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Wastewater Feasibility Study

WASTEWATER FEASIBILITY STUDY

CONN CREEK WINERY

8711 Silverado Trail St. Helena, California APN 030-120-032



Revised: November 17, 2020

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Conn Creek Winery Wastewater Feasibility Study July 10, 2019

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PROJECT OVERVIEW & SITE DESCRIPTION

Conn Creek Winery, located at 8711 Silverado Trail in St. Helena (APN 030-120-032), is applying for a use permit modification to Use Permit 95532-MOD to increase the number of employees and allow pairing of food prepared offsite with wine tasting. There are no proposed changes to the approved wine production of 260,000 gallons per year of fruit crushed on site and 590,000 gallons of bulk wine processed, or additional changes to the marketing and visitation plan. The site is a 5.99-acre parcel in an agricultural area on Silverado Trail. Refer to Enclosure A for a vicinity map and Enclosure B for an overall site plan. The topography consists of gently sloping vineyards and the property is located wholly within the 100-year floodplain and partially within the 100-year floodway. The site plan in Enclosure B includes the floodway boundary. The existing sanitary sewage (SS) system is located to the north of the winery building, with a process wastewater (PW) treatment pond located to the east of the winery.

The SS system will be improved to accommodate additional SS flows from employees. Summit Engineering has prepared the following Wastewater Feasibility Study to assess the feasibility of treating and disposing of the increase in SS associated with the proposed increase in employees, visitation, and marketing events.

WINERY PROCESS WASTEWATER SYSTEM

No changes are proposed to the existing PW system, land application area, or total vineyard onsite as approved per P18-00007-VMM, as the facility is not proposing any increase to the permitted wine production capacity. The pond water balance prepared to support Use Permit application P18-00007-VMM has been provided for reference. Note that the total outdoor processing area is reduced to 0.33 acres, rather than the original 0.39 acres estimated at that time. This leads to a net decrease in effluent land application from what was previously approved.

SANITARY SEWAGE TREATMENT AND DISPOSAL SYSTEM

OVERVIEW

Separate systems are used for sanitary sewage and process wastewater treatment. The existing SS treatment system at the site was approved via permits 92-12720 and 92-12721 with a design flow of 750 gallons per day (GPD). Refer to Enclosure C for the as-built wastewater disposal system plans of the existing SS treatment and system. Domestic wastewater from the winery flows via gravity into septic tanks prior to being pumped to the pressure distribution (PD) leachfield.

An existing, separate PW disposal PD leachfield is installed to handle treated PW effluent after the pond when it is not used for vineyard irrigation, designed for 9,300 GPD. A minor modification to the facility's use permit, P18-00007 allowed for the diversion of stormwater to the PW treatment pond, allowed by Napa County if the collected stormwater is beneficially reused for irrigation. This would require abandoning the existing 9,300 GPD PD leachfield for PW disposal.

To accommodate the increased SS generated from additional employees, and the increases in Napa County estimated SS associated with daily visitation and events, converting leachlines from the PW PD system is

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proposed. The total proposed SS system, after improvements, will be sized for a peak daily flow of up to 1,290 GPD.

The existing system and proposed upgrades are discussed in greater detail in the subsequent sections of this wastewater feasibility study.

SANITARY SEWAGE CHARACTERISTICS

SS will consist primarily of wastewater generated from restrooms and tasting room facilities. Typical SS characteristics are as summarized below:

Characteristic	<u>Units</u>	Raw Wastewater ¹ <u>Range</u>
BODs	mg/L	110 - 220
Grease	mg/L	50-100
Total Suspended Solids (TSS)	mg/L	100 - 220
Volatile Suspended Solids	mg/L	80 - 165
Total Dissolved Solids (TDS)	mg/L	250 - 500
Nitrogen	mg/L	20 - 40
Nitrate	mg/L	0
Phosphorous	mg/L	4 - 8
Alkalinity (CaCO₃)	mg/L	50 - 100
Chloride	mg/L	30 - 50
Sulfate	mg/L	20 - 30

¹Typical composition of untreated domestic wastewater, Metcalf & Eddy, "Wastewater Engineering, Third Edition", 1991

SANITARY SEWAGE DESIGN FLOWS

Sanitary sewage at Conn Creek Winery will consist of typical wastewater generated from restrooms, tasting room, and hospitality functions. The estimated peak day flows associated with the proposed increase in employees, visitation and events are provided below.

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SANITARY SEWAGE							
Average Day w/o Major Event - Non-ha	<u>arvest</u>						
Employee (full-time)	20	х	15	gpcd	=	300	gal/day
Employee (part-time)	1	х	15	gpcd	=	15	gal/day
Tasting Visitors	70	х	3	gpcd	=	210	gal/day
Private Marketing Event w/ Meal	15	х	5	gpcd	=	75	gal/day
Total					=	600	gal/day
					=	600	gal/day
Peak Tasting Day Harvest w/Event							
Employee (full-time)	20	х	15	gpcd	=	300	gal/day
Employee (part-time)	1	х	15	gpcd	=	15	gal/day
Tasting Visitors	225	х	3	gpcd	=	675	gal/day
Garden Event	60	х	5	gpcd	=	300	gal/day
Total					=	1,290	gal/day
DESIGN FLOW					=	1,290	gal/day

The average daily visitation is assumed to be 70 wine tasting guests per day, estimated based on the 500 weekly guests allowed by previously approved Use Permits. Similarly, peak wine tasting visitation is assumed to be 225 guests per day based on earlier Use Permits. All food served at events is currently prepared offsite and catered, with minimal onsite handling of food or dishwashing. Any water use associated with plating or serving prepared food is expected to be captured within the 3 gallons per person estimate for wine tasting. The facility proposes to continue utilizing offsite catered food prep, so a total of 5 gallons of SS per person at special events with food is proposed. Therefore, the SS system will be designed to handle the peak daily SS flow of up to 1,290 gal/day.

KITCHEN SS DESIGN FLOWS

No onsite food prep is anticipated, therefore a grease interceptor should not be required.

SITE EVALUATION RESULTS

The original PD disposal system sizing was based on a site evaluation performed on March 16, 1999 by Summit Engineering and Napa County representative Christine Secheli. During the evaluation, acceptable soil to a depth of 66" below grade was observed, with a percolation rate of 1-3 minutes per inch (MPI). Based on Napa County Alternative Sewage Treatment System Standards, 1-3 MPI corresponds to an application rate of 1.2 gallons per square foot per day. This application rate was used to size the original PD system, and will be utilized in confirming the total acceptable trench sidewall area for the reconfigured SS disposal system.

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SANITARY SEWAGE CONVEYANCE, TREATMENT AND DISPOSAL

Septic Tank Treatment

The existing and proposed winery SS treatment and disposal system improvements will have the components described below. Refer to Enclosures B & D for the Overall Site Plan and proposed SS system schematic.

- 1) <u>Gravity Collection System</u> The existing gravity collection system is assumed to provide low maintenance and no infiltration or exfiltration. Piping is assumed to be compatible with sanitary sewage and satisfy Uniform Plumbing Code and local requirements.
- 2) <u>Septic Tanks with Effluent Filter</u> The required septic tank size for the increased winery SS flows was determined by evaluating sizing recommendations based on the Uniform Plumbing Code (UPC) formula as shown below:

Uniform Plumbing Code Method:

 $Volume = 1,125 + 0.75 \times Flow Rate$

 $Volume = 1,125 + 0.75 \times 1,290 \ qpd$

 $Volume = 2,092 \ gallons$

The existing 3,000-gallon septic tank will provide adequate tankage when sized per the UPC requirements. Removal of solids in the septic tank will help to reduce BOD loads on the system and minimize the frequency of sludge removal in aerobic systems. An effluent filter will also be provided on the outlet of the final septic tank to remove additional suspended solids which do not settle out in the tank.

- 3) <u>Pressure Distribution Disposal</u> The existing SS dosing tank will be utilized, with pump operation and dosing settings confirmed prior to system expansion. The existing SS PD leachfield zone, along with a portion of the PW PD leachfield proposed to be abandoned will be utilized to provide a combined disposal capacity of a minimum 1,290 GPD.
- 4) <u>Flow measurement</u> Either new or existing (if suitable) inline flow measurement devices will be utilized to measure flows from the dosing tank compartment to the PD leachfield.

PD Leachfield Disposal

The soil application rate, according to Napa County Alternative Sewage Treatment System Standards is 1.2 gal/SF/day based on the site evaluation results discussed above. The existing PD trench section included trenches that were 3.5 feet deep, with 18" of gravel below the distribution lateral. This corresponds to a sidewall area of 3.0 square feet/lineal foot (SF/LF). The minimum size of disposal field required for the 1,425 GPD design flow is calculated as follows:

Therefore, a total of 400 LF of PD leachfield is anticipated to be required for SS disposal, which exceeds the existing 210 LF dedicated to SS disposal. It is proposed that 2 additional PD leachlines of 100 LF each be

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removed from the PW system and connected to the SS system. An additional 100% reserve (400 LF) also needs to be identified. Approximately 1,400 LF total of PW PD leachfield is available, and it is recommended that the reserve area requirement be met with the an additional 400 LF of the PW PD leachfield. The enclosed overall site plan (Enclosure B) show the location of the existing disposal area.

OTHER CONSIDERATIONS

ODOR CONTROL

There should be no noxious odors from a properly designed and operated treatment system. See Alternative Courses of Action for operation alternatives.

GROUNDWATER CONTAMINATION

The nearest existing or proposed water well to the SS treatment and disposal systems is approximately 100 feet. No disposal of wastewater effluent will occur within 100 feet of any existing or proposed wells.

PROTECTION

Exposed wastewater treatment facilities should be posted with appropriate warning signs. The treatment areas will be protected to restrict access and potential damage to the system.

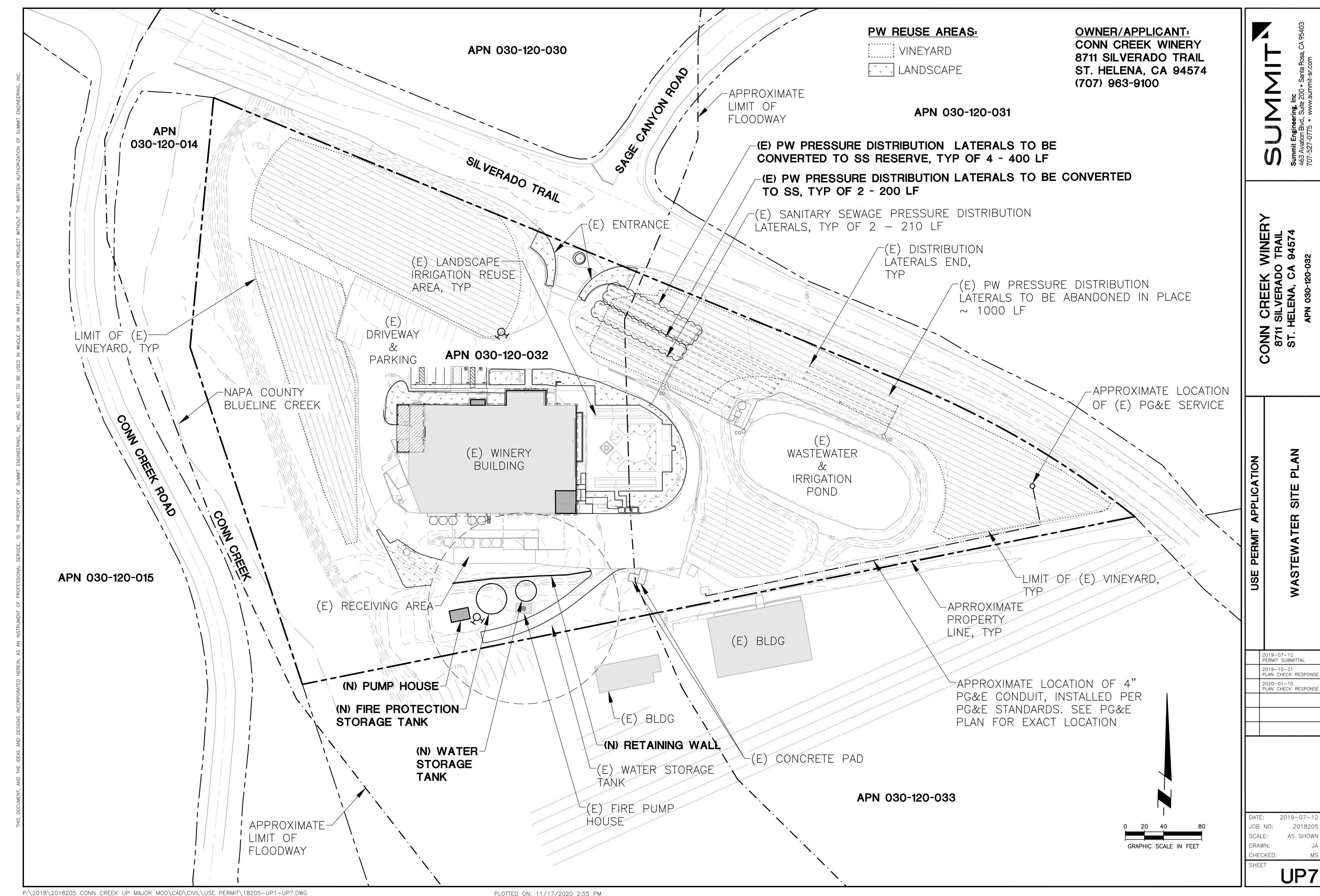
ALTERNATIVE COURSES OF ACTION

For the SS system, should there be any unforeseen operational difficulties, the following additional courses of action would be available if necessary:

- Pumping and truck transfer of treated and diluted wastewater to an approved treatment plant would be used as additional courses of action
- Primary and reserve area expansion to accommodate additional SS disposal
- Additional treatment of SS for land disposal

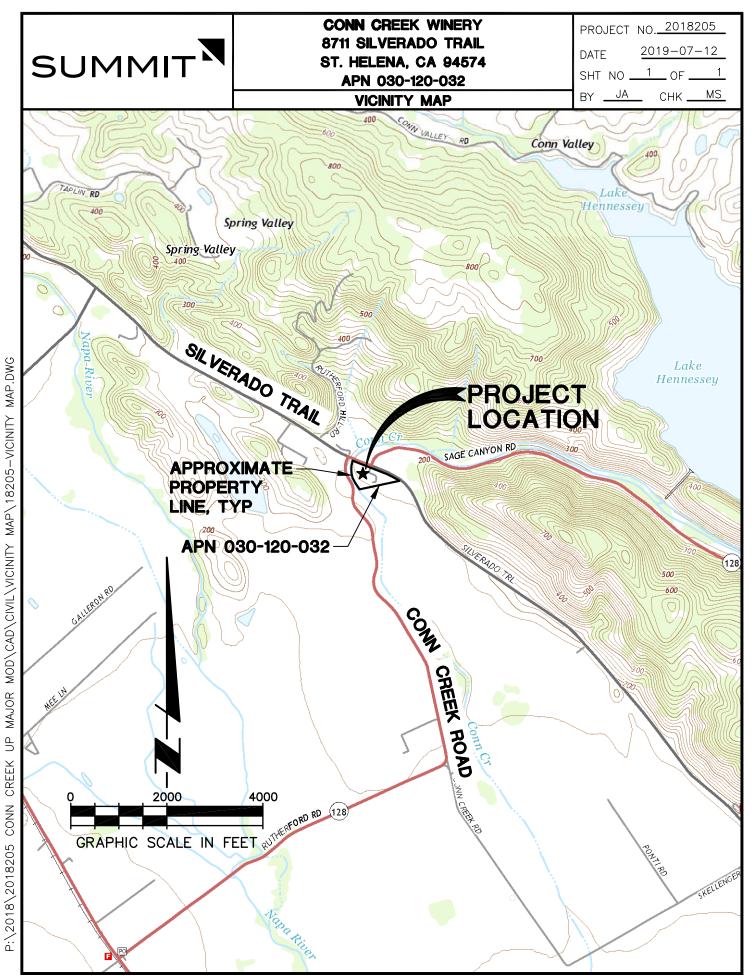
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ENCLOSURE A



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ENCLOSURE B



Summit Engineering, Inc

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Project No. 2019040

ENCLOSURE C

ABBELLATIA

₹	ANGLE	INT	INTERIOR
4	AND	IRR	IRRIGATION
0	AT	JB	JUNCTION BOX
Ę.	CENTERLINE	Jr.	JOINT
OR DIA.	DEGREE	LD	LIGHT DUTY
E CR DIA.	DIAMETER FLOWLINE	LF LP	LINEAL FOOT LOW POINT
1/	PARALLEL	LAT	LATERAL
85	PERCENT	LT	LEFT
2	PROPERTY LINE	MG	MILLION GALLON
AB	ANCHOR BOLT	MH	MANHOLE
AC AD	ASPHALT CONCRETE	M.H.W.L.	MAXIMUM HIGHWATER LII
ADD'I	AREA DRAIN ADDITIONAL	MAX MFGR	MAXIMUM MANUFACTURER
A66	AGGREGATE	MIN	MINIMUM
APPROX	APPROXIMATE	MISC	MISCELLANEOUS
AVG	AVERAGE	MPT	MALE PIPE THREADS
8	BASE CHANNEL WIDTH	N	NORTH
BC BM	BEGIN CURVE	NIC	NOT IN CONTRACT
BLDS	BENCH MARK BUILDING	NTS NO. OR #	NOT TO SCALE
BLK	BLOCK	NOM	NOMINAL
BLKE	BLOCKING	oc .	ON CENTERS
BM	BEAM	OD	OUTSIDE DIAMETER
BO	BOARD	OH	OVERHEAD
BOT	BOTTOM	PI	POINT OF INTERSECTION
CJ	CATCH BASIN CONSTRUCTION JOINT	PP PSD	POWER POLE
CMP	CORRUGATED METAL PIPE	PUE	PERFORATED SUBDRAIN PUBLIC UTILITIES EASEM
20	CLEANOUT	PVC	POLYVINYL CHLORIDE
CSP	CORRUGATED STEEL PIPE	PW	PROCESS WASTEWATER
CKR	CHECKER	PEN	PENETRATION
GL	CLASS	PLYND	PLYWOOD
CLR CO	CLEAR COUNTY	PT PVMT	POINT PAVEMENT
CONC	CONCRETE	R/W	RIGHT OF WAY
CONST	CONSTRUCTION	R OR RAD	RADIUS
CONT	CONTINUOUS	RCP	REINFORCED CONCRETE
CTR	CENTER	RED	REDUCER, REDUCING
D DF	DITCH DEPTH	REF	REFERENCE
DBL	DOUGLAS FIR	REINF REQ'D	REINFORCING REQUIRED
DIA	DIAMETER	RT	RIGHT
DIM	DIMENSION	RND	REDWOOD
DNS	DRAWING	5	SOUTH OR SLOPE
E	EAST	SD	STORM DRAIN
EC EF	END OF CURVE EACH FACE	5F	SQUARE FEET
EN	EACH WAY	99 95	SUBGRADE STAINLESS STEEL
EA	EACH	SSMH	SANITARY SEMER MANH
EL OR (ELEV)	ELEVATION	SAN	SANITARY
ELEC	ELECTRICAL	SCH	SCHEDULE
EMBED	EMBEDMENT	SIM	SIMILAR
EQ EXC	EQUAL OR EQUATION EXCAVATION, EXCAVATE	SPEC SQ	SPECIFICATION SQUARE
EXIST OR (E)	EXISTING	50 55	SANITARY SEWER
EXP	EXPANSION	STA	STATION
FF	FINISH FLOOR	STD	STANDARD
FG	FINISH GRADE	STL	STEEL
FH FP	FIRE HYDRANT	T	TELEPHONE
FIN	FIRE PROTECTION FINISH	TOM TO	TEMPORARY BENCH MAI TOP OF CONCRETE
PL6	FLANGED	TEE	TOP OF CONCRETE CUR
PPT	FEMALE PIPE THREADS	779	TOP OF PAYEMENT
FT	FOOT OR PEET	THK	THICK
FTG	FOOTING	TOT	TOTAL
FÜT	FUTURE	TRANS	TRANSITION
<u> </u>	GAS, ROAD BRADIENT GRADE BREAK	TYP	TRAPEZOIDAL TYPICAL
5V	GATE VALVE	UC	UTILITY CHASE
6A	GAVGE	UNO	UNLESS NOTED OTHERWI
BALV	GALVANIZED	V50	VINEYARD SUBDIRAIN
K	HANDICAPPED	VERT	VERTICAL
HD up	HEAVY DUTY	W	WITH
HP HW	HIGH POINT HIGH WATER	WO	WITHOUT
HDR	HIGH WATER HEADER	M	WEST OR WATER WASTEWATER
	HORIZONTAL	NWF	· · · · · · · · · · · · · · · · · · ·
HORIZ	MUNCHALUNTI PRE	N W W	NELLEL NIKE PARKIC
HOKIZ ID IF	INSIDE DIAMETER	NO	WELDED WIRE FABRIC WOOD

UTILITIES NOTES

INVERT ELEVATION

CONTRACTOR SHALL VERIFY ELEVATIONS AND LOCATIONS OF EXISTING UTILITIES WITHIN THE WORK AREA AND NOTIFY THE ENGINEER OF ANY DISCREPANCIES FROM THAT SHOWN PRIOR TO PROCEEDING WITH THE WORK

YD. YARD, YARDS

DITCH SIDE SLOPE

- 2. COORDINATE INSTALLATION OF ELECTRICAL UTILITIES WITH OWNER'S ELECTRICAL
- 3 WHERE POSSIBLE AND WHERE SEPARATION STANDARDS CAN BE MET, UTILITIES CAN BE INSTALLED IN COMMON TRENCHES. THE CONTRACTOR SHALL VERIFY BEDDING AND BACKFILL DETAILS WITH THE ENGINEER WHERE COMMON TRENCHING IS DESIRED.
- PROVIDE THRUST BLOCKS AT ALL HORIZONTAL AND VERTICAL BENDS ON THE PROCESS WASTEWATER FORCE MAIN (FWFM).
- 5. A COMPACTED CLAY OR SLURRY CEMENT PLUS (MIN 18" LONG X 18" THICK) SHALL BE PLACED IN THE TRENCH AND AROUND THE PWFM AT 50 FEET ON CENTER.
- 6. UTILITY CHASES SHOWN ARE INTENDED TO BE SPARES AFTER THE WORK IS COMPLETE. 7. PIPELINE DEPTH OF BURY:
- A. PWFM & GRAVITY LINES 2'-0" MIN (UNO) 2'-0" MIN (UNO) B. UTILITY CHASES C. ELECTRICAL 2'-6" MIN (UNO) D. WATER 2'-6" MIN (UNO)
- 8. SLOPE FOR WASTEWATER LINES (PWSS) = 0.02 MIN (UNO)

GENERAL NOTES

BEFORE ENTERING SUCH PROPERTIES.

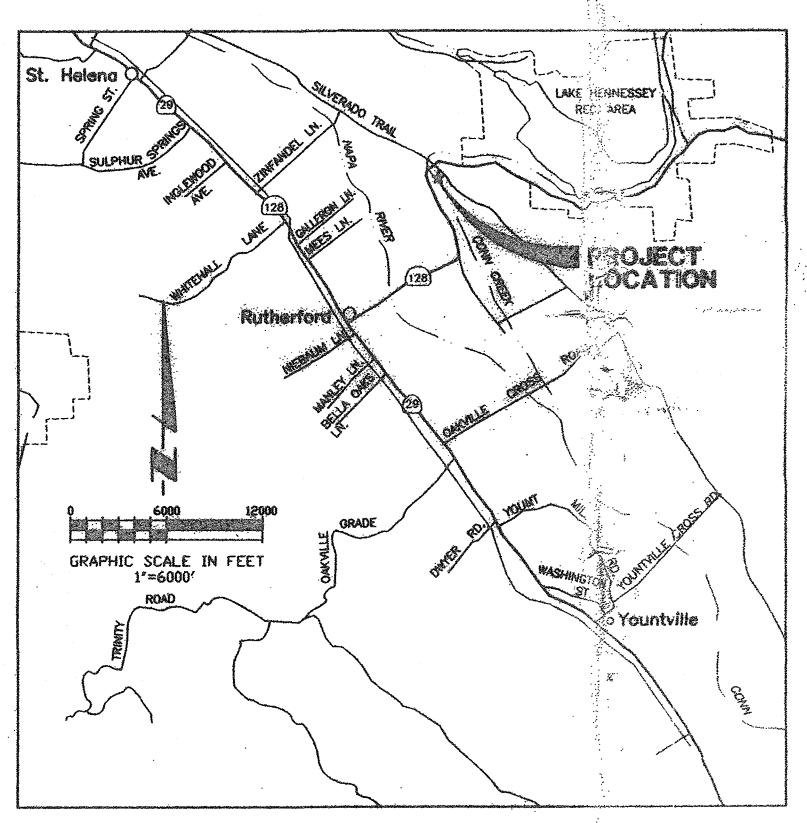
- ALL WORK SHALL CONFORM TO THE LATEST EDITION OF THE UNIFORM BUILDING CODE AND/OR APPLICABLE COUNTY OF NAPA CODES, ORDINANCES, ZONING AND
- 2. ALL WORK SHALL BE IN COMPLIANCE WITH ALL APPLICABLE OCCUPATIONAL SAFETY AND HEALTH ADMINISTRATION (O.S.H.A.) STANDARDS AS SET FORTH BY THE FEDERAL DEPARTMENT OF LABOR AND/OR THE STATE OF CALIFORNIA. THE CONTRACTOR SHALL SECURE A TRENCH PERMIT FROM THE CALIFORNIA DIVISION OF INDUSTRIAL SAFETY PRIOR TO EXCAVATION OF ANY TRENCH OVER FIVE FEET DEEP.
- ALL ONSITE SEMER, WATER AND GAS LINE CONSTRUCTION SHALL CONFORM TO THE REQUIREMENTS OF THE UNIFORM PLUMBING CODE (U.P.C.) AND ALL APPLICABLE REGULATIONS OF THE COUNTY OF NAPA AND COGNIZANT UTILITY COMPANIES.
- 4. THE DRAWINGS SHALL NOT BE SCALED. ALL WORK SHALL BE GOVERNED BY THE DIMENSIONS SHOWN ON THE DRAWINGS. DISCREPANCIES SHALL BE BROUGHT TO THE ENGINEER'S ATTENTION FOR ADJUSTMENT PRIOR TO PROCEEDING WITH THE WORK.
- 5. THE CONTRACTOR SHALL FIELD VERIFY ALL DIMENSIONS SHOWN AND BRING DISCREPANCIES TO THE ATTENTION OF THE ENGINEER PRIOR TO PROCEEDING WITH
- 6. DETAILS OF CONSTRUCTION NOT INDICATED OR NOTED SHALL BE CONSIDERED OF THE SAME CHARACTER SHOWN FOR SIMILAR OR EXISTING CONSTRUCTION.
- THIS DRAWING DOES NOT REPRESENT A PROPERTY SURVEY. PROPERTY LINES HAVE BEEN PLOTTED FOR INFORMATIONAL PURPOSES ONLY AND ARE APPROXIMATE.
- CONTRACTOR SHALL SECURE LETTERS OF PERMISSION FROM ADJACENT LAND OWNERS
- 9. THE NAPA COUNTY CONSERVATION DEVELOPMENT & PLANNING DEPARTMENT (NCCDPD) SHALL BE NOTIFIED 48 HOURS PRIOR TO STARTING ANY WORK. THE CONTRACTOR SHALL BE RESPONSIBLE FOR KEEPING THESE AGENCIES INFORMED OF HIS SCHEDULE.
- 10. CONTRACTOR SHALL PROVIDE 24 HOURS ADVANCE NOTICE TO THE ENGINEER FOR REQUESTED INSPECTIONS.
- II. THE ONNER SHALL PROVIDE FOR NECESSARY MATERIAL AND SOILS TESTING AND OBSERVATION. THE CONTRACTOR SHALL PROVIDE 48 HOURS MINIMUM NOTICE PRIOR TO REQUIRED OBSERVATION OR TESTING.
- 12. THE LOCATIONS OF EXISTING UNDERGROUND UTILITIES AS SHOWN ON THE PLAN ARE BASED ON THE BEST INFORMATION AVAILABLE; HOMEVER, THE ENGINEER ASSUMES NO RESPONSIBILITY FOR THE ACCURACY OF THE INFORMATION SHOWN, OR THE INADVERTENT OMISSION OF ANY SUCH INFORMATION. CONTRACTOR SHALL VERIF LOCATION OF EXISTING UTILITIES; CONFLICTS AND/OR DISCREPANCIES SHALL BE BROUGHT TO THE ATTENTION OF THE ENGINEER. UNLESS NOTED OTHERWISE, EXISTING UTILITIES SHALL BE PROTECTED AND MAINTAINED BY THE CONTRACTOR
- THE LOCATIONS OF ALL EXISTING UNDERGROUND UTILITIES HAVE NOT BEEN INDICATED ON THESE DRAWINGS. GRADING OPERATIONS SHALL BE COORDINATED WITH THE OWNER'S REPRESENTATIVE REGARDING EXISTING FEATURES. THE ENGINEER ASSUMES NO RESPONSIBILITY FOR THE UTILITY LOCATIONS.
- UNDERGROUND SERVICE ALERT (U.S.A.) CALL TOLL FREE (800)642-2444 AT LEAST 48 HOURS PRIOR TO EXCAVATION
- EXISTING UTILITIES SHALL BE KEPT IN SERVICE AT ALL TIMES. UTILITIES THAT INTERFERE WITH WORK TO BE PERFORMED UNDER THIS PROJECT SHALL BE PROTECTED AS REQUIRED IN ACCORDANCE WITH COUNTY OF NAPA, P.G.& E. AND PACIFIC BELL REQUIREMENTS.
- THE CONTRACTOR SHALL NOTIFY P.G. & E. AND PACIFIC BELL PRIOR TO STARTING ANY WORK. THE CONTRACTOR SHALL BE RESPONSIBLE FOR KEEPING THESE UTILITY COMPANIES INFORMED OF HIS SCHEDULE.
- 17. THE CONTRACTOR SHALL PURCHASE AND MAINTAIN SUCH INSURANCE AS WILL PROTECT AND HOLD HIM, THE OWNER AND THE ENGINEER HARMLESS FROM CLAIMS WHICH MAY ARISE OUT OF OR RESULT FROM THE CONTRACTOR'S OPERATIONS UNDER THE CONTRACT, WHETHER SUCH OPERATIONS BE BY HIMSELF OR BY ANY SUBCONTRACTOR OR BY ANYONE DIRECTLY OR INDIRECTLY EMPLOYED BY ANY OF THEM, OR BY ANYONE FOR WHOSE ACTS ANY OF THEM MAY BE LIABLE.
- THE CONTRACTOR SHALL SECURE ALL NECESSARY PERMITS AND INSPECTIONS FROM (NCCDPD). THE OWNER WILL MAKE APPLICATIONS AND PAY ALL PERMIT
- CONTRACTOR SHALL PROVIDE ALL LABOR, MATERIALS, EQUIPMENT, TOOLS AND OTHER SERVICES NECESSARY FOR PROPER EXECUTION OF THIS CONTRACT.
- 20. THE CONTRACTOR SHALL BE RESPONSIBLE FOR THE DAILY RECORD OF DIFFERING CONDITIONS. THE AS-BUILT INFORMATION SHALL BE RECORDED ON SEPIA DRAWINGS PROVIDED BY THE OWNER. PRIOR TO FINAL PAYMENT, THE CONTRACTOR SHALL PROVIDE THE AS-BUILT DRAWINGS, SIGNED AND DATED BY THE CONTRACTOR.
- 21. CONTRACTOR SHALL COORDINATE HIS WORK WITH EXISTING WINERY AND VINEYARD SPERATIONS. CONTRACTOR SHALL BE PREPARED TO PHASE PORTIONS OF THE WORK SO THAT IT DOES NOT INTERFERE WITH OR INHIBIT EXISTING WINERY OPERATIONS.
- 22. CONTRACTOR SHALL PROVIDE FIRST AID FACILITIES AND OTHER TEMPORARY SERVICES SUCH AS WATER, POWER, TELEPHONE, TOILETS, ETC.
- 23. OBTAINING OF CONSTRUCTION WATER AND UTILITIES SHALL BE COORDINATED WITH THE OWNER'S REPRESENTATIVE.
- 24. THE SCREENED CONTOURS AND TOPOGRAPHIC INFORMATION ON THESE DRAWINGS REPRESENT THE APPROXIMATE SURFACE CONDITIONS TO BE FOUND AT THE PROJECT LOCATION AS OF MAY, 1999. THIS INFORMATION HAS BEEN FURNISHED BY ALBION SURVEYS, INC. ST. HELENA, CA. FOR THE BASIS OF BEARINGS: THOMPSON & ASSOC. JOB NO. 448. DATUM ASSUMED.
- 25. FOR INFORMATION ON GEOLOGY AND EARTHWORK REQUIREMENTS, REFER TO GEOTECHNICAL INVESTIGATION FOR WASTEWATER PONDS PREPARED BY BAUER ASSOCIATES.
- 26. THE ENGINEER ASSUMES NO RESPONSIBILITY FOR SOIL CONDITIONS IN THE AREA OF CONSTRUCTION OPERATIONS.
- 27. ALL EXISTING UTILITIES, FENCES AND GATES AT THE SITE SHALL BE LOCATED, PROTECTED AND MAINTAINED AT ALL TIMES.
- 28. ONSITE GRADING SHALL NOT INHIBIT OFFSITE DRAINAGE.
- 29. REMOVE ONLY THOSE TREES THAT ARE NECESSARY TO CLEAR THE NEW CONSTRUCTION. NO TREE SHALL BE REMOVED WITHOUT PRIOR REVIEW WITH THE OWNER'S REPRESENTATIVE.
- 30. THE CONTRACTOR SHALL PROVIDE THE OWNER, AS A CONDITION OF COMPLETION AND RECEIPT OF FINAL PAYMENT, A WRITTEN GUARANTEE COVERING ALL MATERIALS AND WORKMANSHIP FURNISHED AND PERFORMED FOR THIS WORK AGAINST DEFECTS FOR A PERIOD ONE (I) YEAR AFTER THE DATE OF FILING THE NOTICE OF COMPLETION.
- 31. SUBSTITUTIONS FOR MATERIALS OR EQUIPMENT INDICATED ON THE CONTRACT DRAWINGS SHALL BE REVIEWED BY THE ENGINEER. THE ENGINEER ASSUMES NO RESPONSIBILITY FOR WORK AFFECTED BY SUCH CHANGES ACCOMPLISHED WITHOUT
- 32. AS THE RESPONSIBILITY FOR THE ENGINEERING DESIGN WORK DEPICTED ON THESE DRAWINGS RESTS WITH THE FIRM OF SUMMIT ENGINEERING, INC., CONSULTING CIVIL ENGINEERS, NO CHANGES ARE TO BE MADE TO THE WORK DURING OR PRIOR TO CONSTRUCTION WITHOUT THE EXPRESSED WRITTEN PERMISSION OR ACKNOWLEDGMENT OF SUMMIT ENGINEERING, INC., CONSULTING CIVIL ENGINEERS.
- 33. SEE DETAILED SPECIFICATIONS FOR PURTHER INFORMATION.

VILLA MI. EDEN

8711 SILVERADO TRAIL ST. HELENA, CALIFORNIA

WASTEWATER MANAGEMENT SYSTEM IMPROVEMENTS

APRIL, 2000



RECEIVED

LOCATION MAP

LIST OF DRAWINGS CENERAL INFORMATION

- OVERALL SITE PLAN PW POND PLAN
- SECTIONS & DETAILS

PLANS APPROVED

County of Napa

Of Physical Management (1988)

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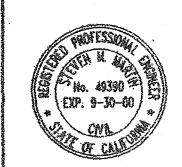
w/ condition

PLANS, SECTIONS AND DETAILS

SECTIONS & DETAILS

- SANITARY SEWER, SECTIONS DETAILS AND NOTES
- PW POND LINER DETAILS
- REFERENCE C: EXISTING MOUND SYSTEM (6 SHEETS)

original set of plans submitted 4/24/00 RECEIPT # 12825 AMT. PD. 123 +35= 258 JOB# 92-12720 + 92-12729 BY W.C.



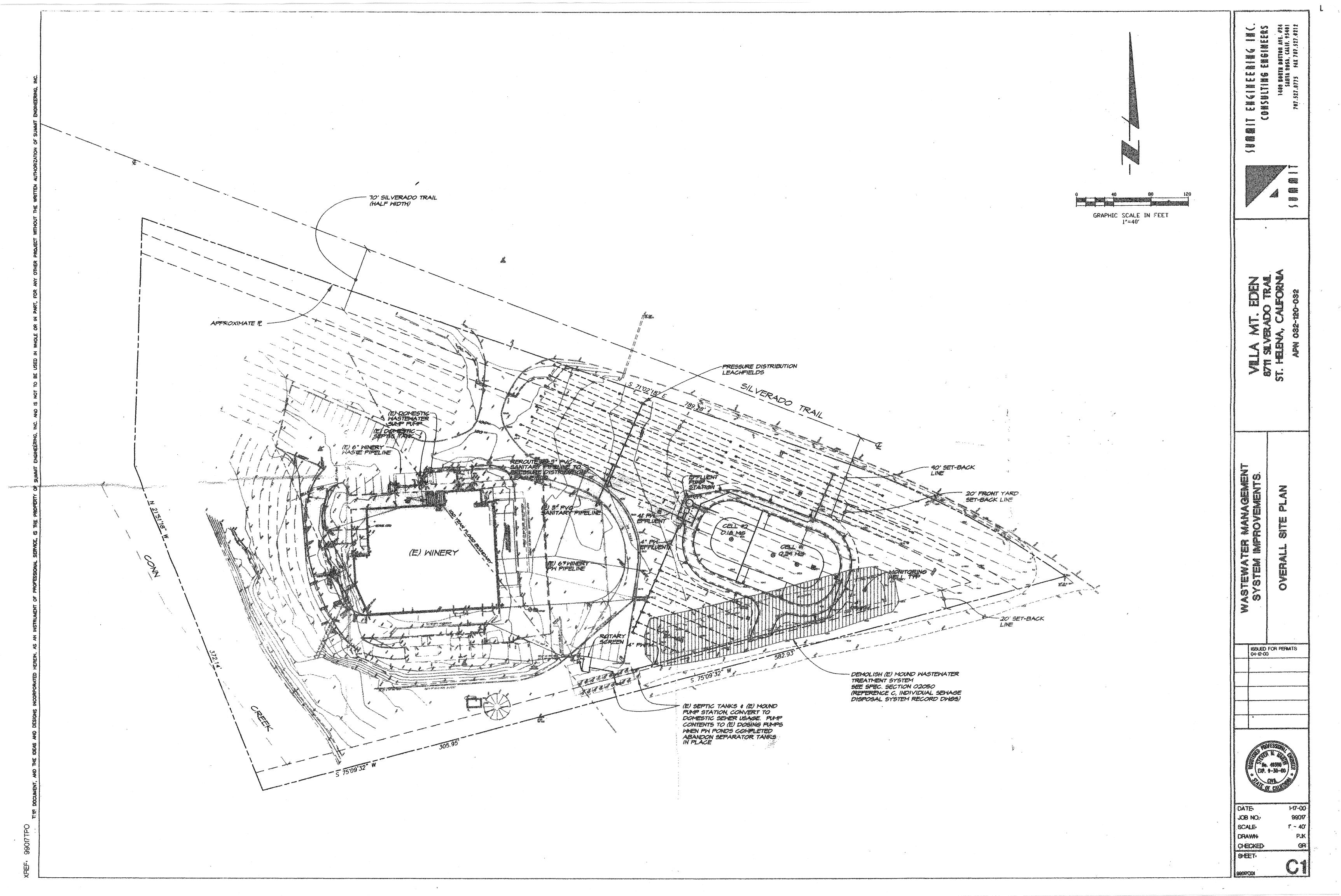
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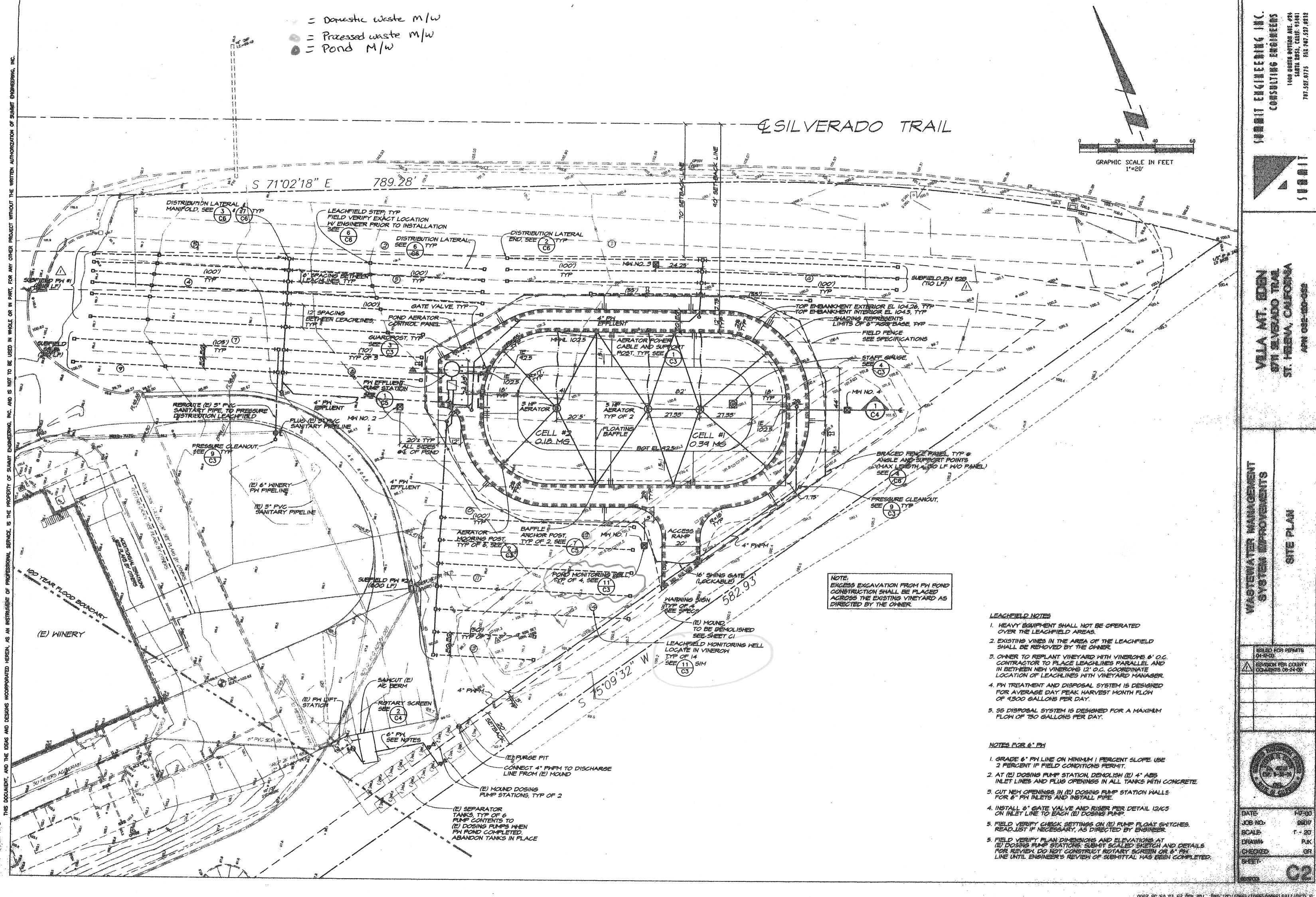
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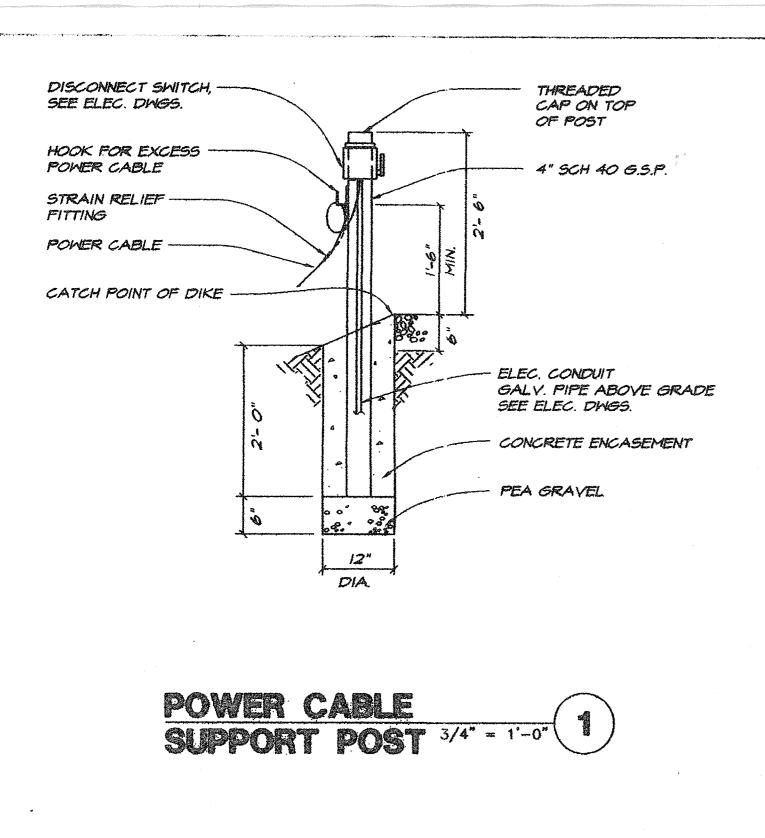
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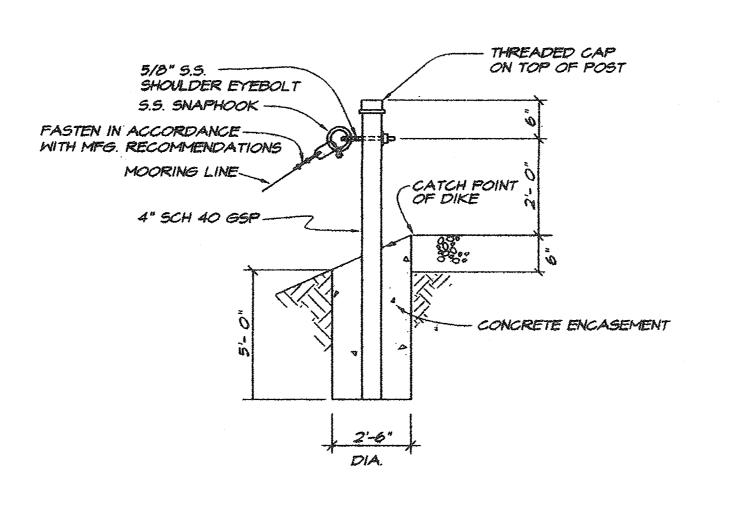
JOB NO. AS NOTED SCALE DRAWN CHECKED

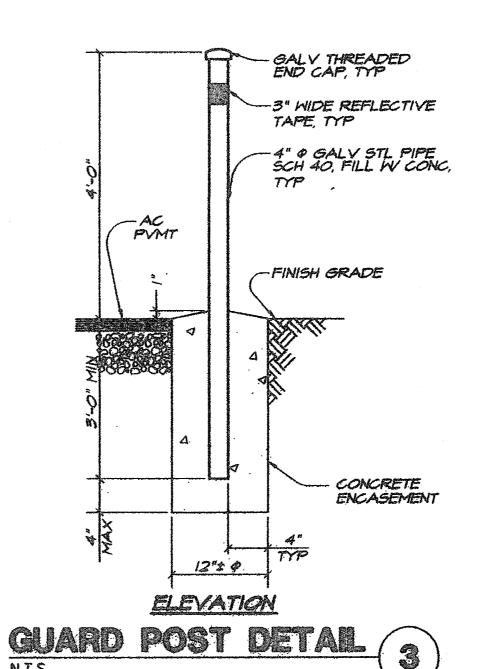
SHEET

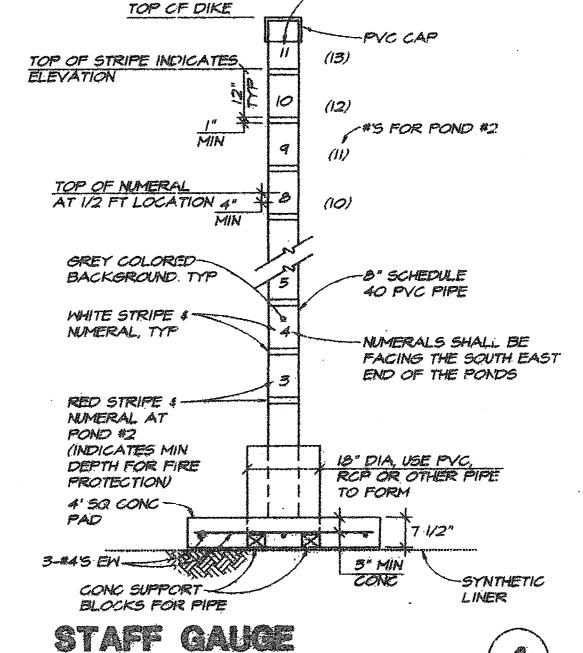




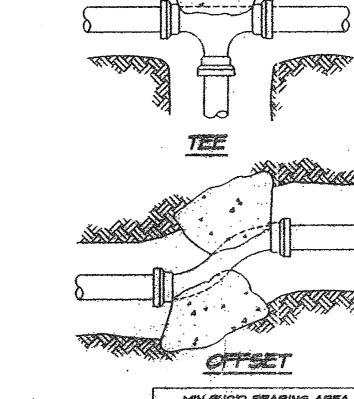






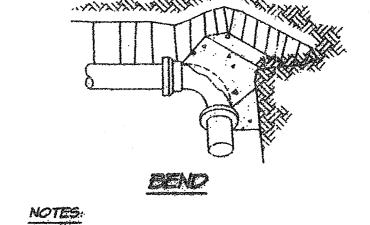


#5 FOR POND #



FLANGED GATE VALVE

VALVE & STEM

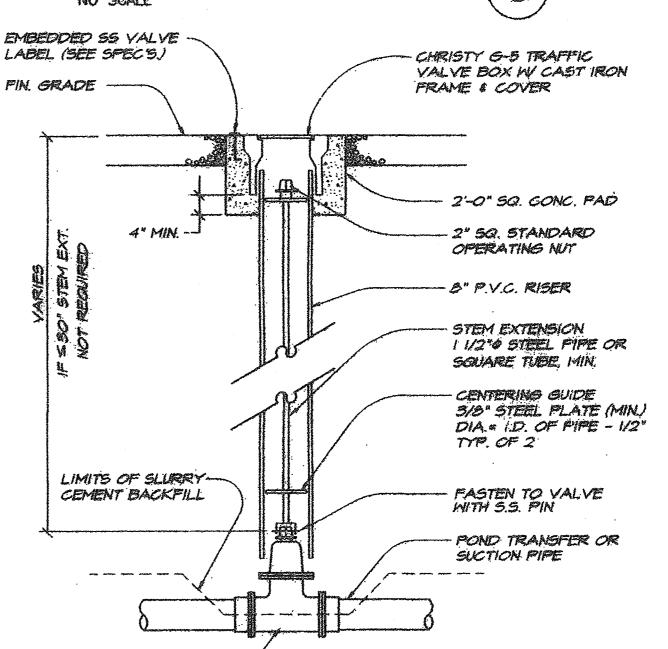


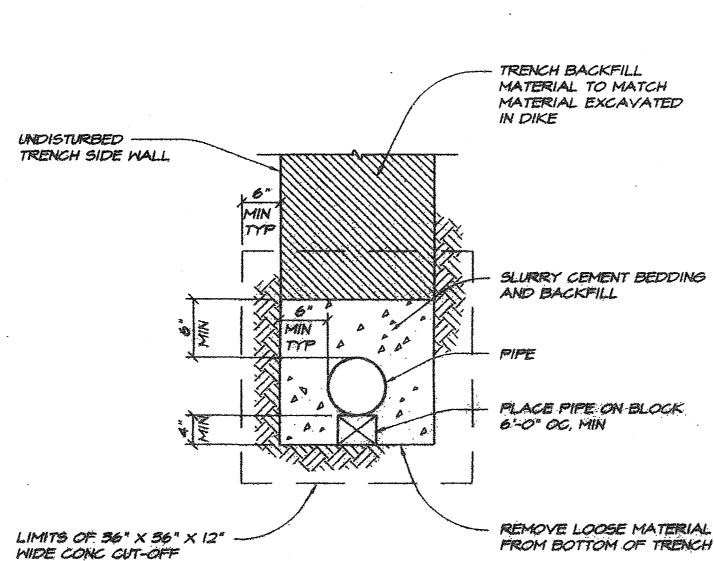
I. SAFE BEARING LOAD OF SOIL FOR HORIZONTAL THRUST SHALL NOT BE 2. CONCRETE BLOCKING, CAST IN PLACE, TO EXTEND PROM BELLS OF FITTINGS TO UNDISTURBED SOIL & ENTIRE BEARING AREA MUST BE AGAINST UNDISTURBED SOIL.

3. IN USING THE THRUST BLOCKING TABLE BELOW, ASSUME 2000 P.S.F. BEARING CAPACITY UNLESS OTHERWISE SHOWN ON THE PLANS.

PIPE SIZE	SOIL BEARING CAPACITY	HARNESS BLOCKS	TESS AND DEAD BIDS	SENDS	45° BENOS	22 1/2 6000;
3.4.	1000 2000	2	2	3	2 1	1
6"	1000 2000	. 4 . 2	4 2	6	3 2	2
8*	1000 2000	7	7 4	<i>IQ</i> 5	5 3	3
12"	1000	16	16 8	22 	12	6







AERATOR MOORING

POST DETAIL

NO SCALE

(WHERE OCCURS)

UNISTRUT P2860-10 -

END CAP

UNISTRUT PIPE CLAMP, (CUSH-A-CLAMP FOR

I. CONNECT CHANNEL TO POST BASE WITH 2 HEX

GALVANIZED METAL

3. PROVIDE A 12" SQ X 6"

MIN THK, CONC PAD FOR

PIPE SUPPORTS WHERE

2. ALL UNITS TO BE

HOT-DIPPED

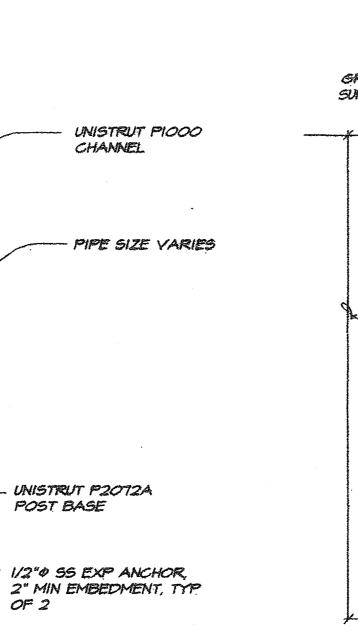
HEAD CAP SCREWS AND

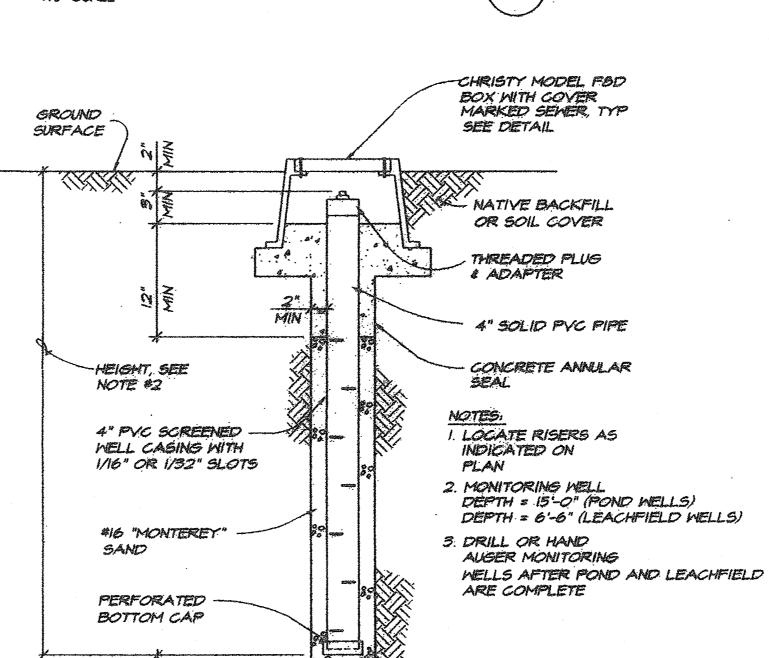
UNISTRUT NUT W SPRING.

PVC PIPE)

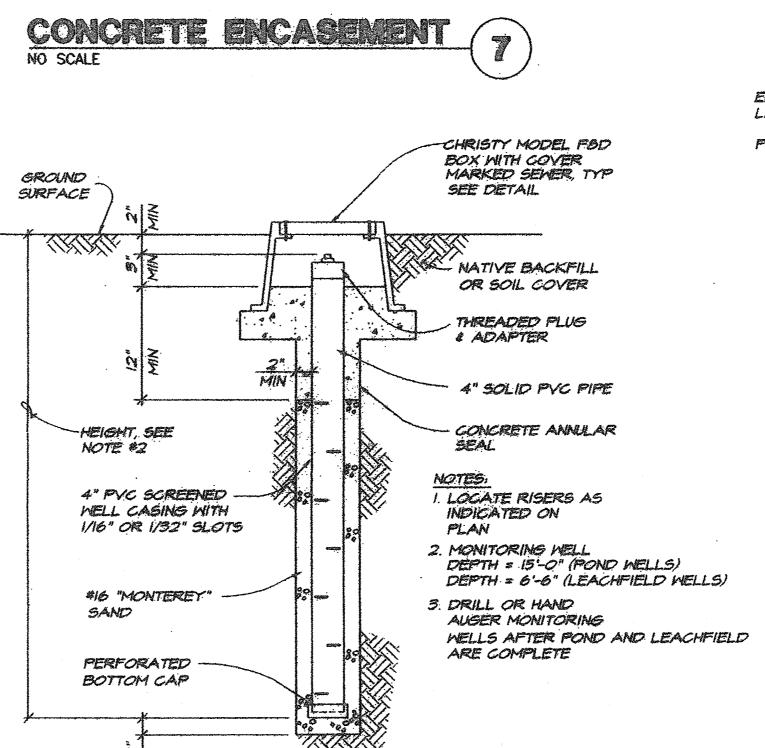
NOTES:







YOUTOING WELL



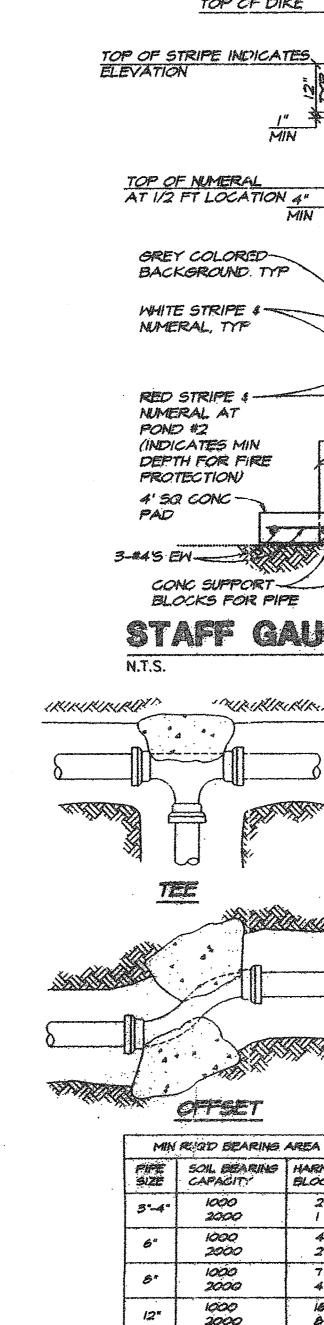
- 3" CLR TYP

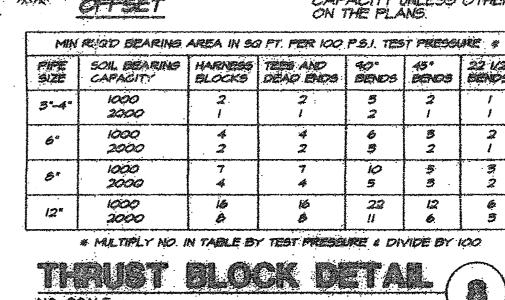
#4 STIRRUPS

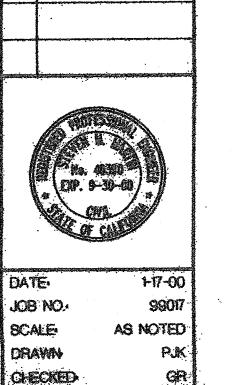
@ 24" OC

PIPE PER PLANS

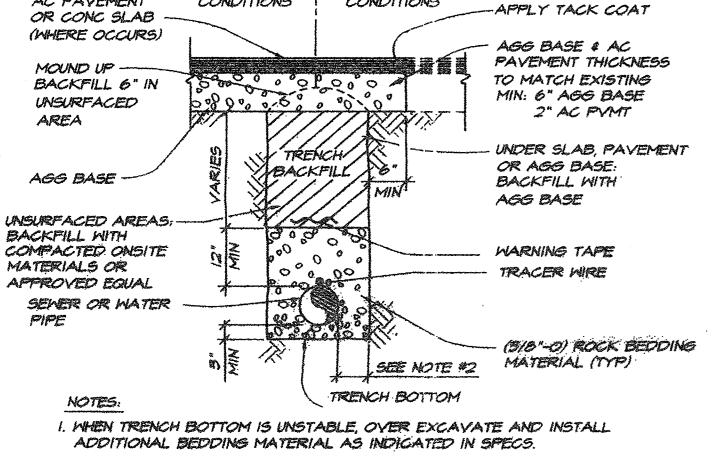
- #4 BARS







ISSUED FOR PERMITS 04-12-00



EXISTING

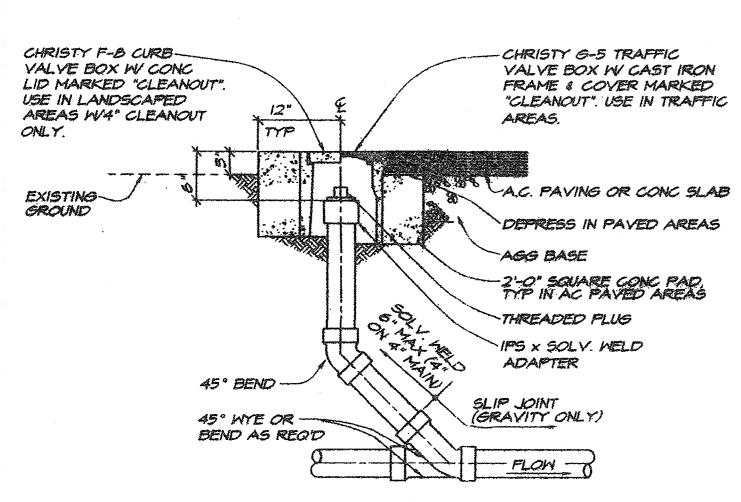
CONDITIONS

2. PIPE DIAMETER 18" OR LESS: 6" MIN, 9" MAX PIPE DIAMETER GREATER THAN 18": 4" MIN, 12" MAX

CONDITIONS

AC PAYEMENT

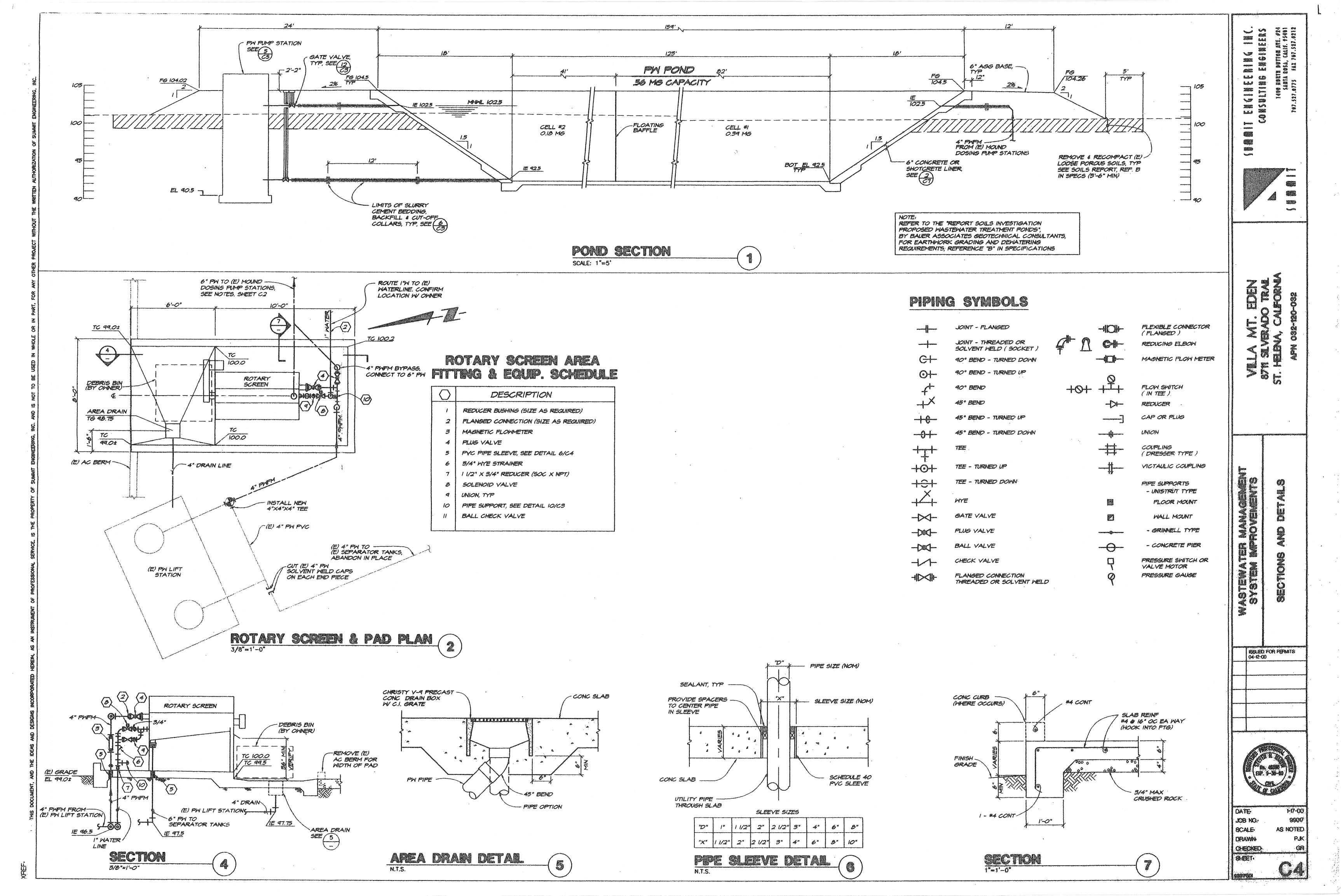
TYPICAL UTILITY PIPE TRENCH SECTION $3/4^{\circ} = 1'-0^{\circ}$

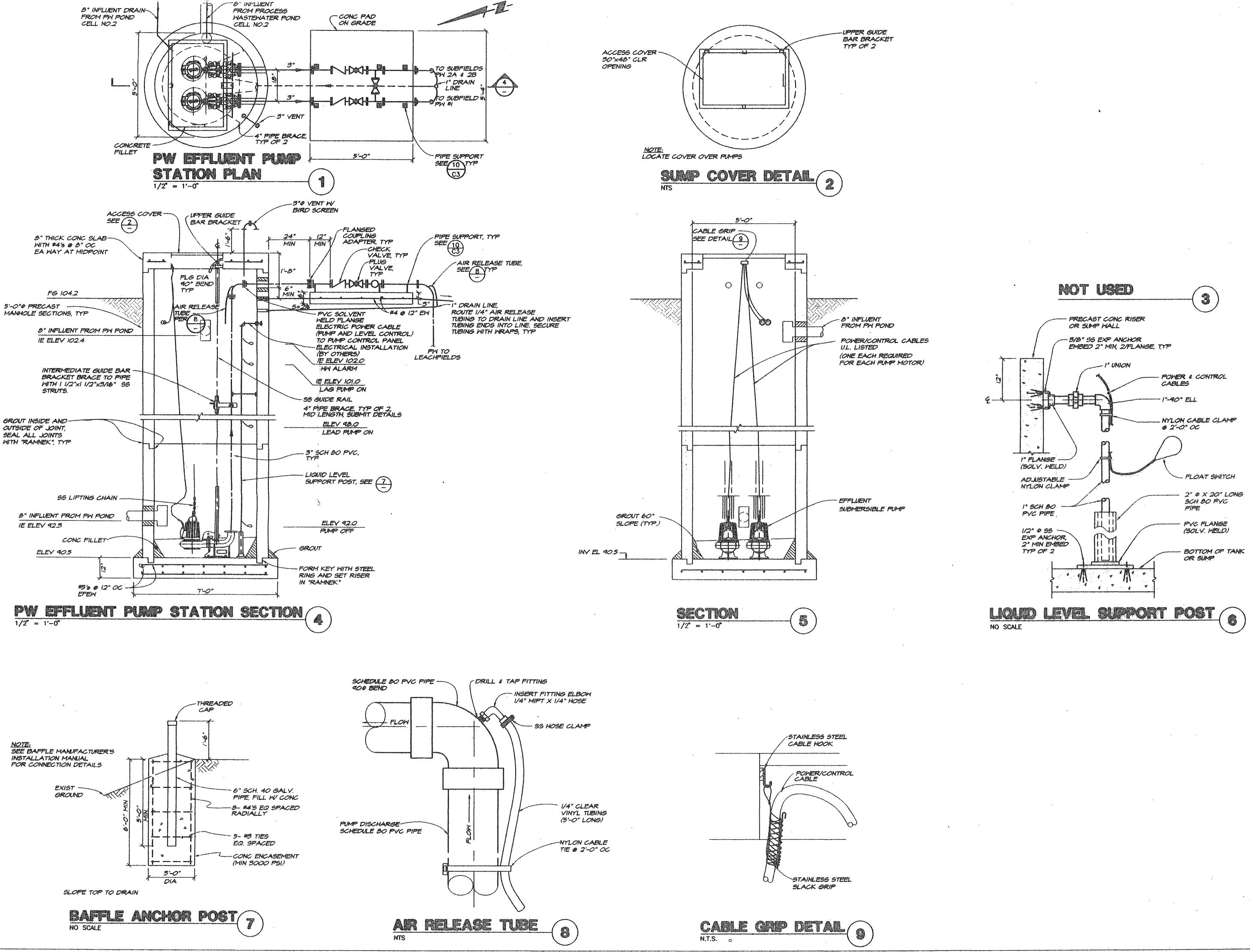


GRAVITY & PRESSURE CLEANOUT (GCO & PCO)

REQUIRED. PIPE SUPPORT NO SCALE

POST BASE





© /CADK:18es/990003,99017/99017601, dwg wed Apr 05 15:48:09 2000

JOB NO:

SCALE:

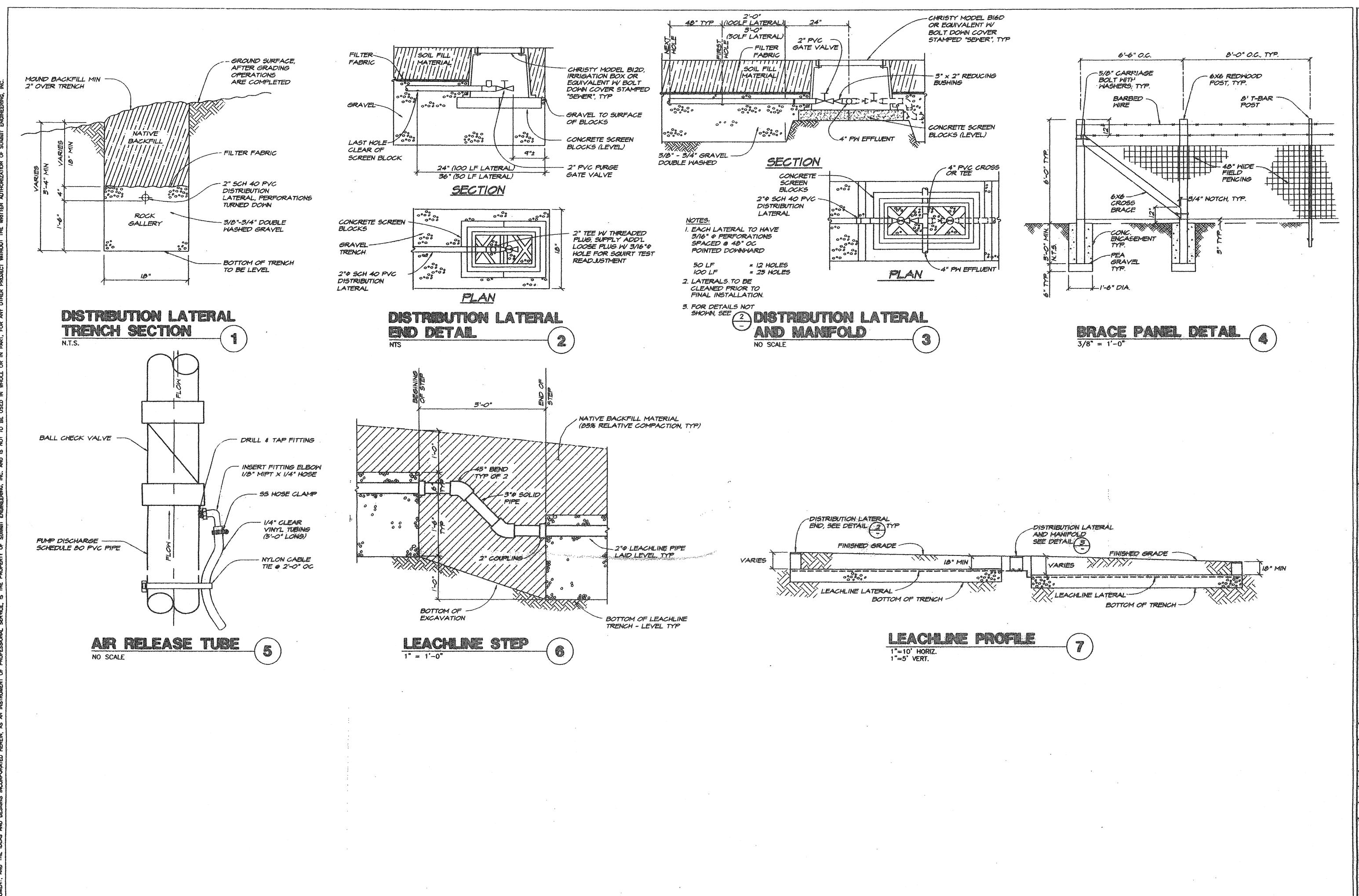
WASTEWATER SYSTEM INF

> ISSUED FOR PERMITS 04-12-00

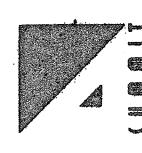
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AS NOTED

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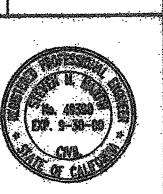


ENGINEENING INCINERS September 1



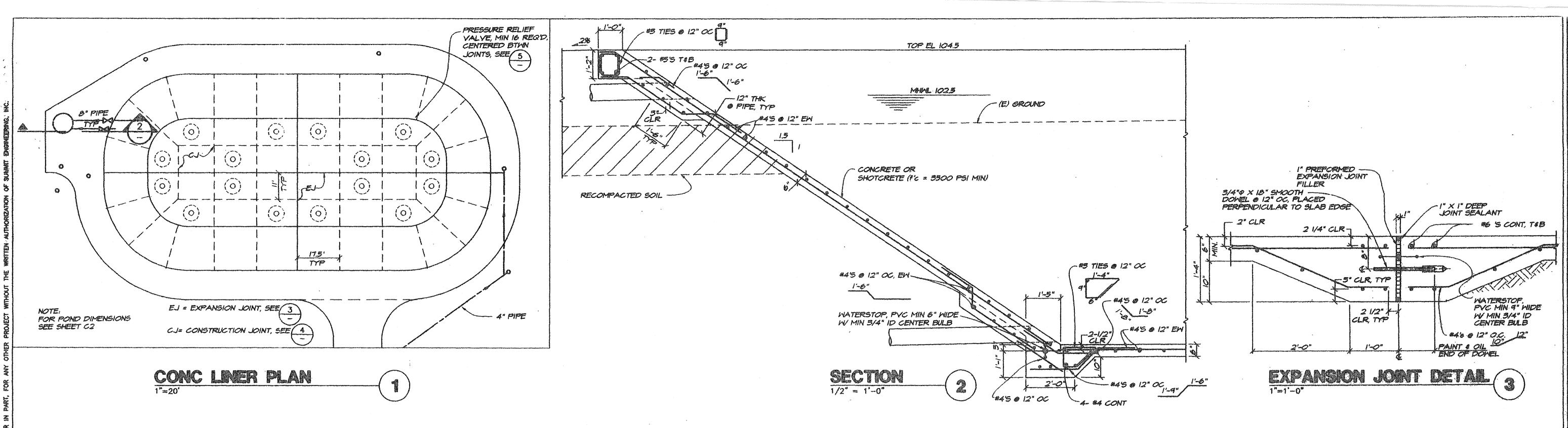
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1-17-00 108 NO: AS NOTED SCALE CHECKED

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GENERAL NOTES

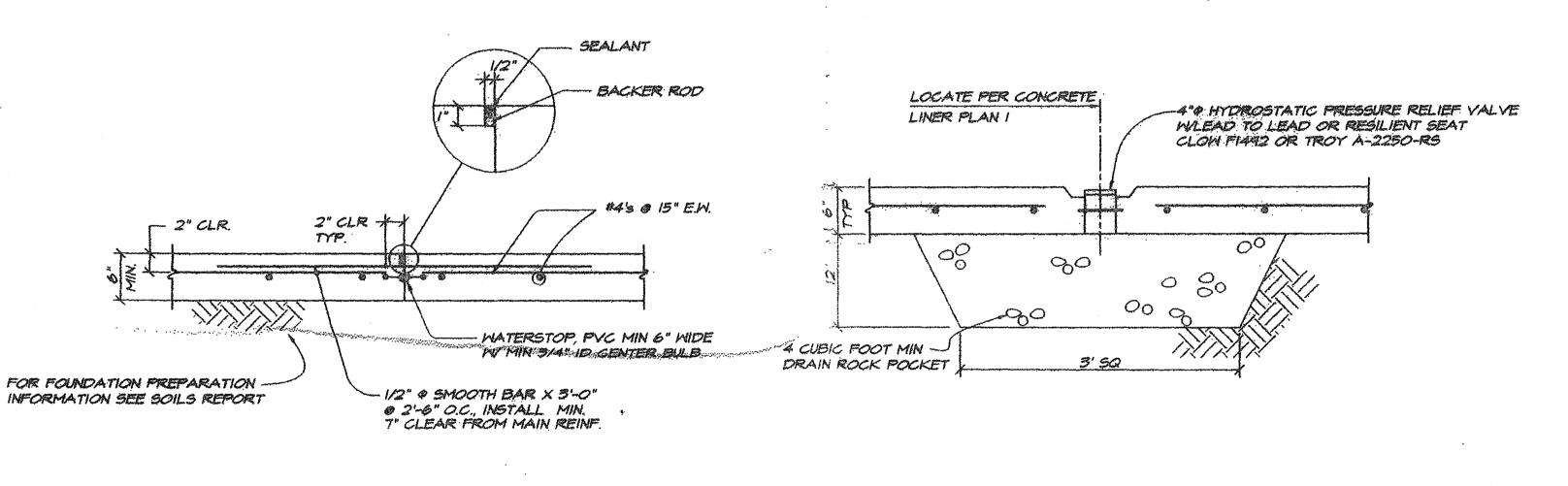
- I. ALL WORK SHALL CONFORM TO THE LATEST EDITION OF THE UNIFORM BUILDING CODE AND/OR APPLICABLE NAPA COUNTY ZONING AND PLANNING LAWS.
- 2. THE DRAWINGS SHALL NOT BE SCALED. ALL MORK SHALL BE GOVERNED BY THE DIMENSIONS SHOWN ON THE DRAWINGS. DISCREPANCIES SHALL BE BROUGHT TO THE ENGINEER'S ATTENTION FOR ADJUSTMENT PRIOR TO PROCEEDING WITH THE MORK.
- 3. DETAILS OF CONSTRUCTION NOT INDICATED OR NOTED SHALL BE CONSIDERED OF THE SAME CHARACTER SHOWN FOR SIMILAR OR EXISTING CONSTRUCTION.
- 4. ALL WORK SHALL BE IN COMPLIANCE WITH ALL APPLICABLE OCCUPATIONAL SAFETY AND HEALTH ADMINISTRATION (O.S.H.A.) STANDARDS AS SET FORTH BY THE FEDERAL DEPARTMENT OF LABOR AND/OR STATE OF CALIFORNIA.
- 5. THE CONTRACTOR SHALL FIELD VERIFY ALL DIMENSIONS SHOWN AND BRING DISCREPANCIES TO THE ATTENTION OF THE ENGINEER PRIOR TO PROCEEDING WITH THE WORK.
- 6. SUBSTITUTIONS FOR MATERIALS OR EQUIPMENT INDICATED ON THE CONSTRUCTION DRAWINGS SHALL BE REVIEWED BY THE ENGINEER. THE ENGINEER ASSUMES NO RESPONSIBILITY FOR WORK AFFECTED BY SUCH CHANGES ACCOMPLISHED WITHOUT HIS REVIEW.
- 7. AS THE RESPONSIBILITY FOR THE ENGINEERING DESIGN WORK DEPICTED ON THESE DRAWINGS RESTS WITH THE FIRM OF SUMMIT ENGINEERING, INC., CONSULTING CIVIL ENGINEERS, NO CHANGES ARE TO BE MADE TO THE WORK DURING OR PRIOR TO CONSTRUCTION WITHOUT THE EXPRESSED WRITTEN PERMISSION OR ACKNOWLEDGEMENT OF SUMMIT ENGINEERING, INC., CONSULTING CIVIL ENGINEERS.

CONCRETE, REINFORGING AND MATERIAL NOTES

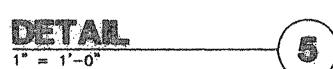
- I. ALL CONCRETE WORK SHALL BE PERFORMED IN ACCORDANCE WITH THE LATEST EDITION OF ACI-518.
- 2. PORTLAND CEMENT SHALL BE A STANDARD BRAND CONFORMING TO ASTM C-150, TYPE
- 3. CONCRETE SHALL HAVE THE FOLLOWING, MINIMUM COMPRESSIVE STRENGTH AT 28 DAYS,

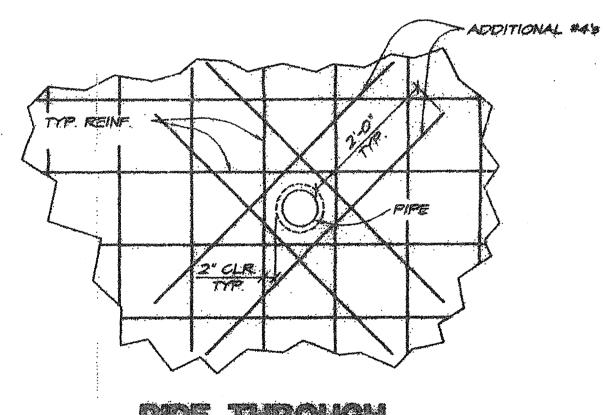
MAXIMUM AGC	megate size shall	BE I', MINIMUM 5.5 SACK MIX.
LOCATION	COMPRESSIVE 'STRENGTH	SPECIAL INSPECTION REQUIRED
POND LINER	5500 PSI	NO - DESIGN BASED UPON 2500 PSI

- 4. MAXIMUM SLUMP SHALL BE 4".
- 5. MAXIMUM WATER CEMENT RATIO SHALL BE .55.
- 6. REINFORCING STEEL SHALL CONFORM TO ASTM A-615, GRADE 60.
- 7. ALL REINFORCING HOOKS AND BENDS SHALL BE IN ACCORDANCE WITH ACI 318.
- 8. ALL BAR SPLICES SHALL BE LAPPED 40 BAR DIAMETERS, MINIMUM.
- 9. ALL CONCRETE SHALL BE TRANSIT MIXED IN ACCORDANCE WITH ASTM C94.
- IO. ALL CONCRETE EXCEPT THOSE SURFACES TO RECEIVE SEALANTS SHALL BE COATED WITH CURING COMPOUND CONFORMING TO ASTM C309, NON-STAINING AND CONTAINING A FUGITIVE DYE.
- II. CONTRACTOR SHALL SUBMIT MIX DESIGN FOR REVIEW BY ENGINEER PRIOR INCORPORATION INTO THE WORK.
- 12. CONSTRUCTION JOINTS SHALL BE LOCATED FOR THE CONVENIENCE OF THE CONTRACTOR. JOINTS INDICATED ON THE CONSTRUCTION DRAWINGS ARE THE MINIMUM JOINTS REQUIRED. IF ADDITIONAL JOINTS ARE PROVIDED, COORDINATE WITH THE ENGINEER TO VERIFY ADEQUACY OF REINFORCING.
- IS. WATERSTOPS SHALL BE PVC, CENTER BULB TYPE, MINIMUM 6" LENGTH WITH MINIMUM 5/4" DIAMETER CENTER BULB CONFORMING TO CORPS OF ENGINEERS CRD-C-572, BURKE DBI4-6 OR EQUAL.
- 14. EXPANSION JOINT MATERIALS SHALL BE NEOPRENE SPONGE RUBBER CONFORMING TO CORPS OF ENGINEERS CRD-C504 TYPE I.
- 15. JOINT SEALANT SHALL BE BURKE U-SEAL 3204 HAND GRADE (GRAY).
- 16. PRESSURE RELIEF VALVES SHALL BE TROY A2550 RS 6" DIA. FLOOR RELIEF VALVES AS MANUFACTURED BY TROY VALVE, P.O. BOX 181, TROY, PENNSYLVANIA.



CONST JOINT DETAIL





COLC LUISIN

NO SCALE

SERED FOR PERMITS O4-2-00

w iz



DATE: H7-00
JOB NO: 9807
SCALE: F-10
DRAWN JEB
CHECKED: GR

cor //

SUMMIT ENGINEERING, INC.
Project No. 2019040

ENCLOSURE D

SUMMIT

CONN CREEK WINERY 8711 Silverado Trail ST. HELENA, CA APN 030-120-032

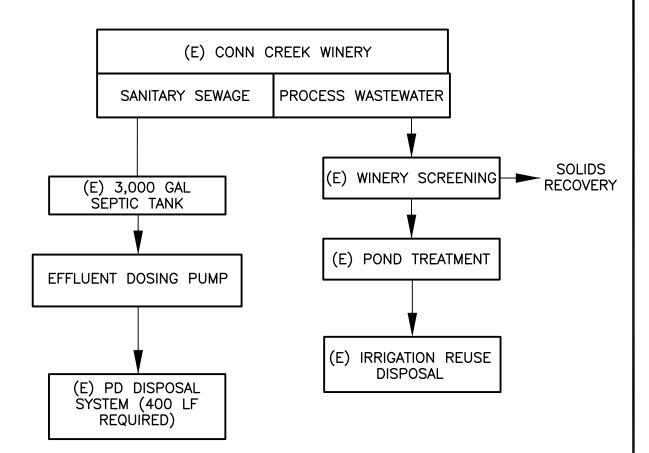
 PROJECT NO.
 208205

 DATE
 2019-05-07

 SHT NO
 1
 0F
 1

 BY
 SW
 CHK
 GG

SANITARY SEWAGE FLOW SCHEMATIC



PLOTTED ON: 5/7/2019 1:07 PM

SUMMIT ENGINEERING, INC.
Project No. 2019040

ENCLOSURE E

SUMMIT ENGINEERING, INC.	CONN CREEK WINERY	PROJECT NO.	2018205
,	Wastewater Feasibility Study	BY:	sw
	Existing Sanitary Sewage Flows	снк:	GG

SANITARY SEWAGE

Average Day w/o Event - Non-harvest					
Employee (full-time)	15 x	15 gpcd	=	225 gal/day	
Employee (part-time)	1 x	15 gpcd	=	15 gal/day	
Tasting Visitors	70 x	3 gpcd	=	210 gal/day	
Wine Tasting w/ Meal	15 x	5 gpcd	=	75 gal/day	
Total			=	525 gal/day	
			=	<u>530</u> gal/day	
Peak Tasting Day Harvest					
Employee (full-time)	15 x	15 gpcd	=	225 gal/day	
Employee (part-time)	1 x	15 gpcd	=	15 gal/day	
Tasting Visitors	225 x	3 gpcd	=	675 gal/day	
Private Promo Meal & Tasting	60 x	5 gpcd	=	300 gal/day	
Total			=	1,215 gal/day	
			=	<u>1,220</u> gal/day	
DESIGN FLOW			=	1,220 gal/day	

SUMMIT ENGINEERING, INC.	CONN CREEK WINERY	PROJECT NO.	2018205
•	Wastewater Feasibility Study	ву:	sw
	Proposed Sanitary Sewage Flows	снк:	GG

SANITARY SEWAGE

Average Day w/o Major Event - Non-harv	<u>est</u>			
Employee (full-time)	20 x	15 gpcd	=	300 gal/day
Employee (part-time)	1 x	15 gpcd	=	15 gal/day
Tasting Visitors	70 x	3 gpcd	=	210 gal/day
Private Marketing Event w/ Meal	15 x	5 gpcd	=	75 gal/day
Total			=	600 gal/day
			=	600 gal/day
Peak Tasting Day Harvest w/Event				
Employee (full-time)	20 x	15 gpcd	=	300 gal/day
Employee (part-time)	1 x	15 gpcd	=	15 gal/day
Tasting Visitors	225 x	3 gpcd	=	675 gal/day
Garden Event	60 x	5 gpcd	=	300 gal/day
Total			=	1,290 gal/day
				, 8-,,

SUMMIT ENGINEERING, INC.
Project No. 2019040

ENCLOSURE F

SUMMIT ENGINEERING, INC. **Consulting Civil Engineers**

CONN CREEK WINERY PW System Review

Process Wastewater Design Criteria

PROJECT NO. BY: CHK:

2016030 SW GG

FLOW CRITERIA AT PERMITTED PRODUCTION

FULL PRODUCTION

<mark>1,575</mark> ton/year **Annual Harvest** Wine Generation Rate 165 gal wine/ton Production 260,000 gal wine/year **PW Generation Rate** 4.8 gal PW/gal wine Annual PW Flow (crushed onsite) 1,248,000 gal PW/year

Bulk Wine bottled onsite 590,000 gal

Generation Rate 0.5 gal PW/gal wine

Annual PW Flow (bottled) 295,000 gal PW **Total Annual Volume** 1,543,000 gal PW

Months of Harvest Aug-Sept

Average Day Harvest Flow 4,100 gal PW/day Average Day Peak Harvest Month Flow 8,450 gal PW/day

Pond Volume 0.603 Mgal

Pond HRT (at peak flow, without

stormwater) 71.4 days Pond HRT (at peak PW + SW inflow) 63.7 days

Pond HRT (average flow, with

stormwater) 97.4 days

DESIGN PROCESS WASTEWATER FLOWS

	Monthly		Monthly		
	Percentage of		Storm	Monthly Total	Average Daily
Month	Annual Flow ^a	Monthly Flow	Inflow	Inflow	Flow
	(%)	(Mgal)	(Mgal)	(Mgal)	(gal)
August	8.1%	0.125	0.002	0.127	4,103
September	11.8%	0.182	0.007	0.189	6,306
October	16.4%	0.253	0.040	0.293	9,463
November	10.7%	0.166	0.089	0.255	8,485
December	6.5%	0.100	0.144	0.244	7,887
January	7.0%	0.108	0.175	0.284	9,150
February	7.6%	0.117	0.129	0.246	8,774
March	5.6%	0.086	0.107	0.193	6,212
April	6.5%	0.101	0.049	0.150	4,993
May	6.4%	0.099	0.016	0.115	3,707
June	7.2%	0.111	0.005	0.115	3,848
July	6.1%	0.095	0.000	0.095	3,065
Total	100%	1.543	0.763	2.306	_

Monthly percentage of flow based on PW distribution from flow data received from client. (2007-2015)

SUMMIT ENGINEERING, INC. Consulting Civil Engineers

CONN CREEK UP ASSISTANCE PW System Review Aeration Requirements PROJECT NO. BY: CHK: 2016030 SW GG

DESIGN CRITERIA - EXISTING

Sizing Parameters

BOD Concentration 7,700 mg/L

Average Day, Peak Harvest Month Flow 8,450 gal PW/day

Oxygen Requirement 1.5 lbs O₂/lb BOD

Oxygen Transfer Rate (Submersible Aspirator)

Power/ Volume Ratio, Pond No. 1 0.10 - 0.20 Hp/ 1,000 cu ft

Pond No. 1 Volume

Pond No. 1 Volume

O.60 Mgal

Aeration Pond No. 1

BOD Mass Loading

Aerator Run Time

24 Hrs/day

Oxygen Requirement

Aerator Horsepower Required

Aerator Horsepower Recommended

Check Power-to-Volume Ratio

543 lbs BOD/day

Ada Hrs/day

14 Hp

15 Hp

16 Hp

17 Hp

18 Hp

18

P\V range desired is 0.10 to 0.20, this will enable oxygen transfer and mixing to occur within the upper 3-4 feet of the pond as required in a facultative aerated lagoon system.

SUMMIT ENGINEERING, INC. Consulting Civil Engineers	CONN CREEK UP ASSISTANCE	PROJECT NO.	2016030
	PW System Review	BY:	SW
	Climate Data	снк:	GG

		Average	Reference						100-year
Month	Days	Temp ^a	Evapotranspiration ^b	Pan Evaporation ^c	Lake Evaporation ^d	Average Precipitation ^e	10-Year Precipitation ^f	100-Year Precipitation ^f	Stormwater Inflow ^g
		(F)	(in)	(in)	(in)	(in)	(in)	(in)	(gal)
August	31	70.7	5.9	7.2	5.5	0.1	0.2	0.3	2,443
September	30	67.6	5.2	6.4	4.9	0.3	0.5	0.7	6,884
October	31	61.7	3.3	3.9	3.0	1.8	2.9	4.2	39,973
November	30	52.3	1.1	1.9	1.5	4.0	6.5	9.3	88,829
December	31	46.6	1.2	1.4	1.1	6.5	10.6	15.1	144,347
January	31	46.0	0.8	1.5	1.2	7.9	12.9	18.4	175,438
February	28	50.2	2.3	2.0	1.5	5.8	9.5	13.5	128,802
March	31	52.3	3.6	3.4	2.6	4.8	7.8	11.2	106,595
April	30	56.3	5.2	4.2	3.2	2.2	3.6	5.1	48,856
May	31	62.4	6.7	5.9	4.5	0.7	1.2	1.7	15,767
June	30	68.0	7.0	6.5	5.0	0.2	0.3	0.5	4,664
July	31	71.1	6.9	8.9	6.9	0.0	0.0	0.0	222
Total	365	58.8	49.2	53.2	41.0	34.4	56.2	80.0	762,821

Average monthly temperature observed between 1961 and 1995, for St. Helena, CA. See http://www.worldclimate.com

Average monthly reference evaporation rates for Zone 8, Inland San Fransisco Bay Area, typical rainfall year, CIMIS, DWR, 2001. See www.itrc.org.

Average monthly pan evaporation rates observed at Yountville, CA between 1962 and 1969.

d Pan evaporation rates adjusted by a factor of 0.77 to determine lake evaporation.

^e Average monthly rainfall observed between 1931 and 1995, for St. Helena, CA. See http://www.worldclimate.com

f Average monthly rainfall adjusted by the ratio of 10-yr and 100-yr wet year return storm identified by Pearsons Log III Distribution.

^g Assumed runoff area equal to 0.39 acres.

SUMMIT ENGINEERING, INC.	CONN CREEK UP ASSISTANCE	PROJECT NO.	2016030
Consulting Civil Engineers	PW System Review	BY:	SW
	Pond Worksheet	CHK:	GG

		Pond No.	<u>1</u>		
Bottom Width	35.0'	Bottom Radius	17.0'	Start Month	August
Bottom Length	135.0'	Top Radius	35.0'	Min. Depth	3.0'
Interior Side Slope (x:1)	2.0	Depth	10.0'	Annual PW	1.54 Mgal
Length:Width	0.3	Freeboard	2.0'	Initial Depth	10.0'

Depth	Length	Width	Radius	Surface Area (ft²)	Total Volume			
(ft)	(ft)	(ft)	(ft)	(11)	(Mgal)			
0	135	35	17	4,478	0.000			
1	139	39	19	5,119	0.036			
2	143	43	21	5,787	0.077			
3	147	47	22	6,480	0.123			
4	151	51	24	7,201	0.174			
5	155	55	26	7,948	0.230			
6	159	59	28	8,721	0.293			
7	163	63	30	9,521	0.361			
8	167	67	31	10,347	0.435			
9	171	71	33	11,200	0.516			
10	175	75	35	12,079	0.603			
11	179	79	35	13,095	0.697			
12	183	83	35	14,143	0.799			

SUMMIT ENGINEERING, INC
Consulting Civil Engineers

CONN CREEK UP ASSISTANCE PW System Review Pond Summary

PROJECT NO. 2016030 BY: SW CHK: GG

Pond No. 1

Month	Initial	Pond	PW Inflow	10 Year	Proposed	Volume	Total	Divert	Final	Final Pond	Volume	Surface Area	Infiltrati
	Volume	Evaporation		Precipitation	Storm	Change	Volume	Volume	Volume	Depth	Check		on ^a
					Inflow								
	(Mgal)	(Mgal)	(Mgal)	(Mgal)	(Mgal)	(Mgal)	(Mgal)	(Mgal)	(Mgal)	(ft)	(Mgal)	(ft ²)	(Mgal)
August	0.603	-0.042	0.125	0.001	0.002	0.087	0.690	0.087	0.603	10.0	0.087	12,079	-0.001
September	0.603	-0.037	0.182	0.004	0.007	0.156	0.759	0.156	0.603	10.0	0.156	12,079	-0.001
October	0.603	-0.022	0.253	0.021	0.040	0.292	0.894	0.292	0.603	10.0	0.292	12,079	-0.001
November	0.603	-0.011	0.166	0.046	0.089	0.289	0.892	0.289	0.603	10.0	0.289	12,079	-0.001
December	0.603	-0.008	0.100	0.074	0.144	0.310	0.913	0.310	0.603	10.0	0.310	12,079	-0.001
January	0.603	-0.009	0.108	0.090	0.175	0.365	0.968	0.365	0.603	10.0	0.365	12,079	-0.001
February	0.603	-0.012	0.117	0.066	0.129	0.300	0.903	0.300	0.603	10.0	0.300	12,079	-0.001
March	0.603	-0.020	0.086	0.055	0.107	0.228	0.831	0.228	0.603	10.0	0.228	12,079	-0.001
April	0.603	-0.024	0.101	0.025	0.049	0.150	0.753	0.150	0.603	10.0	0.150	12,079	-0.001
May	0.603	-0.034	0.099	0.008	0.016	0.089	0.692	0.089	0.603	10.0	0.089	12,079	-0.001
June	0.603	-0.038	0.111	0.002	0.005	0.080	0.683	0.080	0.603	10.0	0.080	12,079	-0.001
July	0.603	-0.052	0.095	0.000	0.000	0.044	0.646	0.044	0.603	10.0	0.044	12,079	-0.001
Total	<u> </u>	-0.309	1.543	0.392	0.763	2.389	·	2.389		·	2.389	<u> </u>	-0.012

Pond water balance was evaluated as a single unit (not per cell) since the cells are separated by a baffle and water level in the pond will change uniformly for all cells.

a Infiltration rate 1.0 x 10-6 cm/s through the pond liner

Pond Liner Permeability

1.00E-06 cm/s

SUMMIT ENGINEERING, INC. Consulting Civil Engineers Cons

Applied Irrigation Area Vineyard Pasture 2.0 acres acres

Total Area Available for Irrigation Vineyard Pasture acres acres

Month	Reference ET ^a	Pasture Crop	Vineyard	Pasture ET ^d	Vineyard	Precipitation ^e	Irrig	ation	Operating	Perco	olation	Assim	ilative	Efflu	ent	Excess
		Coefficient ^b	Crop		ET ^d		Demand ^f		Days per	Capacity ^h		Capacity ⁱ		Applied		Capacity
			Coefficient ^c						Month ^g							
	(in)			(in)	(in)	(in)	(in)	(Mgal)	(d)	(in)	(Mgal)	(in)	(Mgal)	(Mgal)	(in)	(Mgal)
August	5.9	0.9	0.5	5.3	2.6	0.2	3.0	0.203	31	29.76	2.022	32.8	2.225	0.087	1.28	2.14
September	5.2	0.9	0.3	4.7	1.3	0.5	1.5	0.102	30	28.80	1.956	30.3	2.058	0.156	2.29	1.90
October	3.3	0.9	0.1	3.0	0.2	2.9	0.0	0.000	16	15.36	1.043	15.4	1.043	0.292	4.29	0.75
November	1.1	0.8	0.0	0.8	0.0	6.5	0.0	0.000	14	13.44	0.913	13.4	0.913	0.289	4.26	0.62
December	1.2	0.8	0.0	1.0	0.0	10.6	0.0	0.000	5	4.80	0.326	4.8	0.326	0.310	4.57	0.02
January	0.8	0.8	0.0	0.6	0.0	12.9	0.0	0.000	6	5.76	0.391	5.8	0.391	0.365	5.38	0.03
February	2.3	0.8	0.0	1.8	0.0	9.5	0.0	0.000	5	4.80	0.326	4.8	0.326	0.300	4.42	0.03
March	3.6	0.8	0.0	2.9	0.0	7.8	0.0	0.000	12	11.52	0.783	11.5	0.783	0.228	3.35	0.55
April	5.2	0.9	0.2	4.7	0.8	3.6	0.0	0.000	13	12.48	0.848	12.5	0.848	0.150	2.22	0.70
May	6.7	0.9	0.6	6.0	3.9	1.2	3.2	0.215	16	15.36	1.043	18.5	1.259	0.089	1.31	1.17
June	7.0	0.9	0.7	6.3	5.0	0.3	4.9	0.334	17	16.32	1.109	21.2	1.442	0.080	1.18	1.36
July	6.9	0.9	0.6	6.2	4.4	0.0	4.8	0.324	30	28.80	1.956	33.6	2.281	0.044	0.64	2.24
Total	49.2		•	43.4	18.4	56.2	17.3	1.2	195.0	187.2	12.7	204.5	13.9	2.4	35.2	11.51

- (a) Average monthly reference evapotranspiration rates, see Climate Data Worksheet.
- (b) Kc coefficients for pasture from Table 5-1, "Irrigation with Reclaimed Municipal Wastewater-A Guidance Manual" California State Water Resources Control Board, July 1984 (San Joaquin Valley).
- (c) Kc coefficients for vineyards from Table 5-12, Irrigation with Reclaimed Municipal Wastewater A Guidance Manual, 84-1 wr, SWRCB.
- (d) ET=ETo x Kc. A weighted value is determined on the basis of the available irrigated acreage of vineyard and pasture.
- (e) Precipitation, 10-year rainfall event, see Climate Data Worksheet.
- (f) Irrigation Demand = ET-Precipitation, inches. A weighted value is determined on the basis of the available irrigated acreage of vineyard and pasture.
- (q) Number of operating days per month based on estimated irrigation days available based on 24-hr post storm criteria for a 100-year return period. Summit Engineering, NBRID Capacity Study, April 1996.
- (h) Design percolation rate is a maximum of 0.96 inches per day for the number of operating day per month. Design perc rate based on USDA soil survey data for the site, adjusted by a 0.04 safety factor to account for typical slow rate land application design methodology.
- (i) Assimilative capacity is the sum of irrigation demand and percolation applied.

Conn Creek Winery Wastewater Feasibility Study July 10, 2019

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