  |
| Actuated Green, G (s) |  | 10.1 |  |  | 10.1 |  | 37.8 | 37.8 |  |  | 37.8 |  |
| Effective Green, g (s) |  | 10.1 |  |  | 10.1 |  | 37.8 | 37.8 |  |  | 37.8 |  |
| Actuated g/C Ratio |  | 0.18 |  |  | 0.18 |  | 0.68 | 0.68 |  |  | 0.68 |  |
| Clearance Time (s) |  | 4.0 |  |  | 4.0 |  | 4.0 | 4.0 |  |  | 4.0 |  |
| Vehicle Extension (s) |  | 3.0 |  |  | 3.0 |  | 3.0 | 3.0 |  |  | 3.0 |  |
| Lane Grp Cap (vph) |  | 263 |  |  | 282 |  | 361 | 1260 |  |  | 1250 |  |
| v/s Ratio Prot |  |  |  |  | 0.00 |  |  | 0.33 |  |  |  |  |
| v/s Ratio Perm |  | c0.09 |  |  |  |  | 0.10 |  |  |  | 0.55 |  |
| v/c Ratio |  | 0.52 |  |  | 0.00 |  | 0.15 | 0.48 |  |  | 0.81 |  |
| Uniform Delay, d1 |  | 20.7 |  |  | 18.8 |  | 3.3 | 4.3 |  |  | 6.5 |  |
| Progression Factor |  | 1.00 |  |  | 1.00 |  | 1.00 | 1.00 |  |  | 1.00 |  |
| Incremental Delay, d2 |  | 1.7 |  |  | 0.0 |  | 0.2 | 0.3 |  |  | 3.9 |  |
| Delay (s) |  | 22.4 |  |  | 18.8 |  | 3.5 | 4.6 |  |  | 10.4 |  |
| Level of Service |  | C |  |  | B |  | A | A |  |  | B |  |
| Approach Delay (s) |  | 22.4 |  |  | 18.8 |  |  | 4.5 |  |  | 10.4 |  |
| Approach LOS |  | C |  |  | B |  |  | A |  |  | B |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM Average Control Delay |  |  | 9.9 |  | HCM Le | el of S | rvice |  | A |  |  |  |
| HCM Volume to Capacity ratio |  |  | 0.75 |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length (s) |  |  | 55.9 |  | Sum of | st time |  |  | 8.0 |  |  |  |
| Intersection Capacity Utilization |  |  | 78.4\% |  | ICU Lev | of Ser | vice |  | D |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |  |
| c Critical Lane Group |  |  |  |  |  |  |  |  |  |  |  |  |



Analysis Period (min) 15
c Critical Lane Group

|  | 4 | $\rightarrow$ |  | $\checkmark$ |  |  | 4 | $\dagger$ | $p$ |  | $\dagger$ | $\pm$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | $\uparrow$ |  |  | \& |  | ${ }^{7}$ | $\uparrow$ |  |  | $\dagger$ |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) |  | 4.0 |  |  | 4.0 |  | 4.0 | 4.0 |  |  | 4.0 |  |
| Lane Util. Factor |  | 1.00 |  |  | 1.00 |  | 1.00 | 1.00 |  |  | 1.00 |  |
| Frpb, ped/bikes |  | 0.98 |  |  | 0.97 |  | 1.00 | 1.00 |  |  | 1.00 |  |
| Flpb, ped/bikes |  | 1.00 |  |  | 1.00 |  | 1.00 | 1.00 |  |  | 1.00 |  |
| Frt |  | 0.92 |  |  | 0.86 |  | 1.00 | 1.00 |  |  | 0.99 |  |
| Flt Protected |  | 0.98 |  |  | 1.00 |  | 0.95 | 1.00 |  |  | 1.00 |  |
| Satd. Flow (prot) |  | 1634 |  |  | 1562 |  | 1770 | 1863 |  |  | 1851 |  |
| Flt Permitted |  | 0.87 |  |  | 1.00 |  | 0.26 | 1.00 |  |  | 1.00 |  |
| Satd. Flow (perm) |  | 1452 |  |  | 1562 |  | 481 | 1863 |  |  | 1851 |  |
| Volume (vph) | 88 | 1 | 136 | 0 | 0 | 1 | 52 | 586 | 0 | 1 | 1031 | 43 |
| Peak-hour factor, PHF | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 |
| Adj. Flow (vph) | 92 | 1 | 142 | 0 | 0 | 1 | 54 | 610 | 0 | 1 | 1074 | 45 |
| RTOR Reduction (vph) | 0 | 85 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 2 | 0 |
| Lane Group Flow (vph) | 0 | 150 | 0 | 0 | 0 | 0 | 54 | 610 | 0 | 0 | 1118 | 0 |
| Confl. Bikes (\#/hr) |  |  | 5 |  |  | 5 |  |  | 5 |  |  | 5 |
| Heavy Vehicles (\%) | 4\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% |
| Turn Type | Perm |  |  | Perm |  |  | Perm |  |  | Perm |  |  |
| Protected Phases |  | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |  |
| Actuated Green, G (s) |  | 11.0 |  |  | 11.0 |  | 45.5 | 45.5 |  |  | 45.5 |  |
| Effective Green, g (s) |  | 11.0 |  |  | 11.0 |  | 45.5 | 45.5 |  |  | 45.5 |  |
| Actuated g/C Ratio |  | 0.17 |  |  | 0.17 |  | 0.71 | 0.71 |  |  | 0.71 |  |
| Clearance Time (s) |  | 4.0 |  |  | 4.0 |  | 4.0 | 4.0 |  |  | 4.0 |  |
| Vehicle Extension (s) |  | 3.0 |  |  | 3.0 |  | 3.0 | 3.0 |  |  | 3.0 |  |
| Lane Grp Cap (vph) |  | 248 |  |  | 266 |  | 339 | 1314 |  |  | 1306 |  |
| v/s Ratio Prot |  |  |  |  | 0.00 |  |  | 0.33 |  |  |  |  |
| v/s Ratio Perm |  | c0.10 |  |  |  |  | 0.11 |  |  |  | 0.60 |  |
| v/c Ratio |  | 0.61 |  |  | 0.00 |  | 0.16 | 0.46 |  |  | 0.86 |  |
| Uniform Delay, d1 |  | 24.7 |  |  | 22.2 |  | 3.2 | 4.2 |  |  | 7.1 |  |
| Progression Factor |  | 1.00 |  |  | 1.00 |  | 1.00 | 1.00 |  |  | 1.00 |  |
| Incremental Delay, d2 |  | 4.2 |  |  | 0.0 |  | 0.2 | 0.3 |  |  | 5.7 |  |
| Delay (s) |  | 28.9 |  |  | 22.2 |  | 3.4 | 4.4 |  |  | 12.8 |  |
| Level of Service |  | C |  |  | C |  | A | A |  |  | B |  |
| Approach Delay (s) |  | 28.9 |  |  | 22.2 |  |  | 4.3 |  |  | 12.8 |  |
| Approach LOS |  | C |  |  | C |  |  | A |  |  | B |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM Average Control Delay |  |  | 11.9 |  | HCM Lev | el of S | rvice |  | B |  |  |  |
| HCM Volume to Capacity ratio |  |  | 0.81 |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length (s) |  |  | 64.5 |  | Sum of los | st time |  |  | 8.0 |  |  |  |
| Intersection Capacity Utilization |  |  | 84.3\% |  | ICU Leve | l of Se | vice |  | E |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |  |
| c Critical Lane Group |  |  |  |  |  |  |  |  |  |  |  |  |



Analysis Period (min) 15
c Critical Lane Group

HCM Signalized Intersection Capacity Analysis 3: Zinfandel Lane \& Silverado Trail

Existing + Approved Dvipmnts. + Project Signalized Weekday PM Peak Hour



Analysis Period (min) 15
c Critical Lane Group


[^0]:    ${ }^{1}$ Crane Transportation Group, Traffic Impact Report for Proposed Castellucci Family Winery, November 2013.
    Updated Traffic Study for Raymond Winery
    Use Permit Modification \#P11-00156

