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## Wastewater Feasibility Study

WASTEWATER FEASIBILITY  
STUDY

BOYD FAMILY VINEYARDS

4042 Big Ranch, Napa, California  
APN 036-190-003



CIVIL STRUCTURAL ELECTRICAL WATER|WASTEWATER

Project No. 2017120  
October 20, 2017

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## LIST OF ENCLOSURES

- Enclosure A:     Vicinity Map  
                  Overall Site Plan (UP2)  
                  Wastewater Site Plan (UP4)  
                  Wastewater System Schematic
- Enclosure B:     Sanitary Sewage Flow Estimates  
                  Process Wastewater Flow Estimates  
                  PD & Subsurface Drip Disposal Field Sizing  
                  Irrigation Holding Tank Sizing  
                  Irrigation Balance  
                  Climate Data
- Enclosure C:     Site Evaluation Data

## **PROJECT OVERVIEW**

Boyd Family Vineyards is applying for a Use Permit for the Boyd Family Vineyards new winery facility to be located at 4042 Big Ranch Road, in Napa (APN: 036-190-003). The project site is located approximately 0.3 miles southwest of the Napa River, and 1.7 miles northeast of Highway 29/128. The project site extends over a gently sloping terrain along the valley floor, sloping northeast at approximately 3% or less towards the Napa River.

Boyd Family Vineyards is made up of a single 20.88 acre parcel, with approximately 13.68 acres of existing vineyard. The parcel has an existing residence with a guest cottage and garage, a barn, a shed, and a well pump house with a water supply tank. The Use Permit Application includes the construction of a new 4,200 square foot winery with a production capacity of 30,000 gallons per year. The new winery will require 2 full-time employees, with 6 full-time employees during crush and marketing events, and anticipates 15 maximum visitors per day with an average of 40 visitors per week. The existing sanitary sewer leach field system will continue to be used for disposal of the sewer from the existing residence and guest house on the site. Summit Engineering has prepared the following Wastewater Feasibility Study outlining the process wastewater (PW) and sanitary sewage (SS) flows from the proposed winery and the associated treatment and disposal systems.

## **WINERY PROCESS WASTEWATER MANAGEMENT SYSTEM**

To accommodate a proposed annual production of 30,000 gallons of wine, the new PW management system will include a gravity collection system with screens on floor drains for solids removal, a PW pump station, and treatment and disposal through one of the following alternatives:

1. PW Hold and Haul, with SS disposal through a pressure distribution (PD) leachfield.
2. Primary treatment and disposal through a PD leachfield (combined with SS).
3. Treatment through package treatment system and in-ground disposal via a subsurface drip dispersal system (combined or not with SS).
4. Treatment through a high rate package treatment system, storage of treated PW, and surface reuse for vineyard irrigation.

The PW management system will be designed and installed in accordance with the memorandum of understanding and all necessary Napa County Planning, Building and Environmental Services (PBES) and Regional Water Quality Control Board (RWQCB) criteria and permits.

## **PROCESS WASTEWATER CHARACTERISTICS**

Process wastewater will consist primarily of wastewater collected at floor drains and trenches within the winery, receiving, crush, tank, and wash down areas. All exterior tank and process areas will be covered and graded to preclude stormwater from entering the PW collection system. No distillation will occur at the facility; hence there will be no stillage waste. Typical winery wastewater characteristics are as summarized below:

**PROCESS WASTEWATER DESIGN FLOWS**

Based on typical flow data from wineries of similar size and characteristics and corresponding process wastewater (PW) generation rates, projected flows are calculated as follows:

**Annual Volume**

Annual Production	=	30,000 gal wine/year
Generation Rate (assumed) <sup>a</sup>	=	165 gal wine/ton grapes
Tons Crushed	=	181 tons grapes/year
Process Wastewater (PW) Generation Rate <sup>b</sup>	=	6.00 gal PW/gal wine
Annual PW Flow	=	<u>180,000 gal PW/year</u>

**Average Day Flow** = **493 gal PW/day**

**Napa County Peak Day Flow**

Peak Harvest Day Flow (45 day harvest) = **1,000 gal PW/day**

**Average, Day Peak Harvest Month Flow**

The harvest month of September accounts for approximately 16.4 percent of the annual PW flow.

Peak Flow	=	<u>984 gal PW/day</u>
	=	<b><u>1,000 gal PW/day</u></b>

Notes:

- a. 165 Gal wine per ton of grapes is used as a wine industry standard
- b. 6.0 gal of PW per gallon wine produced over the course of 1 year is based on the average of data from approximately 16 wineries

The PW design flow will account for the most conservative approach; therefore 1,000 gpd will be used for preliminary system sizing as outlined below.

## DISPOSAL METHODS

A Hold & Haul system will be utilized for disposal of PW, eliminating the need for vineyard removal associated with a PD system and 12" of fill. As a backup option, either a PD disposal system or a pre-treatment system will be utilized for treatment and disposal of PW, as presented in the following options.

### **OPTION 2: PD DISPOSAL SYSTEM**

The PD system sized for disposal of PW in combination with SS flows would require a total area of 18,200 square feet. The system would require 2,900 LF of leachline, spaced 6.5 feet on center and with 12" of fill. An additional 200% reserve area is designated as a subsurface drip dispersal field, see Enclosure A.

$$\text{PD Leach Field Size} = \frac{1,315 \text{ gpd}^a}{1.33 \frac{\text{SF}}{\text{LF}} \times \frac{0.35 \text{ gal}}{\text{SF} \times \text{day}}} = 2,825 \text{ LF minimum}$$

<sup>a</sup> The total flow accounts for 350 gpd of SS and 1,000 gpd of PW

A total of 28 – 100 foot pressure distribution lines will provide a total of 2,900 lineal feet. With trench spacing at 6.5 feet on-center, a total of 18,200 SF of leachfield area for disposal of combined SS and PW flows. A 200% reserve area will be provided for via a subsurface drip system, sized accordingly to the system type as shown in Option 3. Reduced sizing requirements for an SS only PD disposal system can be found in the Sanitary Sewage Treatment and Disposal section, page 11.

## SETTLING TANKS WITH EFFLUENT FILTER

Solids settling and digestion in the settling tanks helps to reduce BOD and TSS concentrations entering the disposal system or pre-treatment system, resulting in higher treatment unit performance, and reduced potential for clogging of the disposal field. An effluent filter will also be provided to remove additional suspended solids which do not settle out in the settling tank. The required settling tank size for the PW flows was evaluated based on Napa County PBES criteria, which requires 3 days min of settling capacity.

$$\begin{aligned} \text{Volume} &= 3 \text{ HRT} \times \text{Flow rate} \\ \text{Volume} &= 3 (1,000 \text{ gpd}) \\ \underline{\text{Volume}} &= \underline{3,000 \text{ gallons}} \end{aligned}$$

A new 3,000 gallon precast concrete settling tank will be provided to remove solids and reduce BOD loads to the system.

## pH CONTROL SYSTEM

A pH control system could be provided (if necessary) for neutralization of the winery PW, with dosing of neutralizing chemicals into the sump. The combination of naturally occurring alkalinity in source water and alkaline cleaning compounds used within wineries usually provides sufficient buffering to maintain pond pH above 6.5. Neutralizing chemicals should only be used when absolutely necessary. It is recommended that the

and a minimum 200% reserve area of 10,600 square feet (to accommodate both options of PW and SS flows combined, or PW flows only). Warning signs and/or fencing will be installed to indicate the boundaries of the drip field area. See Enclosure B for more details on the subsurface drip disposal field design.

***OPTION 4: PACKAGE TREATMENT SYSTEM WITH SURFACE REUSE/DISPOSAL (PW ONLY)***

**PACKAGE TREATMENT SYSTEM**

A package treatment plant would be provided with the following additional items as discussed in Option 3.

**EFFLUENT STORAGE TANK**

An effluent storage tank shall be sized to accommodate approximately 15 days of storage during the winter months, to account for a prolonged rain event, when irrigation with treated PW effluent is prohibited.

**FLOW MEASUREMENT**

An additional flow measurement device will be provided to measure the discharge flows to the irrigation system.

**FILTER**

A filter will be provided to screen secondary effluent prior to irrigation.

**IRRIGATION DISPOSAL AREA**

The proposed vineyard and landscape areas should provide adequate capacity for reuse and disposal (through percolation) of PW effluent from the package treatment plant. Reuse/disposal of effluent will be via drip irrigation of approximately 1 acre of vineyard/landscape. The irrigation demand of the vineyards and landscaping exceeds the estimated annual process wastewater volume. To meet the additional irrigation demand the treated PW can be supplemented with well water. The irrigation demand is the lowest during the wet weather season (November through April) and application rates during this period should be less than 1 inch per month. An air gap or separate plumbing will be installed for the existing irrigation system plumbing to prevent cross-contamination with treated effluent applied to the irrigation distribution network. See Enclosure D for the PW irrigation balance.

**SANITARY SEWAGE CHARACTERISTICS**

SS will consist primarily of wastewater generated from restrooms, laboratories, and tasting room facilities. Typical SS characteristics are summarized below:

**TABLE 2. TYPICAL SANITARY SEWER CHARACTERISTICS**

<u>Characteristic</u>	<u>Units</u>	<u>Raw Wastewater<sup>1</sup> Range</u>
BOD <sub>5</sub>	mg/L	110 - 220
Grease	mg/L	50-100
Total Suspended Solids (TSS)	mg/L	100 - 220
Volatile Suspended Solids	mg/L	80 - 165
Total Dissolved Solids (TDS)	mg/L	250 - 500
Nitrogen	mg/L	20 - 40
Nitrate	mg/L	0
Phosphorous	mg/L	4 - 8
Alkalinity (CaCO <sub>3</sub> )	mg/L	50 - 100
Chloride	mg/L	30 - 50
Sulfate	mg/L	20 - 30

<sup>1</sup>Typical composition of untreated domestic wastewater, Metcalf & Eddy, "Wastewater Engineering, Third Edition", 1991

Uniform Plumbing Code Method:

$$Volume = 1,125 + 0.75 \times Flow Rate$$

$$Volume = 1,125 + 0.75 \times 315 \text{ gpd}$$

$$Volume = 1,362 \text{ gallons}$$

A 1,500 gallon precast concrete septic tank will be provided for solids removal prior to in-ground disposal of SS flows.

**OPTION 1: PD DISPOSAL SYSTEM (SS ONLY)**

PD DISPOSAL SYSTEM - SS

The PD system sized for disposal of the SS flows would require a total area of 4,550 square feet based on the soils evaluation information previously noted (See Calculations below). An additional 200% reserve area is designated as a subsurface drip dispersal system for combined PW and SS flows, see Enclosure A.

$$PD \text{ Leach Field Size} = \frac{350 \text{ gpd}^a}{1.33 \frac{SF}{LF} \times \frac{0.35 \text{ gal}}{SF \times \text{day}}} = 752 \text{ LF minimum}$$

<sup>a</sup> The total flow accounts for 350 gpd of SS

A total of 7 – 100 foot pressure distribution lines will provide a total of 800 lineal feet. With trench spacing at 6.5 feet on-center, a total of 4,550 SF of leach field area for disposal of SS flows will be provided. 12 inches of fill will be required over all lines.

**OPTION 2: PD DISPOSAL SYSTEM (SS & PW)**

PD DISPOSAL SYSTEM - SS & PW

The PD system sized for disposal of the SS in combination with PW flows would require a total area of 18,200 square feet (See Option 1 of PW management system). An additional 200% reserve area is designated as a subsurface drip dispersal system for combined PW and SS flows, see Enclosure A.

**OPTION 3: PACKAGE TREATMENT PLANT SYSTEM WITH SUB-SURFACE DRIP DISPOSAL**

See Option 3 of PW Management System for combined treatment and sub-surface drip disposal details.

**OTHER CONSIDERATIONS**

**ODOR CONTROL**

There should be no noxious odors from a properly designed and operated treatment system. See Alternative Courses of Action for operation alternatives.

**ENCLOSURE A**

**VICINITY MAP**

**OVERALL SITE PLAN**

**WASTEWATER SITE PLAN**

**WASTEWATER SYSTEM SCHEMATIC**



**BOYD FAMILY VINEYARDS**  
**4042 BIG RANCH ROAD**  
**NAPA, CA 94558**  
**APN 036-190-003**  
**USE PERMIT ASSISTANCE**

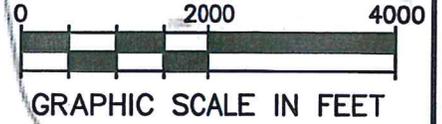
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 DATE 2015-XX-XX1  
 SHT NO. \_\_\_\_\_ OF \_\_\_\_\_  
 BY JA CHK INITIALS2

**PROJECT LOCATION**

**APPROXIMATE PROPERTY LINE, TYP**

**BIG RANCH ROAD**

**APN 036-190-003**



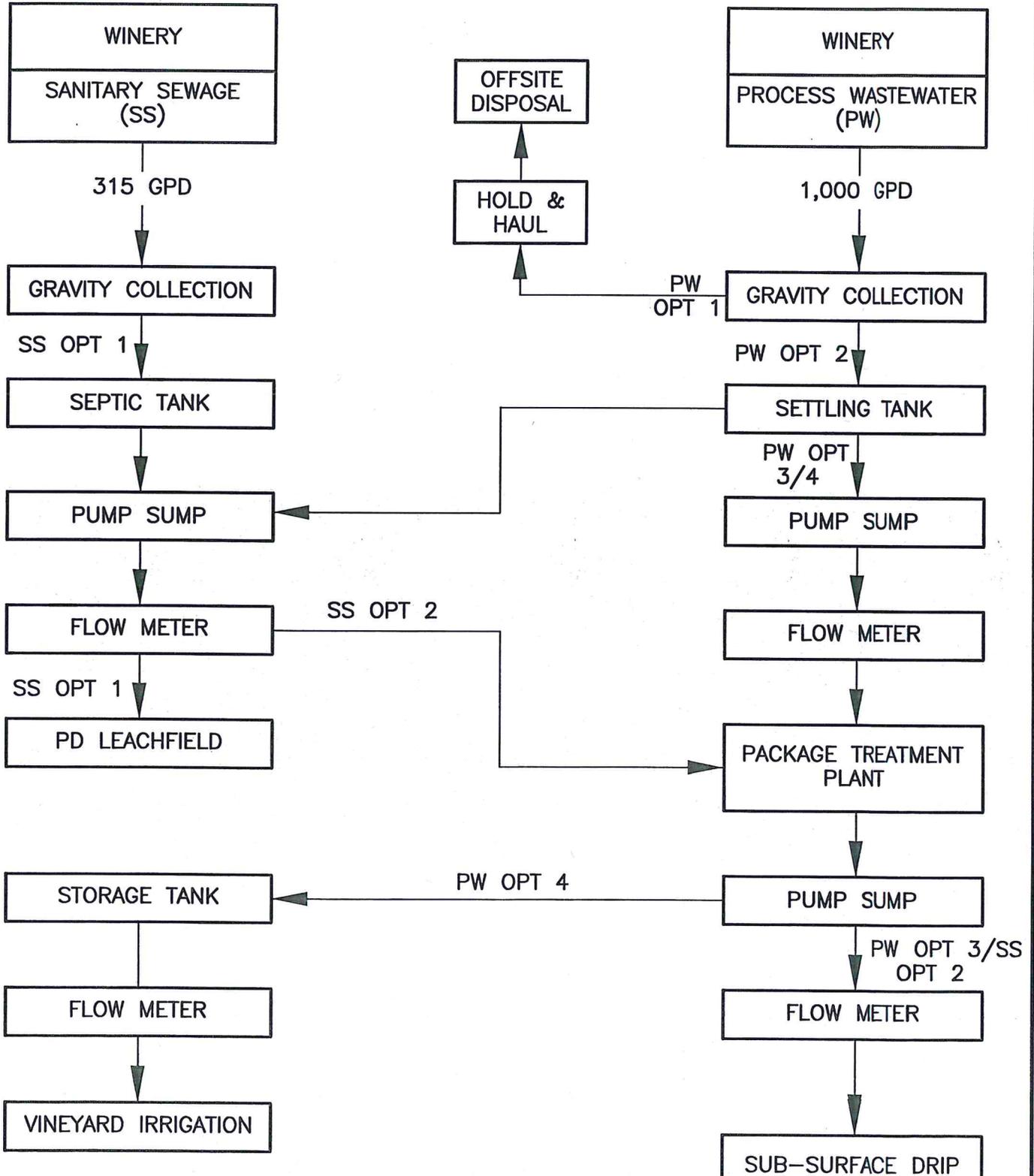
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SUMMIT

BOYD VINEYARDS  
4042 BIG RANCH  
NAPA, CA  
APN 036-190-003

PROJECT NO. 2015148  
DATE 10-09-15  
SHT NO 1 OF 1  
BY CL CHK GG

PW & SS TREATMENT SCHEMATIC



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**ENCLOSURE B**

**SANITARY SEWAGE FLOW ESTIMATES**  
**PROCESS WASTEWATER FLOW ESTIMATES**  
**PD & SUBSURFACE DRIP DISPOSAL FIELD SIZING**  
**IRRIGATION HOLDING TANK SIZING**  
**IRRIGATION BALANCE**  
**CLIMATE DATA**

SUMMIT ENGINEERING, INC.	<p style="text-align: center;">BOYD VINEYARDS Wastewater Feasibility Study Sanitary Sewage Flows Estimate</p>	<p>PROJECT NO. 2015148 BY: CL CHK: JR</p>
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**SANITARY SEWAGE**

Peak Tasting Day Harvest

Employee (full-time)	6 x	15 gpcd	=	90 gal/day
Tasting Visitors	15 x	3 gpcd	=	45 gal/day
Maximum Marketing Visitors	30 x	6 gpcd	=	180 gal/day
<b>Total</b>			<b>=</b>	<b>315 gal/day</b>

Portable toilets will be provided for marketing events resulting in more than 45 total visitors on-site

SUMMIT ENGINEERING, INC.	<p style="text-align: center;">BOYD VINEYARDS Wastewater Feasibility Study Process Wastewater Flows Estimate</p>	<p style="text-align: right;">PROJECT NO. 2015148 BY: CL CHK: JR</p>
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PROCESS WASTEWATER

Annual Volume

Annual Production (projected)		=	12,500 cases wine/year
Generation Rate (assumed) <sup>a</sup>		=	2.4 gal wine/case of wine
Annual Production	12,500 cases wine/year	x	2.4 gal wine/case of wine
		=	30,000 gal wine/year
Generation Rate (assumed) <sup>b</sup>		=	165 gal wine/ton grapes
Tons Crushed	30,000 gal wine/year	÷	165 gal wine/ton grapes
		=	182 tons grapes/year
Process Wastewater (PW) Generation Rate <sup>c</sup> (assumed)		=	6.00 gal PW/gal wine
Annual PW Flow	30,000 gal wine/year	x	6.00 gal PW/gal wine
		=	<u>180,000 gal PW/year</u>

Average Day Flow

$$180,000 \text{ gal PW/year} \div 365 \text{ days} = \underline{493 \text{ gal PW/day}}$$

Napa County Peak Day Flow

Length of Harvest		=	45 days
Peak Flow	$\frac{30,000 \text{ gal wine/year}}{45 \text{ days}}$	x	1.5
		=	<u>1,000 gal PW/day</u>
		=	<u>1,000 gal PW/day</u>

Average, Day Peak Harvest Month Flow

- Assume:
- 1 16.4% of the PW flows are accounted for during September
  - 2 30 days in September

Peak Flow	$\frac{180,000 \text{ gal PW/year}}{30 \text{ days}}$	x	16%	=	<u>984 gal PW/day</u>
				=	<u>1,000 gal PW/day</u>

<p style="text-align: center;">SUMMIT ENGINEERING, INC. Consulting Civil Engineers</p>	<p style="text-align: center;">BOYD VINEYARDS Wastewater Feasibility Study Process Wastewater Flow Estimates</p>	<p>PROJECT NO. 2015148 BY: CL CHK: JR</p>
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**DESIGN CRITERIA**

**FULL PRODUCTION**

Production Level	12,500 cases/year	
Annual Production	30,000 gal wine/year	
Crush Period	45 day	* per PBES criteria
Annual PW Flow	180,000 gal PW/year	
Average PW Flow	493 gal PW/day	
PW Generation Rate	6.0 gal PW/gal wine	
Peak Harvest Day	1,000 gal PW/day	* per PBES criteria
PW Flows accounted during September	16.4 %	
Average Day Peak Harvest Month	1,000 gal PW/day	

**DESIGN PROCESS WASTEWATER FLOWS**

Month	PW Monthly Percentage of Annual Flow <sup>a</sup> (%)	Total PW Flow <sup>a</sup> (Mgal)
August	10.5%	0.019
September	16.4%	0.030
October	12.9%	0.023
November	7.4%	0.013
December	6.4%	0.012
January	6.6%	0.012
February	7.2%	0.013
March	7.6%	0.014
April	6.8%	0.012
May	6.4%	0.012
June	5.6%	0.010
July	6.2%	0.011
<b>Total</b>	<b>100%</b>	<b>0.180</b>

<sup>a</sup> Assumption of monthly percentage of annual flow based on average of PW flow data for similar small wineries

<b>SUMMIT ENGINEERING, INC.</b> Consulting Civil Engineers	<b>BOYD VINEYARDS</b> <b>Wastewater Feasibility Study</b> <b>PD &amp; Subsurface Drip Disposal Field Sizing</b>	<b>PROJECT NO. 2015148</b> BY: CL CHK: JR
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**Option 1: PD System (SS only - Primary)**

Design Flow	=	1,315 gal/day	
Depth to Groundwater or other limit	=	55 inches	Based on TP 1, 2 and 3
Depth of Fill	=	5 inches	
Rock below pipe	=	8 inches	
Sidewall area (orifices up)	=	1.33 sf/lf	
Application	=	0.35 gal/sf/day	Moderate sandy clay per
Lineal Feet required	=	2825 lf	Napa Guidelines (pits
Proposed Lineal Feet installed	=	2900 lf	1,2,3)
Leachline length	=	100 ft	
Trench spacing On-Center	=	6.5 ft	
Primary Area required	=	18,202 square feet	

**Option 2: Subsurface Drip System (PW only or PW & SS comingled - Primary & Reserve)**

Sizing based on Geoflow guidelines			
Design Flow	=	1,315 gal/day	
Depth to Groundwater or other limit	=	36 inches *minimum	
Application	=	0.25 gal/sf/day	Moderate clay & sandy
Square Footage required	=	5,260 sf	clay per Napa County
Primary Area required	=	53 x 100	Guidelines, with
	=	5,300 square feet	pretreatment
200% Reserve Area Required	=	106 x 100	
	=	10,600 square feet	
	=	0.24 acres	
Total Area	=	15,900 square feet	
	=	0.37 acres	

<b>SUMMIT ENGINEERING, INC.</b>	<b>BOYD VINEYARDS</b> Wastewater Feasibility Study PW Effluent Storage Tank Sizing (Option 3)
	PROJECT NO. 2015148 BY: CL CHK: JR

**PW EFFLUENT STORAGE TANK**

Min. Tank Volume = 20,680 gallons  
Tank Volume = 13,535 gallons  
Useable Tank Volume = 12,459 gallons  
Actual Tank Height = 16 ft  
Useable Tank Height = 14 ft  
Tank Diameter = 12 ft  
Inside Diameter = 12.308 ft  
Unit Volume = 846 gal/ft

(Can be split into multiple tanks)  
(provides 15 days of storage at average peak harvest month flows)

Accounting for 2 feet of freeboard  
Based on CST aqua store tank capacities

Month	Initial Volume (gal)	Total Inflow (gal)	Divert Volume <sup>a</sup> (gal)	Final Volume (gal)	Final Depth (ft)
August	0	18,900	18,900	0	0.0
September	0	29,520	29,520	0	0.0
October	0	23,220	23,220	0	0.0
November	0	13,320	7,500	5,820	6.9
December	5,820	11,520	7,500	9,840	11.6
January	9,840	11,880	6,500	15,220	18.0
February	15,220	12,960	7,500	20,680	24.4
March	20,680	13,680	34,360	0	0.0
April	0	12,240	12,240	0	0.0
May	0	11,520	11,520	0	0.0
June	0	10,080	10,080	0	0.0
July	0	11,160	11,160	0	0.0
<b>TOTAL</b>	<b>51,560</b>	<b>180,000</b>	<b>180,000</b>		

<sup>a</sup> Monthly volume of effluent to be used for onsite irrigation or reuse.

SUMMIT ENGINEERING, INC.	BOYD VINEYARDS Wastewater Feasibility Study PW Irrigation Balance	PROJECT NO. BY: CHK:	2015148 CL JR
Applied Irrigation Area	Vineyard	1.00	acres
Total Area Available for Irrigation	Vineyard		acres

Month	Reference ET <sup>a</sup> (in)	Turfgrass Crop Coefficient <sup>b</sup>	Vineyard Crop Coefficient <sup>c</sup>	Turfgrass ET <sup>d</sup> (in)	Vineyard ET <sup>d</sup> (in)	100 year Precipitation <sup>e</sup> (in)	Irrigation Demand <sup>f</sup> (in)	(Mgal)	Operating Days per Month <sup>g</sup> (d)	Percolation Capacity <sup>h</sup> (in)	(Mgal)	Assimilative Capacity <sup>i</sup> (in)	(Mgal)	Effluent Applied <sup>j</sup> (in)	(Mgal)	Excess Capacity (Mgal)
August	6.5	0.9	0.5	5.6	2.9	0.2	2.8	0.075	31	11.46	0.311	14.2	0.386	0.019	0.70	0.37
September	5.1	0.7	0.3	3.8	1.3	0.9	0.4	0.012	30	11.09	0.301	11.5	0.313	0.030	1.09	0.28
October	3.4	0.8	0.1	2.6	0.2	4.0	0.0	0.000	16	5.91	0.161	5.9	0.161	0.023	0.86	0.14
November	1.8	0.7	0.0	1.2	0.0	10.4	0.0	0.000	14	5.17	0.141	5.2	0.141	0.008	0.28	0.13
December	0.9	0.6	0.0	0.6	0.0	11.3	0.0	0.000	5	1.85	0.050	1.8	0.050	0.008	0.28	0.04
January	1.2	0.6	0.0	0.8	0.0	16.1	0.0	0.000	6	2.22	0.060	2.2	0.060	0.007	0.24	0.05
February	1.7	0.6	0.0	1.1	0.0	15.3	0.0	0.000	5	1.85	0.050	1.8	0.050	0.008	0.28	0.04
March	3.4	0.8	0.0	2.6	0.0	11.5	0.0	0.000	12	4.44	0.121	4.4	0.121	0.034	1.27	0.09
April	4.8	1.0	0.2	5.0	0.8	3.8	0.0	0.000	13	4.80	0.131	4.8	0.131	0.012	0.45	0.12
May	6.2	1.0	0.6	5.9	3.6	1.5	2.1	0.058	16	5.91	0.161	8.0	0.218	0.012	0.42	0.21
June	6.9	0.9	0.7	6.1	4.9	0.4	4.5	0.123	17	6.28	0.171	10.8	0.294	0.010	0.37	0.28
July	7.4	0.9	0.6	7.0	4.8	0.1	4.7	0.127	30	11.09	0.301	15.8	0.428	0.011	0.41	0.42
<b>Total</b>	<b>49.4</b>			<b>42.1</b>	<b>18.5</b>	<b>75.4</b>	<b>14.5</b>	<b>0.4</b>	<b>195.0</b>	<b>72.1</b>	<b>2.0</b>	<b>86.6</b>	<b>2.4</b>	<b>0.18</b>	<b>6.6</b>	<b>2.17</b>

- (a) Average monthly reference evapotranspiration rates, see Climate Data Worksheet.
- (b) Kc coefficients for pasture from Table 1, "Landscape Irrigation System Evaluation and Management" - University of California Cooperative Extension, April 2009
- (c) Kc coefficients for vineyards from Table 5-12, Irrigation with Reclaimed Municipal Wastewater - A Guidance Manual, 84-1 wr, SWRCB.
- (d) ET=ET<sub>o</sub> x Kc. A weighted value is determined on the basis of the available irrigated acreage of vineyard and pasture.
- (e) Precipitation, 10-year rainfall event, see Climate Data Worksheet.
- (f) Irrigation Demand = ET-Precipitation, inches. A weighted value is determined on the basis of the available irrigated acreage of vineyard and pasture.
- (g) Number of operating days per month based on estimated irrigation days available based on 24-hr post storm criteria for a 100-year return period. Summit Engineering, NBRID Capacity Study, April 1996.
- (h) Design percolation rate is a maximum of 75 inches per day for the number of operating day per month. Per USDA soil survey, predominant soil type is bale loam. Sizing percolation rate based on clay soils. Pretreated loading rates for non-shrink clay soils adjusted by a 0.04 safety factor to account for typical slow rate land application design methodology.
- (i) Assimilative capacity is the sum of irrigation demand and percolation applied.
- (j) Effluent applied depths exceeding 1 inch/month could result in ponding; if ponding occurs, additional disposal area may be required for expansion

<b>Percolation Adjustment</b>	
Hourly Percolation Rate	0.385 in/hr
Daily Percolation Rate	24 hr/day
Land Application Safety Factor	9.24 in/day
Adjusted Percolation Rate	0.04
	0.37 in/day

<b>SUMMIT ENGINEERING, INC.</b> Consulting Civil Engineers	<b>BOYD VINEYARDS</b> <b>WASTEWATER FEASIBILITY STUDY</b> Climate Data	<b>PROJECT NO.</b> BY: CHK:	2015/48 CL JR
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Month	Days	Average Temp <sup>a</sup> (F)	Reference Evapotranspiration <sup>b</sup> (in)	Pan Evaporation <sup>c</sup> (in)	Lake Evaporation <sup>d</sup> (in)	Average Precipitation <sup>e</sup> (in)	10-Year Precipitation <sup>f</sup> (in)	100-Year Precipitation <sup>f</sup> (in)
August	31	71.0	6.5	12.06	9.3	0.08	0.1	0.2
September	30	68.6	5.1	8.67	6.7	0.41	0.6	0.9
October	31	62.5	3.4	5.72	4.4	1.84	2.8	4.0
November	30	53.4	1.8	2.48	1.9	4.83	7.3	10.4
December	31	47.6	0.9	1.66	1.3	5.22	7.9	11.3
January	31	47.9	1.2	1.53	1.2	7.46	11.3	16.1
February	28	51.4	1.7	2.15	1.7	7.10	10.7	15.3
March	31	54.1	3.4	3.79	2.9	5.31	8.0	11.5
April	30	58.6	4.8	5.82	4.5	1.74	2.6	3.8
May	31	63.6	6.2	8.90	6.9	0.68	1.0	1.5
June	30	68.8	6.9	11.00	8.5	0.17	0.3	0.4
July	31	71.6	7.4	13.22	10.2	0.04	0.1	0.1
<b>Total</b>	<b>365</b>		<b>49.4</b>	<b>77.0</b>	<b>59.3</b>	<b>34.9</b>	<b>52.6</b>	<b>75.4</b>

<sup>a</sup> Average monthly temperature observed between 1931 and 2001 for Saint Helena, Napa, CA from NOAA

<sup>b</sup> Average monthly reference evaporation rates for Zone 8, Inland San Francisco Bay Area, typical rainfall year, CIMIS, DWR, 2001. See [www.itrc.org](http://www.itrc.org).

<sup>c</sup> Average monthly pan evaporation rates observed at Lake Berryessa, between 1957 and 1970. See <http://www.calclim.dri.edu/ccda/comparative/avgpan.html>

<sup>d</sup> Pan evaporation rates adjusted by a factor of 0.77 to determine lake evaporation.

<sup>e</sup> Average monthly rainfall observed between 1931 and 2001 for Saint Helena, Napa, CA from NOAA

<sup>f</sup> Average monthly rainfall adjusted by the ratio of 10-yr and 100-yr wet year return storm identified by Pearsons Log III Distribution (St Helena)

Boyd Family Vineyards  
Wastewater Feasibility Study  
October 23, 2017

SUMMIT ENGINEERING, INC.  
Project No. 2015148

**ENCLOSURE C**

**SITE EVALUATION DATA**

Please attach an 8.5" x 11" plot map showing the locations of all test pits triangulated from permanent landmarks or known property corners. The map must be drawn to scale and include a North arrow, surrounding geographic and topographic features, direction and % slope, distance to drainages, water bodies, potential areas for flooding, unstable landforms, existing or proposed roads, structures, utilities, domestic water supplies, wells, ponds, existing wastewater treatment systems and facilities.

Permit #:	
APN:	030-190-03
(County Use Only) Reviewed by:	Date: 09/29/15

**PLEASE PRINT OR TYPE ALL INFORMATION**

Property Owner Boyd Vineyards	<input type="checkbox"/> New Construction <input checked="" type="checkbox"/> Addition <input type="checkbox"/> Remodel <input type="checkbox"/> Relocation <input type="checkbox"/> Other:
Property Owner Mailing Address 4042 Big Ranch	<input type="checkbox"/> Residential - # of Bedrooms:                      Design Flow :                      gpd
City                                      State                                      Zip Napa                                      CA                                      94558	<input checked="" type="checkbox"/> Commercial – Type: Sanitary Waste: 135 gpd                      Process Waste: 1,461 gpd
Site Address/Location 4042 Big Ranch Napa, CA 94558	<input type="checkbox"/> Other: Sanitary Waste:                      gpd                      Process Waste:                      gpd

**Evaluation Conducted By:**

Company Name Summit Engineering, Inc	Evaluator's Name Claudia Llerandi, E.I.T.	Signature (Civil Engineer, R.E.H.S., Geologist, Soil Scientist)
Mailing Address: 463 Aviation Boulevard, Ste 200		Telephone Number 707-527-0775
City                                      State                                      Zip Santa Rosa                                      CA                                      95403	Date Evaluation Conducted 09/23/15	

<p><b>Primary Area</b></p> <p>Acceptable Soil Depth: 55 in. Test pit #'s: 1, 2, 3</p> <p>Soil Application Rate (gal. /sq. ft. /day): 0.2</p> <p>System Type(s) Recommended: PD leachfield</p> <p>Slope: 1 % Distance to nearest water source: +100 ft.</p> <p>Hydrometer test performed? No <input checked="" type="checkbox"/> Yes <input type="checkbox"/> (attach results)</p> <p>Bulk Density test performed? No <input checked="" type="checkbox"/> Yes <input type="checkbox"/> (attach results)</p> <p>Groundwater Monitoring Performed? No <input checked="" type="checkbox"/> Yes <input type="checkbox"/> (attach results)</p>	<p><b>Expansion Area</b></p> <p>Acceptable Soil Depth: 43 in. Test pit #'s: 4 through 12</p> <p>Soil Application Rate (gal. /sq. ft. /day): 0.25</p> <p>System Type(s) Recommended: Subsurface drip w/pretreatment</p> <p>Slope: 1 % Distance to nearest water source: +100 ft.</p> <p>Hydrometer test performed? No <input checked="" type="checkbox"/> Yes <input type="checkbox"/> (attach results)</p> <p>Bulk Density test performed? No <input checked="" type="checkbox"/> Yes <input type="checkbox"/> (attach results)</p> <p>Groundwater Monitoring Performed? No <input checked="" type="checkbox"/> Yes <input type="checkbox"/> (attach results)</p>
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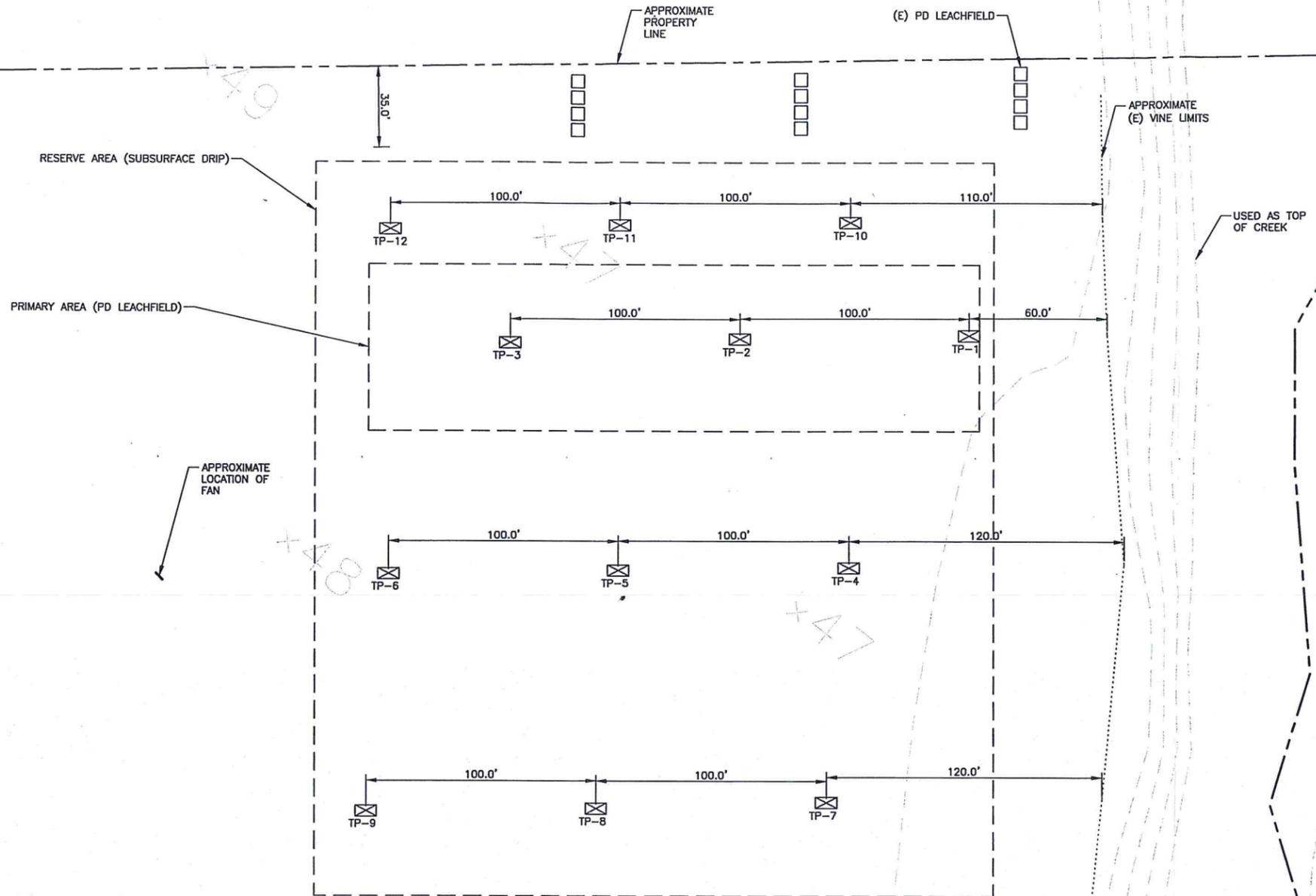
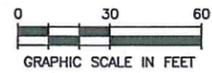
Site constraints/Recommendations:

A pressure distribution system with 12 inches of fill is proposed in the vicinity of test pits #1, 2 and 3 as the primary disposal area. A subsurface drip system with pretreatment is proposed in the vicinity of test pits 4 through 12. Soil was consistent throughout the area evaluated and was found to be clay and sandy clay with moderate texture. No mottling was found in any of the test pits evaluated.

Test Pit #	Horizon Depth (inches)	Boundary	%Rock	Texture	Structure	Consistence			Pores	Roots	Mottling
						Side Wall	Ped	Wet			
1	55		0-5	SC	M,SB	VH	VF	VS,VP	C, F/M	F, F/M	NONE
2	55		0-5	SC	M,SB	VH	VF	VS,VP	C, F/M	F, F/M	NONE
3	50	G	0-5	SC	M,SB	VH	VF	VS,VP	F, F/M	F, F/M	NONE
	70		0-5	SC	S,SB	H	F	P,S	C, F/M	F, F/M	NONE
4	36		0-5	C	W/M,SB	ExH	Ex	VS,VP	F, F/M	F, F/M	NONE
5	48		0-5	SC	M,SB	VH	VF	VS,VP	C, F/M	F, F/M	NONE
6	39		0-5	C	W/M,SB	ExH	Ex	VS,VP	F, F/M	F, F/M	NONE
7	41		0-5	SC	M,SB	VH	VF	P,S	F, F/M	F, F/M	NONE
8	40		0-5	SC	M,SB	VH	VF	VS,VP	C, F/M	F, F/M	NONE
9	37		0-5	C	W/M,SB	ExH	Ex	VS,VP	F, F/M	F, F/M	NONE
10	43		0-5	SC	M,SB	VH	VF	VS,VP	F, F/M	F, F/M	NONE
11	48		0-5	SC	M,SB	H/VH	F/VF	S/VS,P/VP	C, F/M	F, F/M	NONE
12	48		0-5	SC	M,SB	H	F	S/P	C, F/M	F, F/M	NONE

Boundary	Texture	Structure	Consistence			Pores	Roots	Mottling
			Side Wall	Ped	Wet			
A=Abrupt <1" C=Clear 1"-2.5" G=Gradual 2.5"-5" D=Diffuse >5"	S=Sand LS=Loamy Sand SL=Sandy Loam SCL=Sandy Clay Loam SC=Sandy Clay CL=Clay Loam L=Loam C=Clay SiC=Silty Clay SiCL=Silty Clay Loam SiL=Silt Loam Si=Silt	W=Weak M=Moderate S=Strong G=Granular PI=Platy Pr=Prismatic C=Columnar AB=Ang. Blocky SB=Subang.Blocky M=Massive SG=Single Grain C=Cemented	L=Loose S=Soft SH=Slightly Friable H=Hard VH=Very ExH= Extrm Hard	L=Loose VFRB=Very Friable FRB=Friable F=Firm VF=Very Firm Ex= Extrm. Firm	NS=NonSticky SS=Slightly Sticky S=Sticky VS=Very Sticky NP=Non Plastic SP=Slightly Plastic P=Plastic VP=Very Plastic	<u>Quantity:</u> F=Few C=Common M=Many <u>Size:</u> VF=Very Fine F=Fine M=Medium C=Coarse VC=Very Coarse	<u>Quantity:</u> F=Few C=Common M=Many <u>Size:</u> F=Fine M=Medium C=Coarse VC=Very Coarse ExC=Extrm. Coarse	<u>Quantity:</u> F=Few C=Common M=Many <u>Size:</u> F=Fine M=Medium C=Coarse <u>Contrast:</u> Ft=Faint D=Distinct P=Prominent

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USE PERMIT ASSISTANCE

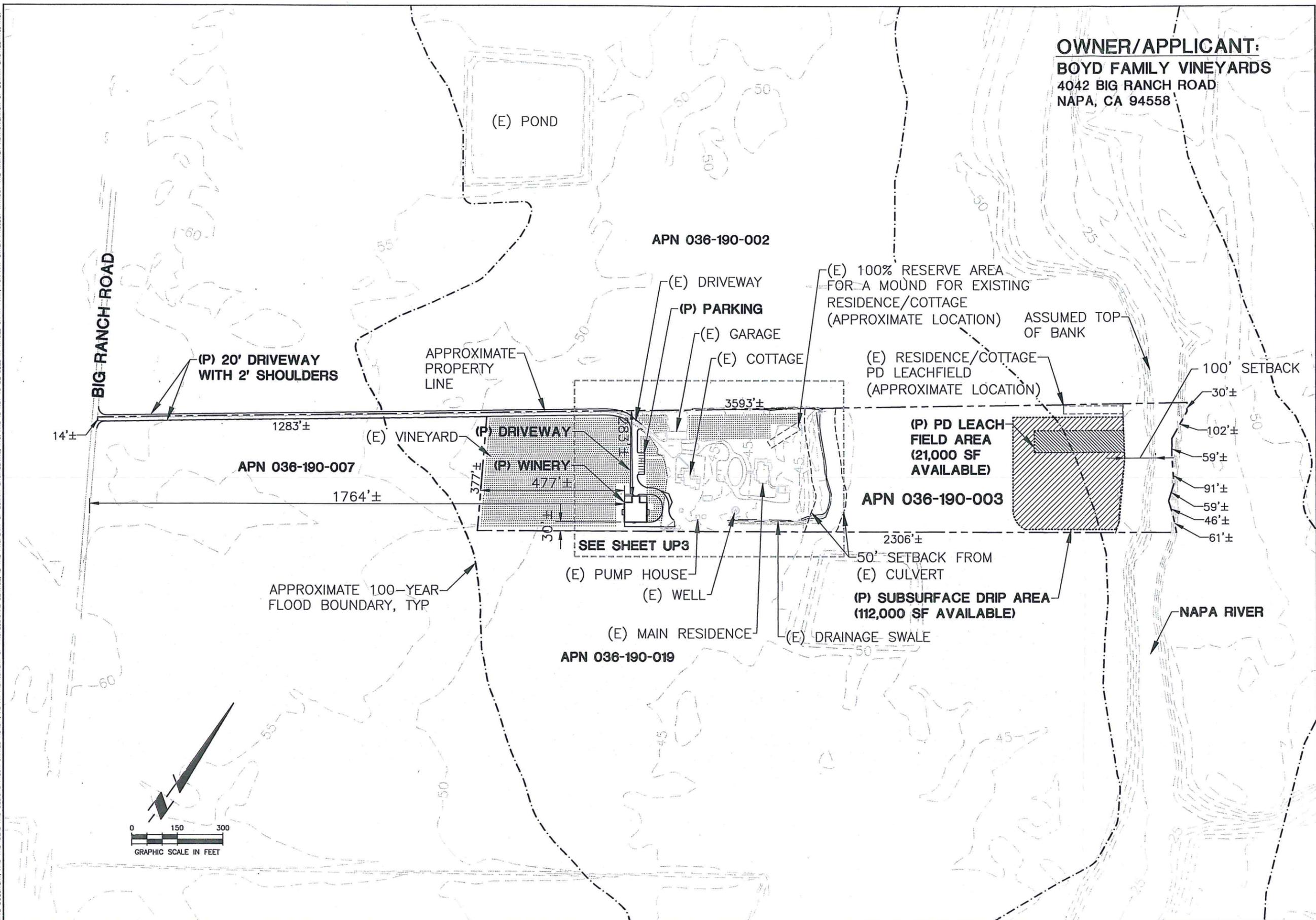
TEST PIT LOCATIONS

XX-XX-XXXX2  
PERMIT SUBMITTAL

DATE: XX-XX-XXXX1  
JOB NO: 2015148  
SCALE: AS SHOWN  
DRAWN: JA  
CHECKED: INITIALS2  
SHEET

**UP5**

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**OWNER/APPLICANT:**  
**BOYD FAMILY VINEYARDS**  
 4042 BIG RANCH ROAD  
 NAPA, CA 94558

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 APN 036-190-003

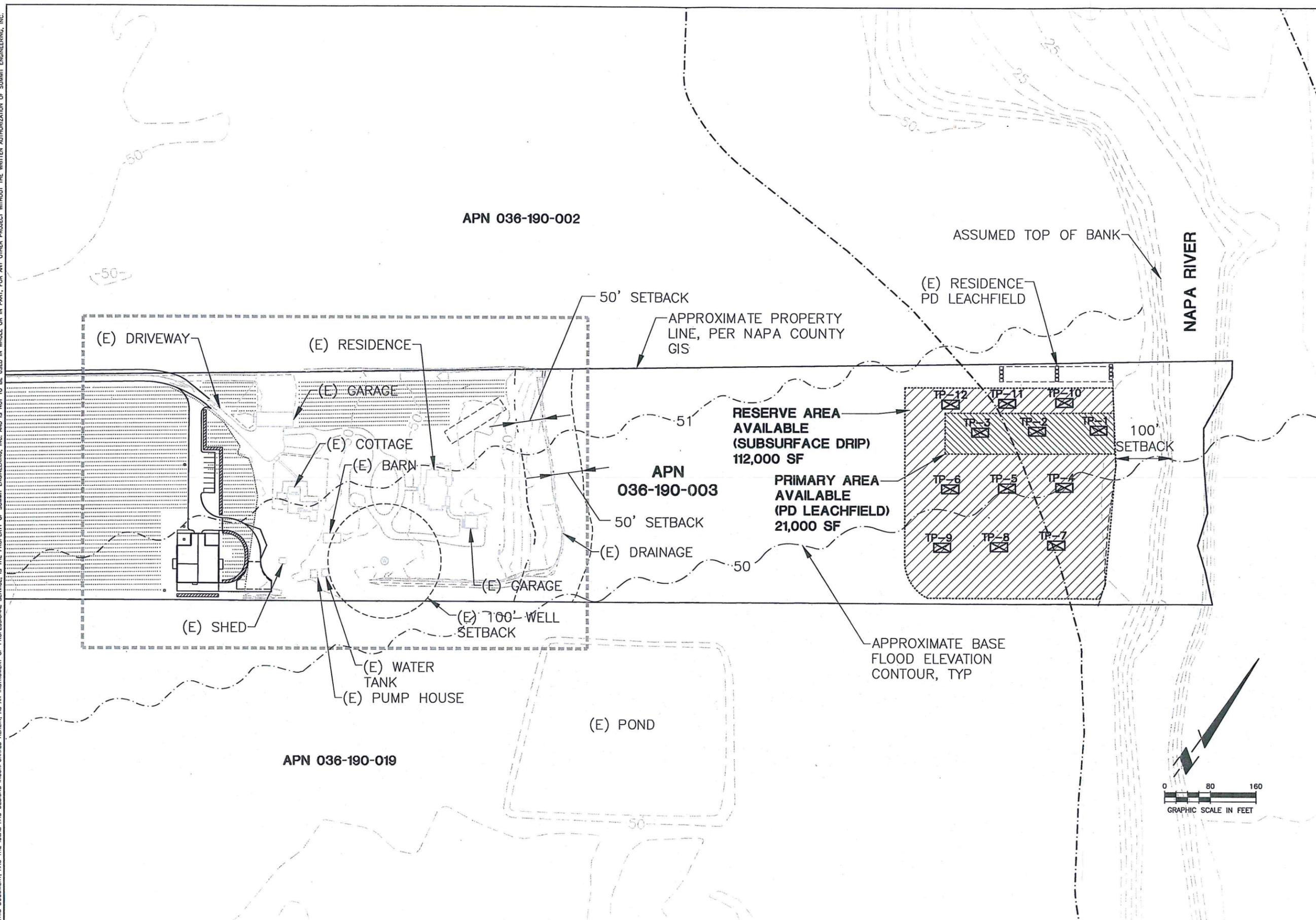
**OVERALL PROPOSED  
 SITE PLAN**

2017-10-20  
 USE PERMIT SUBMITTAL

DATE: 2017-09-20  
 JOB NO: 2017120  
 SCALE: AS SHOWN  
 DRAWN: JA  
 CHECKED: TCS

SHEET  
**UP2**

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NAPA, CA 94558  
APN 036-190-003

USE PERMIT ASSISTANCE  
**WASTEWATER SITE PLAN**

2017-10-20  
PERMIT SUBMITTAL

DATE: 2017-09-20  
JOB NO: 2017120  
SCALE: AS SHOWN  
DRAWN: JA  
CHECKED: CP

SHEET  
**UP4**