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Water Availability Analysis

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WATER AVAILABILITY ANALYSIS
3283 St. Helena Highway, St. Helena
County of Napa, APN 022-080-004

Prepared for

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Napa County Planning, Building
& Environmental Services

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Introduction

The objective of this study is to assess the availability of groundwater for a proposed 12,000 gallon per year winery to be located on the subject property in unincorporated Napa County north of St. Helena (Figure 1). This Water Availability Analysis (WAA) has been prepared using new guidelines adopted with approval of the Napa County Board of Supervisors May 12, 2015, for evaluating groundwater for discretionary projects requiring use permits such as new wineries. The guidelines were developed and disseminated by the Napa County Planning Building & Environmental Services Department (PBES).

The project site is located about three miles north of central St. Helena and just to the south of Bale Grist Mill State Park at the west edge of the Napa Valley. The 11.1 acre parcel lies at the foot of the mountain slope adjacent to State Highway 29 (St. Helena Highway), and at the highest location on its western boundary is about 140 ft above the valley floor. The parcel is located in the "Hillside" zone of the County with respect to the source of groundwater. Such Hillside parcels require a site-specific WAA to evaluate proposed project groundwater use in the context of local hydrogeologic conditions and in relation to estimated annual groundwater recharge.

The responsible professional for the WAA is Matt O'Connor, PhD, California Professional Geologist #6847 and Certified Engineering Geologist #2449, assisted by Michael Sherwood, BS, Professional Geologist #8839. O'Connor Environmental Inc. has conducted approximately 60 similar water availability analyses in bedrock aquifers of water-scarce zones of Sonoma County over the past 12 years, and has conducted a variety of hydrologic and geologic analyses in Napa and Lake County over the past 15 years.

Approach

The WAA procedure requires the applicant

...to estimate the average annual recharge occurring on the project parcels(s) and consider the amount of recharge relative to the estimation of project water use (e.g., all current and project water demands for the property on which the planned project is located). The estimate of annual recharge can be made by various methods including water balance methods. The selected method should be based on data from the parcel or watershed where the proposed project is located. The estimated project water use, including existing and proposed uses of water on the project parcel(s), shall include estimates for normal and dry water years.¹

¹ Water Availability Analysis (WAA), Adopted May 12, 2015 by Board of Supervisors, County of Napa, p. 8.

The analytical tool used to estimate groundwater recharge is the water balance, the most fundamental means available to hydrogeologists. A recently-developed water balance for the Napa River watershed was prepared for the County of Napa (Luhdorff & Scalmanini, 2013), and is used to provide the analytical framework for this site-specific WAA. Prior to conducting a water balance analysis, the contributing area of the local aquifer where recharge is expected to occur must be determined. This requires development of a conceptual model of the local aquifer based on available hydrogeologic data.

The location of wells on the project parcel and neighboring parcels that could be affected by project groundwater use must be located to evaluate potential well interference per Tier 2 criteria of the WAA.

Organization of this WAA

This report is organized as follows. The first section describes the proposed project including land use and projected water use. The second section describes hydrogeologic conditions that define the probable groundwater recharge area in the vicinity of the project based on available maps and drillers' reports for wells on the project parcel. The third section presents the water balance analysis. The fourth section summarizes the Tier 1 WAA for the project. The fifth section addresses the Tier 2 component of the WAA.

Limitations

Groundwater systems of Napa County and the Coast Range are typically complex, and available data rarely allows for more than general assessment of groundwater conditions and delineation of aquifers. This analysis is based on limited available data and relies significantly on interpretation of data from disparate sources of disparate quality. Drillers' reports and water quality data available for this assessment were made available to us by the property owner.

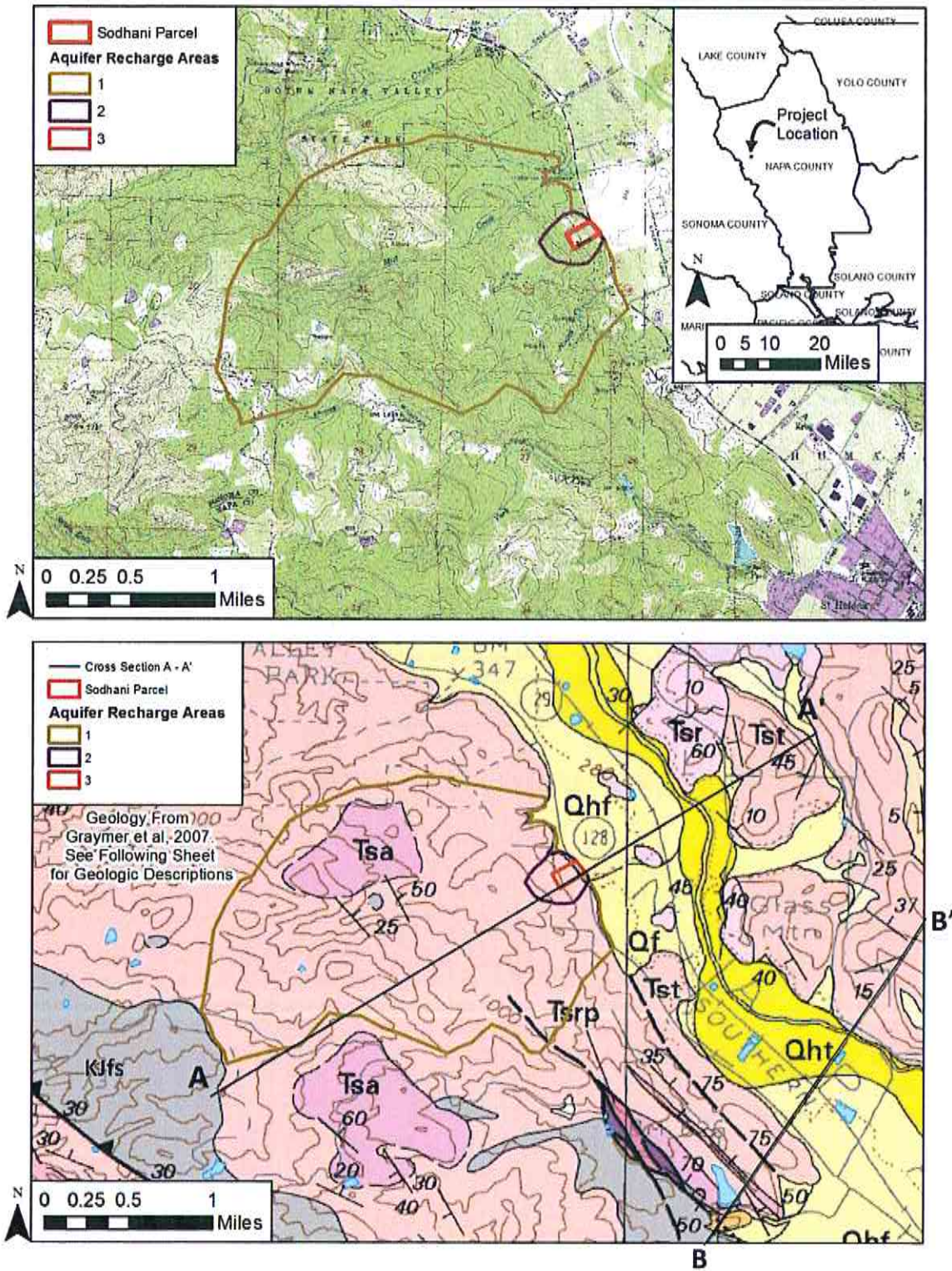


Figure 1. Topographic and geologic maps of project site and vicinity. Hypothesized aquifer recharge Area 1 represents maximum potential extent of drainage area affecting recharge; Area 2 represents likely minimum effective recharge area; Area 3 corresponds to the project parcel. Section B-B' is shown in Fig. 3; A-A' in Fig. 4.

LIST OF MAP UNITS

[Some unit exposures on the map are too small to distinguish the color for unit identification. These units are labeled where possible, and unlabeled units are attributed in the database.]

SURFICIAL DEPOSITS		Sonoma Volcanics		Franciscan Complex	
af	Artificial fill (Historic)	Tsv	Sonoma Volcanics, unfolded (Pliocene and late Miocene)	sp	Serpentinite (Jurassic)
afhw	Artificial fill over Bay mud (Historic)	Tsr	Rhyolite flows	sb	Siliceous basaltic rock
afh	Artificial levee fill (Historic)	Tsd	Rhyolite plugs	sm	Serpentinitic matrix mélange
Qhc	Stream channel deposits (late Holocene)	Tsrp	Soda rhyolite flows	FRANCISCAN COMPLEX	
Qhay	Younger alluvium (late Holocene)	Tsrp	Perlitic rhyolite	fm	Mélange, including blocks, mapped locally, of
Qhts	Terrace deposits (late Holocene)	Tsrp	Rhyolite breccia	sp	Serpentinite
Qha	Alluvium (Holocene)	Tsa	Andesite to basalt lava flows	gs	Graywacke
Qht	Terrace deposits (Holocene)	Tsd	Andesite to dacite plugs	ch	Chert
Qaf	Alluvial fan deposits (Holocene)	Tsb	Basalt flows	gpc	Greenstone and chert
Qhf	Finagraded alluvial fan deposits (Holocene)	Tsd	Basalt or andesite lava flows and scoriae	gt	Greenstone
Qhd	Natural levee deposits (Holocene)	Tst	Pumiceous ash-flow tuff	mg	High-grade metamorphic rocks
Qhb	Barin deposits (Holocene)	Tst	Welded ash-flow tuff	Kfs	Sandstone (Late Cretaceous, Turonian?)
Qhws	Bay mud (Holocene)	Tstx	Tuff(?)	Kfm	Metagraywacke (Late and Early Cretaceous)
Ox	Alluvium (Holocene and late Pleistocene)	Tt	Agglomerate	Kfnc	Metasiltstone (Late and Early Cretaceous)
Qf	Terrace deposits (Holocene and late Pleistocene)	Tt	Tuff breccia	Kfmg	Metagraywacke (Late and Early Cretaceous)
Qf	Alluvial fan deposits (Holocene and late Pleistocene)	Tt	Tuff	Kjfs	Graywacke and mélange (Early Cretaceous and Late Jurassic)
Qfb	Landslide deposits (Holocene and late Pleistocene)	Tt	Volcanic sand and gravel	chj	Chert (Cretaceous to Jurassic)
Qba	Andesite composition	Tt	Diatomite	Kjgpc	Greenstone and chert (Cretaceous to Jurassic)
Qbu	Rhyolite composition	Tt	Wilson Grove Formation (late Pliocene to late Miocene)	Kjgpc	Greenstone (Cretaceous to Jurassic)
Qba	Alluvium (late Pleistocene)	Tt	Sand and gravel of Catai (Pliocene and late Miocene)	MAP SYMBOLS	
Qbf	Terrace deposit (late Pleistocene)	Tt	Petaluma Formation (early Pliocene and late Miocene)	-----	Contact—Depositional or intrusive contact, dashed where approximately located, dotted where concealed.
Qbf	Alluvial fan deposits (late Pleistocene)	Tt	Danville Ranch Volcanics (late Miocene)	-----	Fault—Dashed where approximately located, small dashes where inferred, dotted where location is uncertain, orange denotes Quaternary-active fault, magenta denotes Holocene active fault.
Qba	Alluvium (late and early Pleistocene)	Tt	Nerby Sandstone (late Miocene)	-----	Reverse or thrust fault—Dashed where approximately located, small dashes where inferred, dotted where concealed, spaced where location is uncertain, wavy teeth on upper plate.
Qfb	Landslide deposits (late and early Pleistocene)	Tt	Clerbo Sandstone (late Miocene)	-----	Anticline—Dashed where approximately located, dotted where concealed.
Clear Lake Volcanics		Tt	Burdell Mountain volcanics (late and middle? Miocene)	-----	
Qf	Rhyolite (Pleistocene)	Tt	Unnamed sandstone (middle Miocene)		
Qfb	Offshore basalt (Pleistocene and Pliocene)	Tt	Kicker Tuff (early Miocene and/or Oligocene)		
Qft	Tuff (Pleistocene and/or Pliocene)	Tt	Unnamed sandstone (Eocene and Pliocene)		
T	Rhyolite (Pliocene)	Tt	Unnamed sandstone (Eocene? or Pliocene?)		

Geology Map Units shown in Figure 1 (after Graymer et al. 2007)

Surficial Deposits

- Qht-Terrace deposits (Holocene)
- Qhf-Alluvial fan deposits (Holocene)
- Qf-Alluvial fan deposits (Holocene and late Pleistocene)

Sonoma Volcanics

- Tsr-Rhyolite flows
- Tsrp-Perlitic rhyolite
- Tsa-Anedsite to basalt lava flows
- Tst-Pumiceous ash-flow tuff

Franciscan Complex

- Kjfs-Graywacke and mélange (Early Cretaceous and Late Jurassic)

Project Description and Water Use

The proposed winery would be built adjacent to the residence located on the upper elevations of the 11.1 acre parcel. A single-family residence and 6.3 acre vineyard comprise the current use of the parcel (Figure 2). The proposed 12,000 gallon per year winery would be the only new land use on the parcel that would require additional groundwater use.

Anticipated water use was documented in a Water Availability Analysis Phase One Study prepared by Michael Muelrath, PE No. 67435, dated December 5, 2014 (Appendix A) previously submitted to the Department of Public Works (DPW). At that time, the applicant was advised that new guidelines would apply, and that the Phase One Study submitted was no longer sufficient. Nevertheless, the water use calculations for existing and proposed conditions in the December 2014 Phase One Study remain valid and were adopted for this WAA, with one modification. For this WAA, to be conservative with respect to long-term groundwater use, we assumed annual water use of 0.5 acre-feet per acre of vineyard. There are 6.3 acres of vineyard, so the annual irrigation demand is 3.15 acre-feet. Existing and proposed water use on the subject parcel is summarized in Table 1. Refer to Appendix A for additional details regarding water use estimates.

Table 1. Existing and Proposed Water Use

Land Use	Existing Water Use (ac-ft/yr)	Proposed Water Use (ac-ft/yr)
Residential	0.75	0.75
Vineyard	3.15	3.15
Winery	--	0.26
Winery Landscaping	--	0.25
Winery Employees	--	0.04
Total Water Use	3.9	4.45

Groundwater use for the proposed winery project, including winery production, landscaping and winery employees would total 0.55 acre-feet per year, increasing annual groundwater use to 4.45 acre-feet per year. This represents an 14% increase in groundwater use relative to existing conditions. Under existing conditions, water use is 0.35 ac-ft per acre on the parcel. With expanded water use associated with the proposed winery, water use would be 0.40 ac-ft per acre.

There are two wells located on the project parcel (Figure 2). One well lies near the southeast corner of the parcel at the downhill edge of the vineyard and is referred to as "Vineyard Well" and Well #2 in Figure 2. This well has high concentrations of arsenic (130 ug/L) and is not potable but is suitable for vineyard irrigation (see water quality data, Appendix B). The second well is located near the southwest corner of the parcel and near the high spot on the parcel is referred to as the "House Well" and Well #1 in Figure 2. It provides potable water for domestic use in the residence on the property and is the only existing source of potable water for the

proposed winery (see water quality analysis data, Appendix C). Because of the unsuitability of water from the Vineyard Well for use in the winery, this analysis focuses primarily on the House Well which is the project well.

Bedrock Geology

The recent U.S. Geological Survey map “Geologic Map and Map Database of Eastern Sonoma and Western Napa Counties, California” (Graymer et al. 2007) was used for interpretation of the project area geology, supplemented by the recent Napa County report “Update Hydrogeologic Conceptualization and Characterization of Conditions” (Luhdorff & Scalmanini, 2013).

Figure 1 shows the project parcel, topography, and surface geology for the vicinity north of St. Helena. The project parcel is located just to the west of the Napa Valley floor north of St. Helena (Figure 1) about 0.8 mile west of the Napa River and about 0.4 mile south of Mill Creek. The surficial geology at the project parcel is the tuffaceous member of the Sonoma Volcanics (map unit Tst), which mantles most of the mountain slopes on the west side of Napa Valley from St. Helena north to Calistoga and beyond. The Sonoma Volcanics consist of a thick and highly variable series of volcanic rocks including basalt, andesite, and rhyolite lava flows, tuff, tuff breccia, agglomerate, scoria, and their sedimentary derivatives (Kunkel and Upson, 1960). The tuffaceous, scoriaceous, and sedimentary units are the principle water-bearing units whereas the lava flows generally yield little to no water (Kunkel and Upson, 1960; Faye, 1973). The tuff underlying the project site and the likely aquifer and recharge area (map unit Tst) is described by Graymer et al. as:

Pumiceous ash-flow tuff—Pumiceous tuff, locally welded, and agglomeratic tuff, andesite and basalt flow rocks, tuff breccia, and bedded tuff.

Normal (vertical) faults trending parallel to the orientation of Napa Valley are mapped in the vicinity of the boundary between the valley floor and the hillsides between the project site and St. Helena (Figure 1). Where mapped, the faults dip 75 degrees to the east. These faults have not been mapped as far north as the project site, but it should be assumed that these or similar faults are present at or near the project site. The hydrogeologic investigation for Napa Valley (Luhdorff & Scalmanini, 2013, Figure 5-3, Cross Section A-A') also found evidence suggesting the presence of normal faults in the bedrock underlying the valley floor.

Bedding planes mapped within the tuff in the vicinity of the project site on the west side of the valley north of St. Helena (Figure 1) strike parallel to the fault and valley orientation and dip 25 to 50 degrees to the northeast.

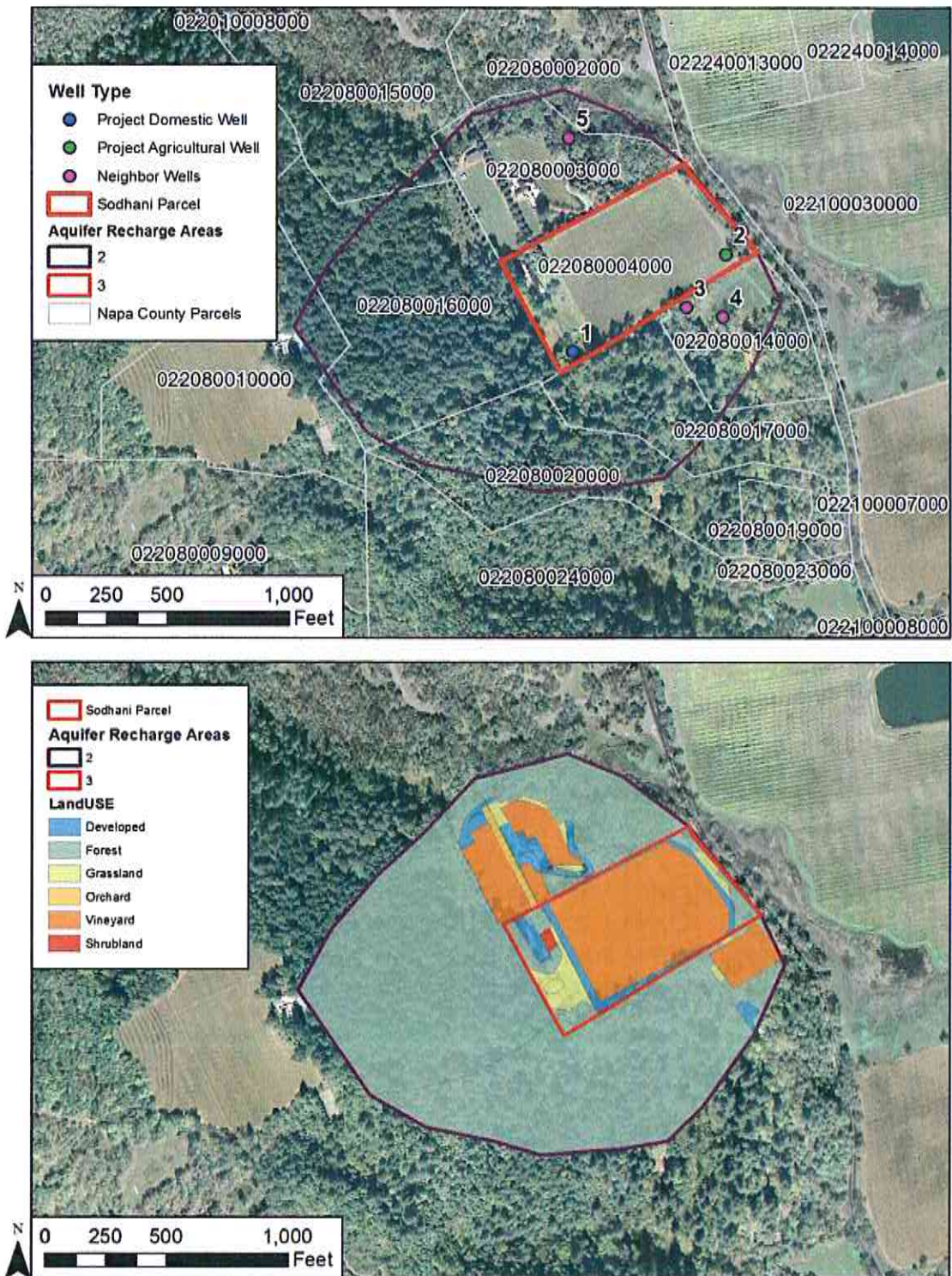


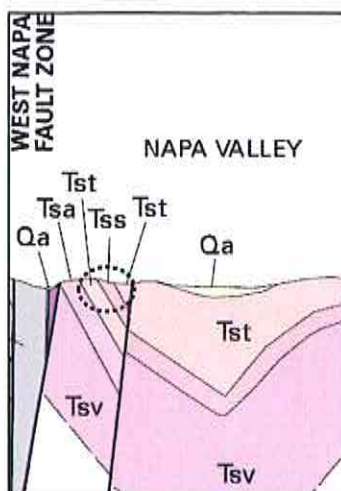
Figure 2. Local area parcel map and well locations (top) and recharge area land use map used in water balance evapotranspiration estimate (bottom). Well 1 is the project well. Well 3 is the nearest well on a neighboring parcel.

Hydrogeologic Conditions

The hydrogeology of the project site is influenced by the foregoing geologic characteristics. The tuff is generally a water-bearing unit of the Sonoma Volcanics, but it includes a variety of layered rocks, some of which are not considered water bearing (e.g. andesite flows). This creates the potential for confined aquifer units where aquitards formed by andesite (or other relatively impermeable volcanic materials) separate strata of more permeable rocks. The orientation of rock layers is variable, but dips in the range 25 to 50 degree to the northeast. Consequently, it is possible that confined aquifer rock units underlying the project site extend to the surface on the hillslopes above and west of the project site. In addition, normal faults (vertical or near-vertical orientation) could be present that affect groundwater flow in the aquifer rocks within the tuff. Faults may or may not affect groundwater flow, but can act as barriers to groundwater flow as well as conduits of groundwater flow.

Regardless of the rock types and structures that may affect the hydrogeologic conditions in the local aquifer, it is expected that the elevation of the potentiometric water surface underlying the mountain slopes west of the valley floor will lie more or less parallel to the ground surface. Consequently, it is expected that there would be a relatively steep hydraulic gradient extending from the project site (located at the base of the mountain front) to a point near the ridge crest about two miles to the west. It is possible that the groundwater flow to the project site originates high on the ridge to the west, infiltrated as rainfall on the ground surface and from stream channels into aquifer rocks, and flowing down-gradient across and through various aquifer rocks in complex flow paths before reaching the well at the project site. This conceptualization of a relatively large confined or semi-confined aquifer gives rise to the drainage area boundary referenced as Area 1 in Figure 1. Although this conceptualization is not unrealistic, it is based on relatively broad assumptions that would be difficult to confirm or constrain.

A more conservative conceptualization of the site aquifer hydrogeology can be inferred from hydrogeologic cross-sections, taking into account the limited structural information on geologic strata and information on aquifer materials from on-site wells. Data describing the geologic materials logged during well construction and well construction details were obtained from Well Completion Reports or County well permits (Appendix D).



The regional geologic cross-section prepared by Graymer et al. (2007)² is oriented southwest to northeast perpendicular to Napa Valley and crosses the west edge of the Napa Valley Floor about two miles south of the project site. Figure 3 shows the portion of that geologic sections shown as B-B' in Figure 1. The circled portion of Figure 3 indicates the portion of the section that corresponds most closely to the position of the project site and portrays steeply dipping geologic contacts presumed approximately parallel to bedding planes. About one mile west of the project site bedding planes in the tuff (map unit Tst) were mapped with dips of 25 and 50 degrees to the northeast, and about one mile southeast a bedding plane in Tst dips 35 degrees to the northeast.

Figure 3. Geologic cross-section from regional geology map.

Based on the foregoing indications regarding the orientation of geologic strata within the tuff unit of the Sonoma Volcanics underlying the project site, it is possible to hypothesize the geometry of the aquifer rocks at the project site using the depths of water bearing strata identified in the well logs (Appendix D). As shown in Figure 4, we determined the depth of the top of geologic strata corresponding to the perforated sections of Well #1 (the project and "House" well) and projected them with a 25 degree northeast dip on the cross-section line A-A' (Figure 1) constructed approximately perpendicular to strike. The lower-most of the water-bearing strata in the project well (#1) reaches the ground surface to the west of a hill crest about 1,000 ft west of the project well (Figure 4). We also considered a 50 degree northeast dip, and found the lower-most water bearing strata reaching the ground surface about 300 ft west of the project well. The projection of the 25 degree dip coincides approximately with a subsidiary ridge crest above the project site that forms a topographic divide and a local drainage area that encompasses the project site parcels as well as adjacent parcels to the north, west and south and shown as Area 2 in Figure 1.

Area 2 represents a conservative conceptualization of the rainfall-recharge area for the project aquifer, and is considered the primary zone of recharge for the project aquifer for purposes of this WAA. As noted above, however, the complex character of groundwater in volcanic rocks, the position of the project well at the base of the mountain front west of Napa Valley, and the likely hydraulic gradient of groundwater underlying the mountain hillslopes to the west suggest that groundwater recharge for the project aquifer is likely to include a portion of Area 1.

² Graymer, R.W. et. al., 2007. Geologic Map and Map Database of Eastern Sonoma and Western Napa Counties, California. Pamphlet to accompany SCIENTIFIC INVESTIGATIONS MAP 2956. U.S. Department of the Interior U.S. Geological Survey.

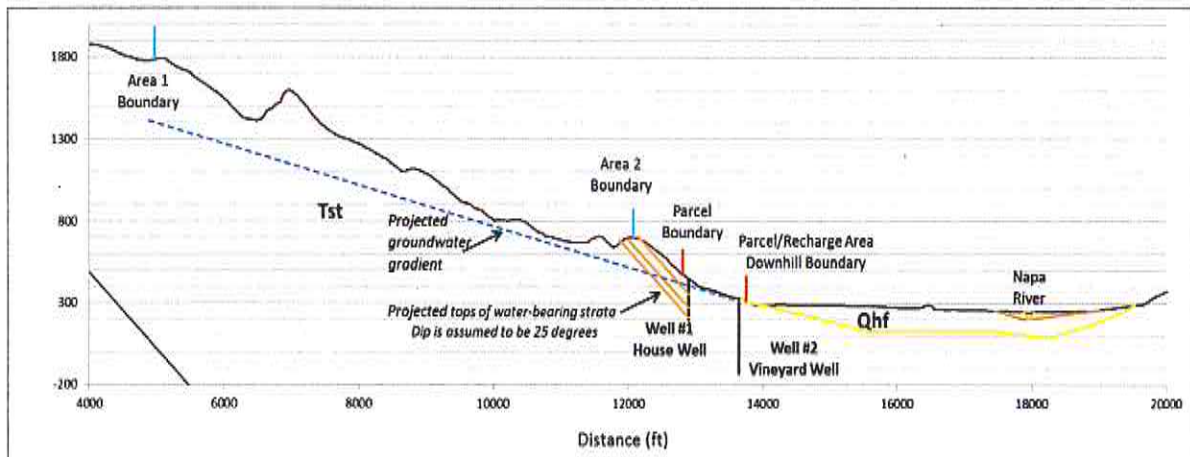


Figure 4. Local area geologic cross-section.

The conceptualization of the aquifer recharge zone for the project well congruent with the project parcel boundary is that represented as Area 3 (Figure 1). Given the likely groundwater hydraulic gradient extending up slope to the west (Figure 4), substantial groundwater flow originating from uphill beyond the parcel boundary likely reaches the project well. Furthermore, the upper 40 to 50 feet of the earth materials overlying the project site is comprised of gravel and boulder deposits likely to represent alluvial fan deposits (Qhf, Qf) mapped in adjacent areas to the east (Figure 1). There are several strata containing significant quantities of clay described in the well logs (project well-Appendix D; Sodhani irrigation well-Appendix E) interspersed with fractured volcanic rock, ash and sands, including a clay-rich strata at the base of the alluvial fan deposits. Although these clay-rich strata do not necessarily prevent downward movement of groundwater, they are likely to inhibit it, suggesting that vertical flow paths from the surface of the project parcel may not be the primary means of recharging water-bearing strata found at depths of 85 to 250 ft below ground surface in Well #1. Preferential flow paths parallel to the dip of rock strata in more permeable rocks separated by clay-rich strata would convey infiltrating groundwater from upslope. Such circumstances suggest that the primary recharge zone for the project well extends uphill to the west of the project parcel, and that conceptualizing the recharge area for the project well as the project parcel would substantially misrepresent local hydrogeologic conditions.

Chemical analyses of water samples from Wells #1 and #2 (Appendices B and C, respectively) indicate some significant differences between the water from these wells. In particular, Well #2 has very high levels of arsenic that render it unfit for human consumption and domestic use, and elevated levels of copper and lead relative to Well #1. Other differences of note are that Well #2 also has high turbidity, low nitrate, and low pH relative to Well #1. These differences, along with the greater depth (200+ feet) and potential effects of faults near or between Wells #1 and #2, suggest that these wells are utilizing distinct aquifers. Furthermore, it suggests that neighboring domestic wells to the south would not be utilizing the same aquifer as Well #2 owing to the high arsenic concentration.

Water Balance

A water balance analysis for Area 2 (Figure 2) to estimate the aquifer annual recharge rate is summarized in this section. The water balance for this WAA adapts the water balance analysis conducted for the Napa River watershed by Luhdorff and Scalmanini (2013) to account for site-specific conditions and hydrologic processes in Area 2.

The watershed-wide water balance was conducted on a monthly time-step at sub-watershed scales corresponding to stream gauging stations; the project site lies within the Napa River at St. Helena sub-watershed. For this sub-watershed, the water balance analysis spanned the period 1940 to 1994. The principal components of the watershed-wide water balance (referred to hereafter as the "L&SWB") are area-weighted precipitation, stream flow of the Napa River at the sub-watershed gauging station, estimated infiltration to the soil (taken as the difference between precipitation and runoff), and estimated evapotranspiration (ET) for a series of land cover types. Estimated groundwater recharge is represented by the difference between estimated infiltration and estimated ET modulated by soil moisture storage. Annual recharge varies with the amount and timing of rainfall, and with soil moisture storage estimated based on USDA NRCS soil survey data.

For the Napa River at St. Helena sub-watershed, the L&SWB estimated mean annual recharge of 22,000 acre-feet³; for the 78.8 square mile drainage area, this is equivalent to average annual recharge of 0.436 acre-feet per acre. Mean annual recharge is equivalent of 14% of mean annual precipitation. Variation in estimated annual recharge over time is induced by variation in annual precipitation, timing of precipitation, and availability of soil moisture in relation to ET. Estimated annual recharge ranged from a low of 0.05 acre-feet per acre to a high of 1.21 acre-feet per acre.

The simplest estimate of annual recharge for the local aquifer recharge zone (Area 2; 52.2 acres) is the recharge rate for the St. Helena sub-watershed estimated in the L&SWB of 0.436 acre-feet per acre times the recharge area: 52.2 acres x 0.436 acre-feet/acre = 22.8 acre-feet. While this estimate is not unreasonable, it is averaged over a large area with substantial variability in water balance parameters. In the following paragraph, readily available site-specific data and observations for Area 2 are described in relation to the average values for the St. Helena sub-watershed from the L&SWB to semi-quantitatively adjust the L&SWB estimate to the project site.

The project site recharge zone (Area 2) is not drained by any defined streams based on field observations and review of available topographic data. This strongly suggests that the proportion of annual precipitation that is subtracted from water available for infiltration is substantially lower in the project site recharge zone than in the L&SWB analysis where 41.5% of annual precipitation is accounted for as runoff. Mean annual precipitation for Area 2 from the

³ Luhdorff and Scalmanini Consulting Engineers and MBK Engineers, 2013. Updated hydrogeologic conceptualization and characterization of conditions. Prepared for Napa County. Table 8-9, p. 97.

PRISM data referenced in L&SWB is 38.5 inches compared to 38.4 inches for the St. Helena sub-watershed overall.

Soils data for Area 2 are tabulated in Appendix F and compared to the spatially-averaged soils for the St. Helena sub-basin, soil hydrologic factors are nearly uniform within Area 2 in that all soil types are in hydrologic Group B, which have moderate infiltration rates and moderate rates of water transmission; these soils are considered moderately well-drained to well-drained. In contrast, the hydrologic soil groups in the St. Helena sub-watershed are 56% Group C and 16% Group D, which have slow to very slow infiltration rates and slow to very slow rates of water transmission, respectively, and have varying degrees of clay and impeding soil horizons that limit downward movement of water. Taken together, the foregoing comparisons strongly suggest that infiltration rates of precipitation to the soil are likely to be substantially higher in Area 2 (the local aquifer recharge area) than the spatially-averaged infiltration rates in the St. Helena sub-watershed estimated by the L&SWB.

Average annual evapotranspiration (ET) for Area 2 was also compared to ET for the St. Helena sub-watershed estimated by the L&SWB. We classified land use and vegetation cover types in Area 2 from a 2007 Napa County aerial photograph according to the classification scheme used in the L&SWB⁴ as shown in Figure 2. Based on these cover types, we estimated mean annual potential evapotranspiration (PET) for Area 2 (Appendix G) to be 80.6 acre-feet, equal to 1.54 feet per year. For the St. Helena sub-watershed, the L&SWB estimated average ET of 1.44 feet per year. By definition PET must be greater than or equal to ET and in a Mediterranean climate with extended summer drought during the growing season, PET is typically substantially greater than ET. Consequently, ET for Area 2 is probably substantially lower than 1.54 ft, and probably not greater than the 1.44 ft ET estimated for the St. Helena sub-watershed in the L&SWB.

In summary, the foregoing comparison of water balance parameters between the project aquifer recharge area (Area 2) and the L&SWB St. Helena sub-watershed suggests that recharge in Area 2 is greater than that estimated by the L&SWB. Local soils in Area 2 are significantly more permeable than average for the St. Helena sub-watershed, and Area 2 is not drained by stream channels, consequently it would be expected that a substantially higher proportion of precipitation infiltrates to the soil and drains to the water table. ET in Area 2 is probably less than average for the St. Helena sub-watershed, also suggesting higher groundwater recharge in Area 2 than average for the St. Helena sub-watershed. Consequently, the mean annual groundwater recharge rate for the St. Helena sub-watershed of 0.436 acre-feet per acre should be considered a minimum estimate for Area 2, the project area groundwater recharge zone.

The calculation of mean annual recharge takes dry year and wet year precipitation and climate variation into account. Potential drawdown of water elevation in dry years is modulated by redistribution of groundwater in the aquifer, and would be expected to recover in normal and

⁴ IBID, Table 8-8, p. 87.

wet years. Water availability in the Sodhani wells for normal use has not been significantly affected by recent drought conditions.⁵

Well Interference Potential

The project well, also referred to as Well #1 and the “House Well”, is located 504 feet (horizontal distance) from the nearest off-site neighboring well (Figure 5). The distance was determined by measuring the ground distance from Well #1 with a fiberglass tape the southwest corner of the vineyard, and along the southernmost vine row to a point due north of the neighboring well. This distance to the fence line on the property boundary was measured, and the remaining distance from the fence to the neighboring well was visually estimated to be 25 ft. These measurements were used to plot the well location in our project GIS map, and the distance from the project well to the nearest neighbor’s well was measured using the GIS measuring tool. Mr. Arvind Sodhani used an iPhone 6 with the application GPS Tour to geolocate Wells 1, 2 and 3 (Figure 2) as described in Appendix H. That method indicated that Wells 1 and 3 were separated by a distance of about 509 feet.

The WAA guidance document regarding well interference states that “...the Tier 2 well interference criterion is presumptively met if there are no non-project wells located within 500 feet of the existing or proposed project well(s)⁶...” Given the location of the project well 504 to 508 feet from the nearest neighboring well, no further evaluation of potential well interference is required.

For reference with respect to Tier 3 WAA considerations, Figure 5 shows stream channels within a 1,500 foot radius of the project well.

Conclusion

Mean annual groundwater recharge in Area 2 is estimated to be not less than 22.8 acre-feet. The minimum estimate of mean annual recharge in Area 2 pro-rated for the project parcel area of 11.1 acres is 4.85 acre-feet (11.1 acre parcel/52.2 acre recharge zone x 22.8 acre-feet).

The proposed winery project, together with existing uses, would require 4.45 acre-feet per year, or about 92% of recharge in Area 2 pro-rated for the project parcel. This affirms the availability of groundwater sufficient for the proposed project.

The nearest neighbor’s well is located 504 feet from the proposed project well, indicating that potential well interference is negligible and requiring no further evaluation per the WAA procedures.

⁵ Pers. comm., Arvind Sodhani.

⁶ Water Availability Analysis (WAA), Adopted May 12, 2015 by Board of Supervisors, County of Napa, p. 8.

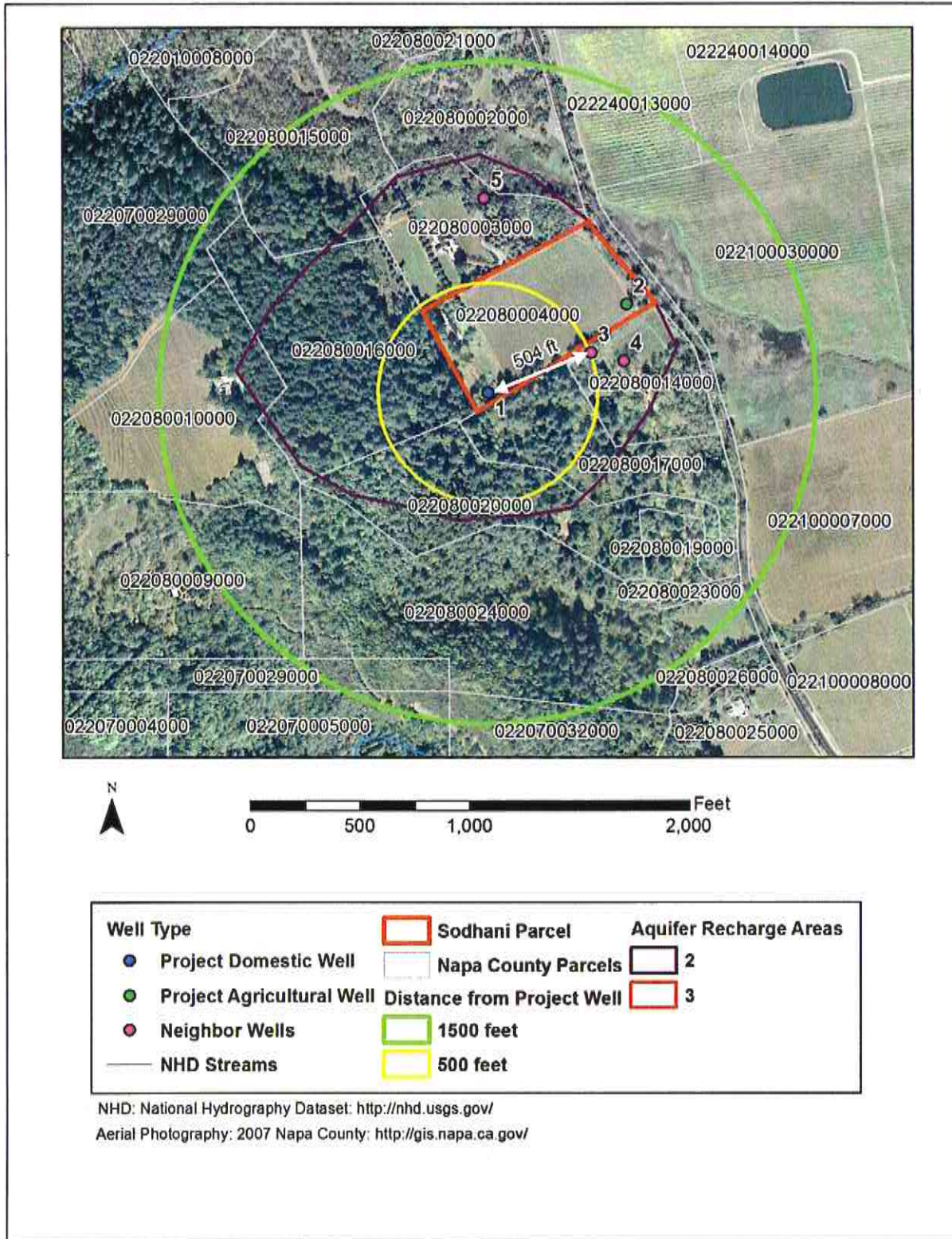


Figure 5. Location of wells and streams in relation to project well.

Appendix A-Phase 1 Water Availability Assessment, December 2014



A Tradition of Stewardship
A Commitment to Service

Department of Public Works

1195 Third Street, Suite 201
Napa, CA 94559-3092
www.co.napa.ca.us/publicworks

Main: (707) 253-4351
Fax: (707) 253-4627

Donald G. Ridenhour, P.E.
Director

WATER AVAILABILITY ANALYSIS - PHASE ONE STUDY

Introduction: As an applicant for a permit with Napa County, it has been determined that Chapter 13.15 of the Napa County Code is applicable to approval of your permit. One step of the permit process is to adequately evaluate the amount of water your project will use and the potential impact your application might have on the static groundwater levels within your neighborhood. The public works department requires that a Phase 1 Water Availability Analysis (WAA) be included with your application. The purpose of this form is to assist you in the preparation of this analysis. You may present the analysis in an alternative form so long as it substantially includes the information required below. Please include any calculations you may have to support your estimates.

The reason for the WAA is for you, the applicant, to inform us, to the best of your ability, what changes in water use will occur on your property as a result of an approval of your permit application. By examining the attached guidelines and filling in the blanks, you will provide the information we require to evaluate potential impacts to static water levels of neighboring wells.

Step #1:

Provide a map and site plan of your parcel(s). The map should be an 8-1/2"x11" reproduction of a USGS quad sheet (1:24,000 scale) with your parcel outlined on the map. Include on the map the nearest neighboring well. The site plan should be an 8-1/2"x11" site plan of your parcel(s) with the locations of all structures, gardens, vineyards, etc in which well water will be used. If more than one water source is available, indicate the interconnecting piping from the subject well to the areas of use. Attach these two sheets to your application. If multiple parcels are involved, clearly show the parcels from which the fair share calculation will be based and properly identify the assessor's parcel numbers for these parcels. Identify all existing or proposed wells

Step #2: Determine total parcel acreage and water allotment factor. If your project spans multiple parcels, please fill a separate form for each parcel.

Determine the allowable water allotment for your parcels:

Parcel Location Factors

The allowable allotment of water is based on the location of your parcel. There are 3 different location classifications. Valley floor areas include all locations that are within the Napa Valley, Pope Valley and Carneros Region, except for areas specified as groundwater deficient areas. Groundwater deficient areas are areas that have been determined by the public works department as having a history of problems with groundwater. All other areas are classified as Mountain Areas.

Please underline your location classification below (Public Works can assist you in determining your classification if necessary):

Valley Floor	1.0 acre feet per acre per year
Mountain Areas	0.5 acre feet per acre per year
MST Groundwater Deficient Area	0.3 acre feet per acre per year

Assessor's Parcel Number(s)	Parcel Size (A)	Parcel Location Factor (B)	Allowable Water Allotment (A) X (B)
022-080-004	11.1	.5	5.5

Step #3:

Using the guidelines in Attachment A, tabulate the existing and projected future water usage on the parcel(s) in acre-feet per year (af/yr). Transfer the information from the guidelines to the table below.

EXISTING USE:		PROPOSED USE:	
Residential	<u>.75</u> af/yr	Residential	<u>.75</u> af/yr
Farm Labor Dwelling	_____ af/yr	Farm Labor Dwelling	_____ af/yr
Winery	_____ af/yr	Winery	<u>.26</u> af/yr
Commercial	_____ af/yr	Commercial	_____ f/yr
Vineyard*	<u>2.3</u> af/yr	Vineyard*	<u>2.3</u> af/yr
Other Agriculture	_____ af/yr	Other Agriculture	_____ af/yr
Landscaping	_____ af/yr	Landscaping	<u>.25</u> af/yr
Other Usage (List Separately):		Other Usage (List Separately):	
_____	_____ af/yr	<u>Winery Emp</u>	<u>.04</u> af/yr
_____	_____ af/yr	_____	_____ af/yr
_____	_____ af/yr	_____	_____ af/yr

TOTAL:	<u>3.05</u> af/yr	TOTAL:	<u>3.60</u> af/yr	TOTAL:
	<u>0.99 M</u> gallons"	TOTAL:	<u>1.17 M</u> gallons"	

Is the proposed use less than the existing usage? Yes No Equal

Step #4:

Provide any other information that may be significant to this analysis. For example, any calculations supporting your estimates, well test information including draw down over time, historical water data, visual observations of water levels, well drilling information, changes in neighboring land uses, the usage if other water sources such as city water or reservoirs, the timing of the development, etc. Use additional sheets if necessary.

- Residential = 0.75 af/yr per County Guidelines and includes landscaping
- Winery = 12,000 gallons x 2.15 af/yr per 100,000 gallons of wine per County Guidelines (production only)
- Vineyard = 6.3 acres x 0.365 ac-ft/ac/r per County Guidelines and Vineyard Manager
- Landscaping = 0.3 acres low water use landscaping around winery per landscape design and water estimates
- Employees = 4 employees x 0.01 ac-ft/yr per employee per County Guidelines

Conclusion: Congratulations! Just sign the form and you are done! Public works staff will now compare your projected future water usage with a threshold of use as determined for your parcel(s) size, location, topography, rainfall, soil types, historical water data for your area, and other hydrogeologic information. They will use the above information to evaluate if your proposed project will have a detrimental effect on groundwater levels and/or neighboring well levels. Should that evaluation result in a determination that your project may adversely impact neighboring water levels, a Phase two water analysis may be required. You will be advised of such a decision.

Signature: _____ Date: 12/5/2014 Phone: (707) 320-4968



WATER AVAILABILITY ANALYSIS - PHASE ONE STUDY

Attachment A: Estimated Water Use Guidelines

Typical Water Use Guidelines:

Primary Residence	0.5 to 0.75 acre-feet per year (includes some landscaping)
Secondary Residence	0.20 to 0.30 acre-feet per year
Farm Labor Dwelling	0.06 to 0.10 acre-feet per person per year

Non-Residential Guidelines:

Agricultural:

Vineyards

Irrigation only 0.2 to 0.5 acre-feet per acre per year

Heat Protection 0.25 acre feet per acre per year

Frost Protection 0.25 acre feet per acre per year

Farm Labor Dwelling 0.06 to 0.10 acre-feet per person per year

Irrigated Pasture 4.0 acre-feet per acre per year

Orchards 4.0 acre-feet per acre per year

Livestock (sheep or cows) 0.01 acre-feet per acre per year

Winery:

Process Water 2.15 acre-feet per 100,000 gal. of wine

Domestic and Landscaping 0.50 acre-feet per 100,000 gal. of wine

Industrial:

Food Processing 31.0 acre-feet per employee per year

Printing/Publishing 0.60 acre-feet per employee per year

Commercial:

Office Space 0.01 acre-feet per employee per year

Warehouse 0.05 acre-feet per employee per year

Appendix B-Water Quality Analysis, Project Well



David W Bess
David W Bess
1115 Mt George Ave
Napa, California 94558
Tel: 707-226-2539
Email: dave@dbesspumpandwell.com
RE: WaterQ Basic (Well Water for Dave Bess)

Work Order No.: DWQ1306008-A

Dear David W Bess:

Torrent Laboratory, Inc. received 1 sample(s) on June 13, 2013 for the analyses presented in the following Report.

All data for associated QC met EPA or laboratory specification(s) except where noted in the case narrative.

Torrent Laboratory, Inc. is certified by the State of California, ELAP #1991. If you have any questions regarding these test results, please feel free to contact the Project Management Team at (408)263-5258; ext 204.

Patti Sandroock
QA Officer

June 18, 2013

Date



Date: 6/18/2013

Client: David W Bess

Project: WaterQ Basic (Well Water for Dave Bess)

Work Order: DWQ1306008-A

CASE NARRATIVE

No issues encountered with the receiving, preparation, analysis or reporting of the results associated with this work order.

Observations:

Primary Contaminants- (Health)

No primary contaminants in the scope of analysis presented in this report were found to be outside of the EPA Federally established Maximum Contaminant Level (MCL) guidelines.

Secondary Contaminant - (Water Aesthetics)

No secondary contaminants in the scope of analysis presented in this report were found to be outside of the EPA Federally established Maximum Contaminant Level (MCL) guidelines (or recommended level where no MCLs exist).

This report is for House Well Sample only and is labeled and stored as DWQ-1306008-A.

The Irrigation Well sample will be reported separately as DWQ-1306008-B.



Sample Result Summary

Report prepared for: David W Bess
David W Bess

Date Received: 06/13/13
Date Reported: 06/18/13
DWQ1306008-001

House well

<u>Parameters:</u>	<u>Analysis Method</u>	<u>DF</u>	<u>MDL</u>	<u>PQL</u>	<u>Results</u>	<u>Unit</u>
Boron	E200.7	1	0.001	0.020	0.048	mg/L
Copper	E200.8	1	0.077	0.50	0.52	ug/L
Lead	E200.8	1	0.018	0.10	0.11	ug/L
Arsenic	E200.8	1	0.11	0.30	1.9	ug/L
Total Hardness (As CaCO3)	SM2340B	1	0.0830	1.0	95	mg/L
Calcium Hardness (as CaCO3)	SM2340B	1	0.0830	0.50	54	mg/L
Nitrate as NO3	E300.0	1	0.077	0.50	4.8	mg/L
pH	SM4500HB	1	0.10	2.00	7.90	S.U.
Total Dissolved Solids	SM2540C	1	1	10	180	mg/L
Turbidity	E180.1	1	0.10	0.20	0.81	NTU



SAMPLE RESULTS

Report prepared for: David W Bess
David W Bess

Date Received: 06/13/13
Date Reported: 06/18/13

Client Sample ID:	House well	Lab Sample ID:	DWQ1306008-A-001A
Project Name/Location:	WaterQ Basic (Well Water for Dave Bess)	Sample Matrix:	Drinking Water
Project Number:			
Date/Time Sampled:	06/12/13 / 11:00		
Tag Number:	Drinking Water Sample for Dave Bess		

Parameters:	Analysis Method	Prep Date	Date Analyzed	DF	MDL	PQL	Results	Lab Qualifier	Unit	Analytical Batch	Prep Batch
Iron	E200.7	6/13/13	06/13/13	1	0.002	0.10	ND		mg/L	416020	8945
Manganese	E200.7	6/13/13	06/13/13	1	0.003	0.050	ND		mg/L	416020	8945
Boron	E200.7	6/13/13	06/13/13	1	0.001	0.020	0.048		mg/L	416020	8945

Parameters:	Analysis Method	Prep Date	Date Analyzed	DF	MDL	PQL	Results	Lab Qualifier	Unit	Analytical Batch	Prep Batch
Copper	E200.8	6/13/13	06/17/13	1	0.077	0.50	0.52		ug/L	416049	8962
Lead	E200.8	6/13/13	06/17/13	1	0.018	0.10	0.11		ug/L	416049	8962
Arsenic	E200.8	6/13/13	06/17/13	1	0.11	0.30	1.9		ug/L	416049	8962

Parameters:	Analysis Method	Prep Date	Date Analyzed	DF	MDL	PQL	Results	Lab Qualifier	Unit	Analytical Batch	Prep Batch
Total Hardness (As CaCO3)	SM2340B	6/13/13	06/13/13	1	0.0830	1.0	95		mg/L	416019	8943
Calcium Hardness (as CaCO3)	SM2340B	6/13/13	06/13/13	1	0.0830	0.50	54		mg/L	416019	8943



SAMPLE RESULTS

Report prepared for: David W Bess
David W Bess

Date Received: 06/13/13
Date Reported: 06/18/13

Client Sample ID:	House well	Lab Sample ID:	DWQ1306008-A-001B
Project Name/Location:	WaterQ Basic (Well Water for Dave Bess)	Sample Matrix:	Drinking Water
Project Number:			
Date/Time Sampled:	06/12/13 / 11:00		
Tag Number:	Drinking Water Sample for Dave Bess		

Parameters:	Analysis Method	Prep Date	Date Analyzed	DF	MDL	PQL	Results	Lab Qualifier	Unit	Analytical Batch	Prep Batch
Nitrite as N	E300.0	NA	06/13/13	1	0.095	0.50	ND		mg/L	416072	NA
Nitrate as NO3	E300.0	NA	06/13/13	1	0.077	0.50	4.8		mg/L	416072	NA

Parameters:	Analysis Method	Prep Date	Date Analyzed	DF	MDL	PQL	Results	Lab Qualifier	Unit	Analytical Batch	Prep Batch
pH	SM4500HB	NA	06/13/13	1	0.10	2.00	7.90		S.U.	416060	NA

Parameters:	Analysis Method	Prep Date	Date Analyzed	DF	MDL	PQL	Results	Lab Qualifier	Unit	Analytical Batch	Prep Batch
Total Dissolved Solids	SM2540C	NA	06/14/13	1	1	10	180		mg/L	416058	NA

Parameters:	Analysis Method	Prep Date	Date Analyzed	DF	MDL	PQL	Results	Lab Qualifier	Unit	Analytical Batch	Prep Batch
Turbidity	E180.1	NA	06/13/13	1	0.10	0.20	0.81		NTU	416059	NA



SAMPLE RESULTS

Report prepared for: David W Bess
David W Bess

Date Received: 06/13/13
Date Reported: 06/18/13

Client Sample ID:	House well	Lab Sample ID:	DWQ1306008-A-001C
Project Name/Location:	WaterQ Basic (Well Water for Dave Bess)	Sample Matrix:	Drinking Water
Project Number:			
Date/Time Sampled:	06/12/13 / 11:00		
Tag Number:	Drinking Water Sample for Dave Bess		

Parameters:	Analysis Method	Prep Date	Date Analyzed	DF	MDL	PQL	Results	Lab Qualifier	Unit	Analytical Batch	Prep Batch
Sulfide, Total	E376.1	NA	06/17/13	1	2	2.0	ND		mg/L	416062	NA



Laboratory Qualifiers and Definitions

DEFINITIONS:

Accuracy/Bias (% Recovery) - The closeness of agreement between an observed value and an accepted reference value.
Blank (Method/Preparation Blank) -MB/PB - An analyte-free matrix to which all reagents are added in the same volumes/proportions as used in sample processing. The method blank is used to document contamination resulting from the analytical process.
Duplicate - a field sample and/or laboratory QC sample prepared in duplicate following all of the same processes and procedures used on the original sample (sample duplicate, LCSd, MSD)
Laboratory Control Sample (LCS ad LCSd) - A known matrix spiked with compounds representative of the target analyte(s). This is used to document laboratory performance.
Matrix - the component or substrate that contains the analyte of interest (e.g., - groundwater, sediment, soil, waste water, etc)
Matrix Spike (MS/MSD) - Client sample spiked with identical concentrations of target analyte (s). The spiking occurs prior to the sample preparation and analysis. They are used to document the precision and bias of a method in a given sample matrix.
Method Detection Limit (MDL) - the minimum concentration of a substance that can be measured and reported with a 99% confidence that the analyte concentration is greater than zero
Practical Quantitation Limit (PQL) - a laboratory determined value at 2 to 5 times above the MDL that can be reproduced in a manner that results in a 99% confidence level that the result is both accurate and precise. PQLs reflect all preparation factors and/or dilution factors that have been applied to the sample during the preparation and/or analytical processes.
Precision (%RPD) - The agreement among a set of replicate/duplicate measurements without regard to known value of the replicates
Surrogate (S) or (Surr) - An organic compound which is similar to the target analyte(s) in chemical composition and behavior in the analytical process, but which is not normally found in environmental samples. Surrogates are used in most organic analysis to demonstrate matrix compatibility with the chosen method of analysis
Tentatively Identified Compound (TIC) - A compound not contained within the analytical calibration standards but present in the GCMS library of defined compounds. When the library is searched for an unknown compound, it can frequently give a tentative identification to the compound based on retention time and primary and secondary ion match. TICs are reported as estimates and are candidates for further investigation.
Units: the unit of measure used to express the reported result - mg/L and mg/Kg (equivalent to PPM - parts per million in <i>liquid</i> and <i>solid</i>), ug/L and ug/Kg (equivalent to PPB - parts per billion in <i>liquid</i> and <i>solid</i>), ug/m3 , mg.m3 , ppbv and ppmv (all units of measure for reporting concentrations in air), % (equivalent to 10000 ppm or 1,000,000 ppb), ug/Wipe (concentration found on the surface of a single Wipe usually taken over a 100cm2 surface)

LABORATORY QUALIFIERS:

<p>B - Indicates when the analyte is found in the associated method or preparation blank</p> <p>D - Surrogate is not recoverable due to the necessary dilution of the sample</p> <p>E - Indicates the reportable value is outside of the calibration range of the instrument but within the linear range of the instrument (unless otherwise noted) Values reported with an E qualifier should be considered as estimated.</p> <p>H- Indicates that the recommended holding time for the analyte or compound has been exceeded</p> <p>J- Indicates a value between the method MDL and PQL and that the reported concentration should be considered as estimated rather the quantitative</p> <p>NA - Not Analyzed</p> <p>N/A - Not Applicable</p> <p>NR - Not recoverable - a matrix spike concentration is not recoverable due to a concentration within the original sample that is greater than four times the spike concentration added</p> <p>R- The % RPD between a duplicate set of samples is outside of the absolute values established by laboratory control charts</p> <p>S- Spike recovery is outside of established method and/or laboratory control limits. Further explanation of the use of this qualifier should be included within a case narrative</p> <p>X -Used to indicate that a value based on pattern identification is within the pattern range but not typical of the pattern found in standards. Further explanation may or may not be provided within the sample footnote and/or the case narrative.</p>



Sample Receipt Checklist

Client Name: David W Bess

Project Name: WaterQ Basic (Well Water for Dave Bess)

Work Order No.: DWQ1306008

Date and Time Received: 6/13/2013 10:30

Received By: ng

Physically Logged By: ng

Checklist Completed By: ng

Carrier Name: FedEx

Chain of Custody (COC) Information

Chain of custody present? No
Chain of custody signed when relinquished and received? No
Chain of custody agrees with sample labels? No
Custody seals intact on sample bottles? Not Present

Sample Receipt Information

Custody seals intact on shipping container/cooler? Not Present
Shipping Container/Cooler In Good Condition? Yes
Samples in proper container/bottle? Yes
Samples containers intact? Yes
Sufficient sample volume for indicated test? Yes

Sample Preservation and Hold Time (HT) Information

All samples received within holding time? Yes
Container/Temp Blank temperature in compliance? No Temperature: 15 °C
Water-VOA vials have zero headspace? No VOA vials submitted
Water-pH acceptable upon receipt? N/A
pH Checked by: n/a pH Adjusted by: n/a

Samples received in a cooler at 15 deg C.



Login Summary Report

Client ID:	TL5834 David W Bess	QC Level:
Project Name:	WaterQ Basic (Well Water for Dave Bess)	TAT Requested: 3 day:25
Project # :		Date Received: 6/13/2013
Report Due Date:	6/18/2013	Time Received: 10:30

Comments: 3day TAT! Metals (Cu,Pb, B, Mn, As and Fe), Anions (NO2, NO3), pH, Turb, TDS, Hardness.

Client did not fill out the CoC, and has been contacted by email for sampling date/time, and for a CoC with a signature on it.
--KB 6/13/13.

Work Order # : **DWQ1306008**

<u>WO Sample ID</u>	<u>Client Sample ID</u>	<u>Collection Date/Time</u>	<u>Matrix</u>	<u>Scheduled Disposal</u>	<u>Sample On Hold</u>	<u>Test On Hold</u>	<u>Requested Tests</u>	<u>Subbed</u>
DWQ1306008-00 1A	House well	06/12/13 11:00	Drinking Water				DWQ_200.8 DWQ_200.7 DWQ_Hardness	
Sample Note: 3day TAT! Metals (Cu, Pb, B, Mn, As and Fe)								
DWQ1306008-00 1B	House well	06/12/13 11:00	Drinking Water				DWQ_Anions DWQ_TDS DWQ_Turb DWQ_pH	
Sample Note: Anions (NO2, NO3), pH, Turb, TDS.								
DWQ1306008-00 1C	House well	06/12/13 11:00	Drinking Water				DWQ_Sulfide	
Sample Note: Sulfide.								
DWQ1306008-00 2A	Irrigation well	06/12/13 11:50	Drinking Water				DWQ_200.8 DWQ_200.7 DWQ_Hardness	
DWQ1306008-00 2B	Irrigation well	06/12/13 11:50	Drinking Water				DWQ_Anions DWQ_pH DWQ_Turb DWQ_TDS	
DWQ1306008-00 2C	Irrigation well	06/12/13 11:50	Drinking Water				DWQ_Sulfide	



Rush Turnaround Services REQUEST FORM



Date | 6/13/13
 Company | Dave Bess
 Ordered By | _____
 Email | XXXXXXXXXXXXXXXXXXXXXXX
 (for Rush report)

Confirmation Number | TR13

For Torrent Lab Use Only	
Project Name	<u>XXXXXXXXXXXXXXXXXX</u>
Project Number	<u>XXXXXXXXXXXXXXXXXX</u>
Order ID	<u>DWQ1306008</u>
Order Taken By	<u>XXXXXXXXXXXXXXXXXX</u>
Accounting	_____

Project Details

TAT Requested
 (please check one)

- Same Day (2-8 Hours)
 One Day Noon
 2 Day Noon
 3 Day Noon
 4 Day Noon

Number of Samples | 2
 Matrix | Water
 (i.e., sample type: Is your sample soil, water, etc?)
 Analysis | Basic Well - no bacT, plus Fe

Weekend work required (refer to chart below for respective surcharge)

This request form may be a courtesy notice which reflects the rush services requested on the chain-of-custody. Please contact *Torrent Express*™ project management immediately at pm@torrentlab.com with the subject line "Rush TAT Cancellation" if you do not want the analysis(es) to proceed. Cancellation of a *Torrent Express*™ service may be subject to a cancellation fee.

In order to facilitate processing and scheduling, please notify Torrent Laboratory at least 24 hours in advance for any *Torrent Express*™ service. Sample(s) must be received or scheduled for pick-up before 5:00 pm in order to be processed that day; all samples received after 5:00 pm will be processed the following day.

All *Torrent Express*™ Same Day and Next Day rush services will be charged a \$250.00 minimum (excluding certain fees) plus the respective surcharge(s); all other *Torrent Express*™ rush services will be charged a \$150.00 minimum (excluding certain fees) plus the respective surcharge(s).

The following table briefly describes Torrent Laboratory's *Torrent Express*™ surcharge pricing structure, please refer to your company specific price list for the precise surcharges.

	Same Day	Next Day*	2 Day*	3 Day*	4 Day*
Regular Rush	300%	150%	75%	50%	37.5%
Noon	-	200%	100%	62.5%	50%
Weekend	300%	300%	-	-	-

*business day(s)



483 Sinclair Frontage Road
 Milpitas, CA 95035
 Phone: 408.263.5258
 FAX: 408.263.8293
 www.torrentlab.com

CHAIN OF CUSTODY

LAB WORK ORDER NO

DWQ1306008

NOTE: SHADED AREAS ARE FOR TORRENT LAB USE ONLY.

Company Name: Dave W. Bess			Location of Sampling:		
Address: 1115 Mt George Ave			Purpose: Drinking Water - WaterQ-Basic (Well Water)		
City: Napa	State: CA	Zip Code: 94558	Special Instructions / Comments: INCLUDE IRON IN THE METALS LIST. 3 DAY TAT!		
Telephone: 707.226.2539		FAX:			
REPORT TO: Dave Bess		SAMPLER:		P.O. #:	
				EMAIL: dave@dbesspumpandwell.com	

TURNAROUND TIME:

- 10 Work Days
 3 Work Days
 Noon - 1hr Day
 7 Work Days
 2 Work Days
 2-8 Hours
 5 Work Days
 1 Work Day
 Other

SAMPLE TYPE:

- Storm Water
 Waste Water
 Ground Water
 Soil
 Air
 Other

REPORT FORMAT:

- QC Level IV
 EDF
 Excel / EDD

ANALYSIS REQUESTED

LAB ID	CLIENT'S SAMPLE I.D.	DATE / TIME SAMPLED	MATRIX	# OF CONT	CONT TYPE	Cu, Pb, B, Mn, As, c	Hardness	TDS, pH, Turb.	Anions (NO2, NO3)	Sulfide	REMARKS
001A/B/C			DW			✓	✓	✓	✓	✓	
002A/B/C						✓	✓	✓	✓	✓	
RUSH 3 DAYS											

1	Relinquished By:	Print:	Date:	Time:	Received By:	Print:	Date:	Time: 10:30 AM
2	Relinquished By:	Print:	Date:	Time:	Received By:	Print:	Date:	Time:

Were Samples Received in Good Condition? Yes NO Samples on Ice? Yes NO Method of Shipment **Fed Ex** Sample seals intact? Yes NO N/A

NOTE: Samples are discarded by the laboratory 30 days from date of receipt unless other arrangements are made.

Log In By: **KB** Date: **6/13/13** Log In Reviewed By: _____ Date: _____ Page **1** of **1**

Appendix C-Water Quality Analysis, Sodhani Irrigation Well



David W Bess
David W Bess
1115 Mt George Ave
Napa, California 94558
Tel: 707-226-2539
Email: dave@dbesspumpandwell.com
RE: WaterQ Basic (Well Water for Dave Bess)

Work Order No.: DWQ1306008-B

Dear David W Bess:

Torrent Laboratory, Inc. received 1 sample(s) on June 13, 2013 for the analyses presented in the following Report.

All data for associated QC met EPA or laboratory specification(s) except where noted in the case narrative.

Torrent Laboratory, Inc. is certified by the State of California, ELAP #1991. If you have any questions regarding these test results, please feel free to contact the Project Management Team at (408)263-5258; ext 204.

Patti Sandrock
QA Officer

June 18, 2013

Date



Date: 6/18/2013

Client: David W Bess

Project: WaterQ Basic (Well Water for Dave Bess)

Work Order: DWQ1306008-B

CASE NARRATIVE

No issues encountered with the receiving, preparation, analysis or reporting of the results associated with this work order.

Observations:

Primary Contaminants- (Health)

The following constituents in the scope of analysis presented in this report were found to be outside of the EPA Federally established Maximum Contaminant Level (MCL) guidelines. Corrective action must be taken to control the failed constituents in order to ensure corrected levels will be below the MCLs.

Turbidity 57 NTU (MCL is 5.0)

Arsenic 130 ug/L (MCL is 10)

THIS WATER SHOULD NOT BE USED FOR DRINKING, BATHING or COOKING!

Secondary Contaminant - (Water Aesthetics)

No secondary contaminants in the scope of analysis presented in this report were found to be outside of the EPA Federally established Maximum Contaminant Level (MCL) guidelines (or recommended level where no MCLs exist).

This report is for Irrigation Well sample only and is labeled and stored as DWQ-1306008-B.

The House Well sample will be reported separately as DWQ-1306008-A.



Sample Result Summary

Report prepared for: David W Bess
David W Bess

Date Received: 06/13/13
Date Reported: 06/18/13
DWQ1306008-002

Irrigation well

<u>Parameters:</u>	<u>Analysis Method</u>	<u>DF</u>	<u>MDL</u>	<u>PQL</u>	<u>Results</u>	<u>Unit</u>
Iron	E200.7	1	0.002	0.10	1.6	mg/L
Manganese	E200.7	1	0.003	0.050	0.10	mg/L
Boron	E200.7	1	0.001	0.020	0.057	mg/L
Copper	E200.8	1	0.077	0.50	5.9	ug/L
Lead	E200.8	1	0.018	0.10	3.0	ug/L
Arsenic	E200.8	1	0.11	0.30	130	ug/L
Total Hardness (As CaCO3)	SM2340B	1	0.0830	1.0	80	mg/L
Calcium Hardness (as CaCO3)	SM2340B	1	0.0830	0.50	41	mg/L
pH	SM4500HB	1	0.10	2.00	7.57	S.U.
Total Dissolved Solids	SM2540C	1	1	10	180	mg/L
Turbidity	E180.1	10	1.0	2.0	57	NTU



SAMPLE RESULTS

Report prepared for: David W Bess
David W Bess

Date Received: 06/13/13
Date Reported: 06/18/13

Client Sample ID:	Irrigation well	Lab Sample ID:	DWQ1306008-B-002A
Project Name/Location:	WaterQ Basic (Well Water for Dave Bess)	Sample Matrix:	Drinking Water
Project Number:			
Date/Time Sampled:	06/12/13 / 11:50		
Tag Number:	Drinking Water Sample for Dave Bess		

Parameters:	Analysis Method	Prep Date	Date Analyzed	DF	MDL	PQL	Results	Lab Qualifier	Unit	Analytical Batch	Prep Batch
Iron	E200.7	6/13/13	06/13/13	1	0.002	0.10	1.6		mg/L	416020	8945
Manganese	E200.7	6/13/13	06/13/13	1	0.003	0.050	0.10		mg/L	416020	8945
Boron	E200.7	6/13/13	06/13/13	1	0.001	0.020	0.057		mg/L	416020	8945

Parameters:	Analysis Method	Prep Date	Date Analyzed	DF	MDL	PQL	Results	Lab Qualifier	Unit	Analytical Batch	Prep Batch
Copper	E200.8	6/13/13	06/17/13	1	0.077	0.50	5.9		ug/L	416049	8962
Lead	E200.8	6/13/13	06/17/13	1	0.018	0.10	3.0		ug/L	416049	8962
Arsenic	E200.8	6/13/13	06/17/13	1	0.11	0.30	130		ug/L	416049	8962

Parameters:	Analysis Method	Prep Date	Date Analyzed	DF	MDL	PQL	Results	Lab Qualifier	Unit	Analytical Batch	Prep Batch
Total Hardness (As CaCO3)	SM2340B	6/13/13	06/13/13	1	0.0830	1.0	80		mg/L	416019	8943
Calcium Hardness (as CaCO3)	SM2340B	6/13/13	06/13/13	1	0.0830	0.50	41		mg/L	416019	8943



SAMPLE RESULTS

Report prepared for: David W Bess
David W Bess

Date Received: 06/13/13
Date Reported: 06/18/13

Client Sample ID:	Irrigation well	Lab Sample ID:	DWQ1306008-B-002B
Project Name/Location:	WaterQ Basic (Well Water for Dave Bess)	Sample Matrix:	Drinking Water
Project Number:			
Date/Time Sampled:	06/12/13 / 11:50		
Tag Number:	Drinking Water Sample for Dave Bess		

Parameters:	Analysis Method	Prep Date	Date Analyzed	DF	MDL	PQL	Results	Lab Qualifier	Unit	Analytical Batch	Prep Batch
Nitrite as N	E300.0	NA	06/13/13	1	0.095	0.50	ND		mg/L	416072	NA
Nitrate as NO3	E300.0	NA	06/13/13	1	0.077	0.50	ND		mg/L	416072	NA

Parameters:	Analysis Method	Prep Date	Date Analyzed	DF	MDL	PQL	Results	Lab Qualifier	Unit	Analytical Batch	Prep Batch
pH	SM4500HB	NA	06/13/13	1	0.10	2.00	7.57		S.U.	416060	NA

Parameters:	Analysis Method	Prep Date	Date Analyzed	DF	MDL	PQL	Results	Lab Qualifier	Unit	Analytical Batch	Prep Batch
Total Dissolved Solids	SM2540C	NA	06/14/13	1	1	10	180		mg/L	416058	NA

Parameters:	Analysis Method	Prep Date	Date Analyzed	DF	MDL	PQL	Results	Lab Qualifier	Unit	Analytical Batch	Prep Batch
Turbidity	E180.1	NA	06/13/13	10	1.0	2.0	57		NTU	416059	NA



SAMPLE RESULTS

Report prepared for: David W Bess
David W Bess

Date Received: 06/13/13
Date Reported: 06/18/13

Client Sample ID:	Irrigation well	Lab Sample ID:	DWQ1306008-B-002C
Project Name/Location:	WaterQ Basic (Well Water for Dave Bess)	Sample Matrix:	Drinking Water
Project Number:			
Date/Time Sampled:	06/12/13 / 11:50		
Tag Number:	Drinking Water Sample for Dave Bess		

Parameters:	Analysis Method	Prep Date	Date Analyzed	DF	MDL	PQL	Results	Lab Qualifier	Unit	Analytical Batch	Prep Batch
Sulfide, Total	E376.1	NA	06/17/13	1	2	2.0	ND		mg/L	416062	NA



Laboratory Qualifiers and Definitions

DEFINITIONS:

Accuracy/Bias (% Recovery) - The closeness of agreement between an observed value and an accepted reference value.
Blank (Method/Preparation Blank) -MB/PB - An analyte-free matrix to which all reagents are added in the same volumes/proportions as used in sample processing. The method blank is used to document contamination resulting from the analytical process.
Duplicate - a field sample and/or laboratory QC sample prepared in duplicate following all of the same processes and procedures used on the original sample (sample duplicate, LCSD, MSD)
Laboratory Control Sample (LCS ad LCSD) - A known matrix spiked with compounds representative of the target analyte(s). This is used to document laboratory performance.
Matrix - the component or substrate that contains the analyte of interest (e.g., - groundwater, sediment, soil, waste water, etc)
Matrix Spike (MS/MSD) - Client sample spiked with identical concentrations of target analyte (s). The spiking occurs prior to the sample preparation and analysis. They are used to document the precision and bias of a method in a given sample matrix.
Method Detection Limit (MDL) - the minimum concentration of a substance that can be measured and reported with a 99% confidence that the analyte concentration is greater than zero
Practical Quantitation Limit (PQL) - a laboratory determined value at 2 to 5 times above the MDL that can be reproduced in a manner that results in a 99% confidence level that the result is both accurate and precise. PQLs reflect all preparation factors and/or dilution factors that have been applied to the sample during the preparation and/or analytical processes.
Precision (%RPD) - The agreement among a set of replicate/duplicate measurements without regard to known value of the replicates
Surrogate (S) or (Surr) - An organic compound which is similar to the target analyte(s) in chemical composition and behavior in the analytical process, but which is not normally found in environmental samples. Surrogates are used in most organic analysis to demonstrate matrix compatibility with the chosen method of analysis
Tentatively Identified Compound (TIC) - A compound not contained within the analytical calibration standards but present in the GCMS library of defined compounds. When the library is searched for an unknown compound, it can frequently give a tentative identification to the compound based on retention time and primary and secondary ion match. TICs are reported as estimates and are candidates for further investigation.
Units: the unit of measure used to express the reported result - mg/L and mg/Kg (equivalent to PPM - parts per million in liquid and solid), ug/L and ug/Kg (equivalent to PPB - parts per billion in liquid and solid), ug/m3 , mg.m3 , ppbv and ppmv (all units of measure for reporting concentrations in air), % (equivalent to 10000 ppm or 1,000,000 ppb), ug/Wipe (concentration found on the surface of a single Wipe usually taken over a 100cm2 surface)

LABORATORY QUALIFIERS:

<p>B - Indicates when the analyte is found in the associated method or preparation blank</p> <p>D - Surrogate is not recoverable due to the necessary dilution of the sample</p> <p>E - Indicates the reportable value is outside of the calibration range of the instrument but within the linear range of the instrument (unless otherwise noted) Values reported with an E qualifier should be considered as estimated.</p> <p>H- Indicates that the recommended holding time for the analyte or compound has been exceeded</p> <p>J- Indicates a value between the method MDL and PQL and that the reported concentration should be considered as estimated rather the quantitative</p> <p>NA - Not Analyzed</p> <p>N/A - Not Applicable</p> <p>NR - Not recoverable - a matrix spike concentration is not recoverable due to a concentration within the original sample that is greater than four times the spike concentration added</p> <p>R- The % RPD between a duplicate set of samples is outside of the absolute values established by laboratory control charts</p> <p>S- Spike recovery is outside of established method and/or laboratory control limits. Further explanation of the use of this qualifier should be included within a case narrative</p> <p>X -Used to indicate that a value based on pattern identification is within the pattern range but not typical of the pattern found in standards. Further explanation may or may not be provided within the sample footnote and/or the case narrative.</p>



Sample Receipt Checklist

Client Name: David W Bess

Project Name: WaterQ Basic (Well Water for Dave Bess)

Work Order No.: DWQ1306008

Date and Time Received: 6/13/2013 10:30

Received By: ng

Physically Logged By: ng

Checklist Completed By: ng

Carrier Name: FedEx

Chain of Custody (COC) Information

Chain of custody present? No
Chain of custody signed when relinquished and received? No
Chain of custody agrees with sample labels? No
Custody seals intact on sample bottles? Not Present

Sample Receipt Information

Custody seals intact on shipping container/cooler? Not Present
Shipping Container/Cooler In Good Condition? Yes
Samples in proper container/bottle? Yes
Samples containers intact? Yes
Sufficient sample volume for indicated test? Yes

Sample Preservation and Hold Time (HT) Information

All samples received within holding time? Yes
Container/Temp Blank temperature in compliance? No Temperature: 15 °C
Water-VOA vials have zero headspace? No VOA vials submitted
Water-pH acceptable upon receipt? N/A
pH Checked by: n/a pH Adjusted by: n/a

Samples received in a cooler at 15 deg C.



Login Summary Report

Client ID:	TL5834 David W Bess	QC Level:	
Project Name:	WaterQ Basic (Well Water for Dave Bess)	TAT Requested:	3 day:25
Project # :		Date Received:	6/13/2013
Report Due Date:	6/18/2013	Time Received:	10:30

Comments: 3day TAT! Metals (Cu,Pb, B, Mn, As and Fe), Anions (NO2, NO3), pH, Turb, TDS, Hardness.

Client did not fill out the CoC, and has been contacted by email for sampling date/time, and for a CoC with a signature on it. --KB 6/13/13.

Work Order # : ***DWQ1306008***

<u>WO Sample ID</u>	<u>Client Sample ID</u>	<u>Collection Date/Time</u>	<u>Matrix</u>	<u>Scheduled Disposal</u>	<u>Sample On Hold</u>	<u>Test On Hold</u>	<u>Requested Tests</u>	<u>Subbed</u>
DWQ1306008-00 1A	House well	06/12/13 11:00	Drinking Water				DWQ_200.8 DWQ_200.7 DWQ_Hardness	
Sample Note: 3day TAT! Metals (Cu, Pb, B, Mn, As and Fe)								
DWQ1306008-00 1B	House well	06/12/13 11:00	Drinking Water				DWQ_Anions DWQ_pH DWQ_TDS DWQ_Turb	
Sample Note: Anions (NO2, NO3), pH, Turb, TDS.								
DWQ1306008-00 1C	House well	06/12/13 11:00	Drinking Water				DWQ_Sulfide	
Sample Note: Sulfide.								
DWQ1306008-00 2A	Irrigation well	06/12/13 11:50	Drinking Water				DWQ_200.8 DWQ_200.7 DWQ_Hardness	
DWQ1306008-00 2B	Irrigation well	06/12/13 11:50	Drinking Water				DWQ_Anions DWQ_pH DWQ_Turb DWQ_TDS	
DWQ1306008-00 2C	Irrigation well	06/12/13 11:50	Drinking Water				DWQ_Sulfide	



Rush Turnaround Services REQUEST FORM



Date | 6/13/13
 Company | Dave Bess
 Ordered By | _____
 Email | XXXXXXXXXXXXXXXXXXXXXXX
 (for Rush report)

Confirmation Number | TR13

For Torrent Lab Use Only
 Project Name | XXXXXXXXXXXXXXXXXXXX
 Project Number | XXXXXXXXXXXXXXXXXXXX
 Order ID | DWQ1306008
 Order Taken By | XXXXXXXXXXXXXXXXXXXX
 Accounting | _____

Project Details

TAT Requested
 (please check one)

- Same Day (2-8 Hours)
 One Day Noon
 2 Day Noon
 3 Day Noon
 4 Day Noon

Number of Samples | 2

Matrix | Water
 (i.e., sample type: Is your sample soil, water, etc?)

Analysis | Basic Well - no bact, plus Fe

Weekend work required (refer to chart below for respective surcharge)

This request form may be a courtesy notice which reflects the rush services requested on the chain-of-custody. Please contact *Torrent Express* project management immediately at pm@torrentlab.com with the subject line "Rush TAT Cancellation" if you do not want the analysis(es) to proceed. Cancellation of a *Torrent Express* service may be subject to a cancellation fee.

In order to facilitate processing and scheduling, please notify Torrent Laboratory at least 24 hours in advance for any *Torrent Express* service. Sample(s) must be received or scheduled for pick-up before 5:00 pm in order to be processed that day; all samples received after 5:00 pm will be processed the following day.

All *Torrent Express* Same Day and Next Day rush services will be charged a \$250.00 minimum (excluding certain fees) plus the respective surcharge(s); all other *Torrent Express* rush services will be charged a \$150.00 minimum (excluding certain fees) plus the respective surcharge(s).

The following table briefly describes Torrent Laboratory's *Torrent Express* surcharge pricing structure, please refer to your company specific price list for the precise surcharges.

	Same Day	Next Day*	2 Day*	3 Day*	4 Day*
Regular Rush	300%	150%	75%	50%	37.5%
Noon	-	200%	100%	62.5%	50%
Weekend	300%	300%	-	-	-

*business day(s)



483 Sinclair Frontage Road
 Milpitas, CA 95035
 Phone: 408.263.5258
 FAX: 408.263.8293
 www.torrentlab.com

CHAIN OF CUSTODY

LAB WORK ORDER NO

DWG1306008

NOTE: SHADED AREAS ARE FOR TORRENT LAB USE ONLY.

Company Name: Dave W. Bess			Location of Sampling:		
Address: 1115 Mt George Ave			Purpose: Drinking Water - WaterQ-Basic (Well Water)		
City: Napa	State: CA	Zip Code: 94558	Special Instructions / Comments: INCLUDE IRON IN THE METALS LIST. 3 DAY TAT!		
Telephone: 707.226.2539		FAX:			
REPORT TO: Dave Bess		SAMPLER:		P.O. #:	
EMAIL: dave@dbesspumpandwell.com					

TURNAROUND TIME:

- 10 Work Days
- 3 Work Days
- Noon - Intl Day
- 7 Work Days
- 2 Work Days
- 2 - 8 Hours
- 5 Work Days
- 1 Work Day
- Other

SAMPLE TYPE:

- Storm Water
- Waste Water
- Ground Water
- Soil
- Air
- Other

REPORT FORMAT:

- QC Level IV
- EDF
- Excel / EDD

ANALYSIS REQUESTED

LAB ID	CLIENT'S SAMPLE I.D.	DATE / TIME SAMPLED	MATRIX	# OF CONT	CONT TYPE	Cu, Pb, B, Mn, As, c	Hardness	TDS, pH, Turb,	Anions (NO ₂ , NO ₃)	Sulfide	REMARKS
001A/B/C			DW			✓	✓	✓	✓	✓	
002A/B/C						✓	✓	✓	✓	✓	

RUSH 3 DAYS

1	Relinquished By:	Print:	Date:	Time:	Received By:	Print:	Date:	Time: 10:30 AM
2	Relinquished By:	Print:	Date:	Time:	Received By:	Print:	Date:	Time:

Were Samples Received in Good Condition? Yes NO Samples on Ice? Yes NO Method of Shipment **Fed Ex** Sample seals intact? Yes NO N/A
 NOTE: Samples are discarded by the laboratory 30 days from date of receipt unless other arrangements are made. Page 1 of 1
 Log In By: **KB** Date: **6/13/13** Log In Reviewed By: _____ Date: _____

Appendix D-Napa County Well Permit, Project Well

HEALTH DEPT. USE ONLY

FEE: 12.00

DATE: 2-20-74

RECEIPT NO: 0900

BY: N. Ettel

RECEIVED # 22-080-04

NAPA COUNTY HEALTH DEPARTMENT
DIVISION OF ENVIRONMENTAL HEALTH

MAY 7 1974

APPLICATION & PERMIT TO CONSTRUCT

A WATER WELL
(ORDINANCE #)

DIVISION OF
ENVIRONMENTAL HEALTH

NAME Callow ADDRESS St. Helena Hwy N DATE 2-20-74
(Owner) (Job Location)

NAME Walter Pittela ADDRESS 1541 Mark West Springs Rd.
(Well Driller) (Santa Rosa)

TYPE OF WORK: NEW WELL RECONDITIONING DEEPENING
TEST HOLES DESTROYING OTHER
TYPE I PERMIT TYPE II PERMIT FEE

PROPOSED USE: DOMESTIC IRRIGATION INDUSTRIAL MUNICIPAL
TEST WELL OTHER

Sewage Disposal On Site (Existing or Proposed) Public Individual Private
Distance from well to any part of nearest sewage disposal system 1871+ feet.
(Sketch of site to accompany application.)

TYPE OF EQUIPMENT TO BE USED: Rotary Cable Hand Dug Other

CONSTRUCTION PROPOSED: Diameter of casing 8" Material steel Annular Space: Size 2"
Sealed with: Concrete Grout Neat Cement Puddled Clay Other
Conductor Casing: Yes No Material
Chlorination By: Owner Pump Co Driller

Walter Pittela
(SIGNATURE OF APPLICANT)

2-20-74
(DATE)

NOTICE TO DRILLER: COMPLETE THIS PORTION AND PROVIDE OWNER WITH THIS COPY.

CASING
2 5/8 - 8"
CONSTRUCTION
Total Depth 250 Ft.
Surface Seal to 25 Ft.
Any Stratas sealed: Yes No
If yes, depth of Stratas
From Ft. to Feet
From Ft. to Feet
Perforations
From 87 Ft. to 130 Feet
From 160 Ft. to 190 Feet
From 210 Ft. to 250 Feet
WATER LEVELS
First water at 70 Feet
Static level at 40 Feet
WELL TESTS
How performed Bailer
Yield 30 GPM with 80 Feet
Drawdown Ft. after 1 Hrs.

WELL LOG
(Formation; describe by color, size of material, structure)
Ft. to Ft.

0-20	Red clay.		
20-30	clay + small boulders	210-240	Brown ash.
30-40	Loose boulders	240-245	Brown ash.
40-47	clay.	245-250	Brown ash.
47-60	broken basalt		
60-85	clay.		
85-95	broken basalt		
95-110	brown ash		
110-125	broken basalt		
125-145	Brown ash.		
145-160	hard clay + gravel		
160-180	ash + gravel		
180-188	clay.		
188-200	Brown rock.		
200-210	clay + boulders		

Signed: Walter Pittela
License # 228 1049

Appendix E-Well Completion Report, Sodhani Irrigation Well

Owner's Copy

WELL COMPLETION REPORT

Refer to Instructions Pamphlet

Page 1 of 2

Owner's Well No. _____

No. **719746**

Date Work Began 7/2/99 Ended 7/14/99

Local Permit Agency NAPA CO. ENVIRONMENTAL MANAGEMENT

Permit No. 96-10399 Permit Date 10/8/99

STATE WELL NO./STATION NO. _____

LATITUDE _____ LONGITUDE _____

APPROXIMATE _____

ORIENTATION (±)			DRILLING METHOD	FLUID	WELL OWNER
<input checked="" type="checkbox"/> VERTICAL <input type="checkbox"/> HORIZONTAL			<u>MUD ROTARY</u>	<u> Bentonite </u>	Name <u>HAROLD & CAROL GREEN</u>
ANGLE _____ (SPECIFY)			DESCRIPTION _____	Mailing Address <u>3283 St. Helena Hwy</u>	
Describe interval, grain size, color, etc.				City <u>St. Helena, CA</u> STATE <u>CA</u> ZIP _____	
0	3	Clay		WELL LOCATION	
3	10	Boulders		Address <u>3283 St. Helena Hwy</u>	
10	26	Gravels		City <u>St. Helena, CA</u>	
26	48	HARD Cobbles		County <u>NAPA</u>	
48	59	Coarse sand		APN Book <u>22</u> Page <u>080</u> Parcel <u>04</u>	
59	76	Clayey sand		Township _____ Range _____ Section _____	
76	85	Hard multi-colored volcanic rock		Latitude _____ Longitude _____	
85	94	Loose volcanic rock & some clay		LOCATION SKETCH NORTH _____ WEST _____ SOUTH _____ EAST _____	
94	96	Clay		ACTIVITY (±)	
96	105	Coarse sand & volcanic rock with small amount of clay		<input checked="" type="checkbox"/> NEW WELL MODIFICATION/REPAIR _____ Deeper _____ Other (Specify) _____	
105	111	Hard & fractured volcanic rock		DESTROY (Describe Percolator and Material Under GEOLOGIC LOG)	
111	117	Sandy clayey ash		PLANNED USES (±)	
117	121	Hard fractured volcanic rock		WATER SUPPLY _____	
121	124	Clay and ash		<input checked="" type="checkbox"/> Domestic _____ Public _____ <input checked="" type="checkbox"/> Irrigation _____ Industrial _____	
124	128	Hard fractured volcanic rock		MONITORING _____	
128	130	Clay & ash		TEST WELL _____	
130	142	Hard fractured volcanic rock		CATHODIC PROTECTION _____	
142	148	Dry ash		HEAT EXCHANGE _____	
148	162	Hard fractured volcanic rock		DIRECT FURN _____	
162	164	Clay and ash		PASSAGE _____	
164	167	Hard fractured volcanic rock		VAPOR EXTRACTION _____	
167	196	Clay and ash		SPARGING _____	
196	198	Hard fractured volcanic rock		REMEDICATION _____	
198	214	Clay and ash		OTHER (SPECIFY) _____	
214	218	Hard fractured volcanic rock		WATER LEVEL & YIELD OF COMPLETED WELL	
218	251	Volcanic conglomerate		DEPTH TO FIRST WATER _____ (ft) BELOW SURFACE	
TOTAL DEPTH OF BOREHOLE <u>458</u> (feet)				DEPTH OF STATIC WATER LEVEL <u>21</u> (ft) & DATE MEASURED <u>7/14/99</u>	
TOTAL DEPTH OF COMPLETED WELL <u>458</u> (feet)				ESTIMATED YIELD <u>18</u> (GPM) & TEST TYPE <u>BATH</u>	
				TEST LENGTH <u>1 1/2</u> (hrs) TOTAL DRAWDOWN <u>97</u> (ft)	
				* May not be representative of a well's long-term yield.	

DEPTH FROM SURFACE ft to ft	BORE-HOLE DIA. (inches)	CASING (S)				ANNULAR MATERIAL					
		TYPE (±)	MATERIAL GRADE	INTERNAL DIAMETER (inches)	GAUGE OR WALL THICKNESS	SLOT SIZE IF ANY (inches)	DEPTH FROM SURFACE ft to ft	CEMENT (±)	BENTONITE (±)	FILO (±)	FILLER PACK (TYPE/QT)
0 - 316	12 1/4						0 - 26	X			
316 - 458	10 5/8						26 - 458			X	3/8 PEA GRU
+ 2 - 458		K	PVC/P490	6"	CL200						
78 - 98		X									
138 - 158		K									

SEE NEXT PAGE TO CONTINUE MICR PERFORATIONS

ATTACHMENTS (±)

- Geologic Log
- Well Construction Diagram
- Geophysical Logs
- Soil/Water Chemical Analysis
- Other _____

ATTACH ADDITIONAL INFORMATION, IF IT EXISTS

CERTIFICATION STATEMENT

I, the undersigned, certify that this report is complete and accurate to the best of my knowledge and belief.

NAME WEEKS DRILLING AND PUMP COMPANY by Ward Thompson

PERSON, FIRM, OR CORPORATION, TYPED OR PRINTED

P.O. Box 176 STAGWOOD, CA 95473

Address City State ZIP

Signed [Signature] Date Signed 7/15/99 Well Completion Report Number 177681

Owner's Copy

Page 2 of 2

Owner's Well No. _____

Date Work Began 7/2/99, Ended 7/14/99

Local Permit Agency NAPA CO. ENVIRONMENTAL MANAGEMENT

Permit No. 96-10399, Permit Date 10/8/99

WELL COMPLETION REPORT

Refer to Instruction Pamphlet

No. 719747

STATE WELL NO./STATION NO.	
LATITUDE	LONGITUDE
APN/TRS/OTHER	

GEOLOGIC LOG

ORIENTATION (±)		DRILLING METHOD	FLUID
<input checked="" type="checkbox"/> VERTICAL	<input type="checkbox"/> HORIZONTAL	MUD ROTARY	Bent.
DEPTH FROM SURFACE		DESCRIPTION	
ft. to ft.	Describe material, grain size, color, etc.		
251	272	Hard fractured volcanic rock	
262	271	Volcanic conglomerate	
271	274	HARD volcanic rock	
274	283	Clay and ash	
283	288	Hard fractured volcanic rock	
288	293	Coarse sand	
293	369	Hard multi-colored volcanic rock with seams of clay	
369	382	Clayee ash	
382	388	Hard and very fractured black and red volcanic rock	
388	392	Clay and ash	
392	412	Coarse sands & rock ledges	
412	420	Clay and ash	
420	449	Coarse sand and rock ledges	
449	458	Stiff clay	

WELL OWNER

Name: HAROLD & CAROL GREEN
 Mailing Address: 3283 St. Helena Hwy
 City: St. Helena, CA STATE ZIP
 WELL LOCATION
 Address: 3283 St. Helena Hwy
 City: St. Helena, CA
 County: NAPA
 APN Book 22 Page 080 Parcel 04
 Township Range Section
 Latitude Longitude

LOCATION SKETCH

ACTIVITY (±)

NEW WELL

MODIFICATION/REPAIR

___ Deepen

___ Other (Specify)

DISTRIB (Describe Procedures and Materials Under GEOLOGIC LOG)

PLANNED USES (±)

WATER SUPPLY

___ Domestic ___ Public

Irrigation ___ Industrial

MONITORING

___ TEST WELL

GATHERING PROTECTION

___ HEAT EXCHANGE

___ DIRECT PUSH

___ INJECTION

___ VAPOR EXTRACTION

___ SPARKING

___ REMEDIATION

___ OTHER (SPECIFY)

WEST EAST

WATER LEVEL & YIELD OF COMPLETED WELL

DEPTH TO FIRST WATER _____ (ft) BELOW SURFACE

DEPTH OF STATIC WATER LEVEL: SEE PAGE 1 (ft) & DATE MEASURED _____

ESTIMATED YIELD _____ (GPM) & TEST TYPE _____

TEST LENGTH _____ (hrs) TOTAL DRAWDOWN _____ (ft)

* May not be representative of a well's long-term yield.

DEPTH FROM SURFACE	BONE-HOLE DIA. (Inches)	TYPE (±)				CASING (S)			
		BLANK	SCREEN	PIPE	OTHER	MATERIAL / GRADE	INTERNAL DIAMETER (Inches)	GAUGE OR WALL THICKNESS	SLOT SIZE IF ANY (Inches)
218	238	X							.032
278	298	X							.032
338	358	X							.032
398	418	X							.032
438	458	X							.032

DEPTH FROM SURFACE	ANNULAR MATERIAL			
	CEMENT (±)	BENTONITE (±)	FILL (±)	FILTER PACK (TYPE/SIZE)
SEE PREVIOUS PAGE 1				

ATTACHMENTS (±)

___ Geologic Log

___ Well Construction Diagram

___ Geophysical Log(s)

___ Soil/Water Chemical Analysis

___ Other _____

ATTACH ADDITIONAL INFORMATION, IF IT EXISTS.

CERTIFICATION STATEMENT

I, the undersigned, certify that this report is complete and accurate to the best of my knowledge and belief.

NAME: WEEKS DRILLING AND PUMP COMPANY by Ward Thompson
 (PERSON, FIRM OR CORPORATION) (TYPE OR PRINT)

P.O. Box 176 Sebastopol, CA 95473

ADDRESS: _____ CITY: _____ STATE: _____ ZIP: _____

Signature: *Ward Thompson* DATE SIGNED: 7/15/99 WELL DRILLER/AUTHORIZED REPRESENTATIVE DATE REPORT: 7/15/99 F. 57 LICENSE NUMBER: 177681

Appendix F-Soil Data for Project Recharge Zone

Map Unit Symbol	Hydrologic Group	Soil Name	Area (acres)
110	B	Boomer-Forward-Felta complex, 30 to 50 percent slopes	1.33
109	B	Boomer gravelly loam, 30 to 50 percent slopes	16.57
108	B	Boomer gravelly loam, 15 to 30 percent slopes	31.12
100	B	Aiken loam, 2 to 15 percent slopes	3.10
139	C	Forward gravelly loam, 9 to 30 percent slopes	0.03

Appendix G-Estimated Annual PET for Project Recharge Zone

Land use acreage for Area 2

Area		52.2								
FID	Land USE	Area (acres)	Total acres Land use	Percent Total Recharge Area	Annual PET from L&S Water Balance (inches)	Area-Weighted PET (inches)				
7	Forest	16.16	16.48	32%	19.9	6.29				
14	Forest	0.32								
1	Forest Mix	5.30								
17	Forest Mix	0.45								
22	Forest Mix	0.59								
27	Forest Mix	14.64								
9	Oak/Forest	0.61	21.59	41%	19.9	8.23				
11	Grassland	0.66	1.26	2%	10.6	0.26				
12	Grassland	0.01								
13	Grassland	0.08								
16	Grassland	0.19								
26	Grassland	0.05								
29	Grassland	0.05								
30	Grassland	0.12								
31	Grassland	0.06								
32	Grassland	0.04								
3	Orchard	0.30					0.30	1%	39.2	0.22
10	shrubland	0.10					0.16	0%	14.9	0.05
28	Shrubland	0.06								
0	Urban/Developed	0.17	2.43	5%	12.4	0.58				
5	Urban/Developed	0.46								
8	Urban/Developed	0.26								
15	Urban/Developed	0.34								
19	Urban/Developed	0.57								
23	Urban/Developed	0.14								
24	Urban/Developed	0.24								
25	Urban/Developed	0.15								
33	Urban/Developed	0.10								
2	Vineyard	0.25					9.95	19%	22.5	4.29
4	Vineyard	0.92								
6	Vineyard	1.30								
18	Vineyard	6.50								
21	Vineyard	0.98								
Total		52.2		100%		19.92				
					PET (acre-feet)	86.60				

Appendix H-Supplemental Estimate of Distance Between Wells

To assist in documenting the project domestic well location relative to the neighboring well to the south GPS data points were taken by the Project property owner on May 25th 2015 using the "GPS Tour" application on his iPhone 6 Plus. The average RMSE in horizontal accuracy for the GPS system installed in a 3G iPhone is stated to be 9 m (Zandbergen, 2009). The latitude and longitude in decimal degrees for each well was recorded and then plotted in the GCS_WGS_1984 coordinate system using simple methods in ArcGIS (see Figure below). The points were then projected into NAD_1983_StatePlane_California_II_FIPS_0402_Feet coordinate system to match the exact coordinate system of the ArcMap document being used to ensure the most accurate georeferencing of the points. Well locations do not match exactly to the locations shown on the 2007 aerial photo and to those mapped in the field; nevertheless, the relative distances between the points are similar to those mapped using field techniques mentioned earlier in this analysis. This discrepancy can be attributed to the relatively large horizontal accuracy of the iPhone GPS. The measured distance between the two well points taken with the iPhone was 508.7 feet, quite close to the 504 ft determined by previous methods.

Zandbergen, P. A., 2009. Accuracy of iPhone Locations: A Comparison of Assisted GPS, WiFi and Cellular Positioning. *Transactions in GIS*, 2009, 13(s1): 5–26. Blackwell Publishing Ltd.