

# Water Availability Analysis

Flora Springs Winery P15-00111-MOD Planning Commission Hearing Date May 3, 2017



# WATER AVAILABILITY ANALYSIS FOR THE FLORA SPRINGS WINERY 1978 WEST ZINFANDEL LANE, ST. HELENA, CA 94574 PARCEL 4 (PREVIOUSLY APN 027-100-037)

As required by Napa County Planning, Building & Environmental Services (PBES), this analysis outlines the availability of groundwater for a potential staffing and marketing plan increase for Flora Springs Winery located at 1978 West Zinfandel Lane, St. Helena, CA 94574. The subject parcel, previously APN 027-100-037, has been distinguished as "Parcel 4" per the pending Lot Line Adjustment (reference #W15-00140).

# **PROJECT DESCRIPTION**

The  $168.8\pm$  acre subject parcel currently contains multiple winery buildings, a tasting room, offices, landscaped areas, miscellaneous structures associated with vineyard operations and  $30.4\pm$  acres of vineyard.

It is our understanding that the project proposes to modify the existing staff and marketing plan while continuing to operate an existing 120,000 gallon per year winery. The Applicant proposes 16 full-time employees, one (1) part-time employee and seven (7) harvest season employees. The Applicant also proposes to offer private tour and tasting appointments for a maximum number of 100 guests per day. Furthermore, the Applicant proposes to offer two (2) food and wine - lunch pairing events per week for parties up to 50 guests and two (2) food and wine - dinner pairing events per week for parties up to 25 guests. Additionally, the Applicant proposes to continue to host two (2) wine club events per week for groups of up to 50 guests. Wine club release events are proposed to occur three (3) times a year for parties up to 250 guests along with one (1) wine club release event - TRILOGY per year for parties up to 350 guests. Additionally, one (1) auction related event will occur per year for up to 60 guests.

To accommodate an increase in the staffing and marketing plan, two (2) domestic water storage tanks and one (1) septic tank are proposed for installation. Additionally, two (2) fire protection tanks will be installed as part of the project. An event parking plan has been prepared which includes required universal access parking. There are no planned improvements for the existing driveway.

### EXHIBITS

The associated USGS "Topographic Site Location Map" shows the project site and approximate property line locations. Information regarding the location of the existing wells and structures are shown on the associated Use Permit Drawings. Geological materials that underlay the subject parcel is shown on the attached "Geological Site Location Map". All exhibits and drawings mentioned above were prepared by Bartelt Engineering.



# WATER USE CRITERIA

TABLE 1: SCREENING CRITERIA	
Parcel Zoning	Agricultural Preserve (AP) - Westerly Portion Agricultural Watershed (AW) - Easterly Portion
Project Parcel Location	All Other Areas
Parcel Size	32.7± acres (zoned AP) 136.1± acres (zoned AW)
Water Use Criteria	Parcel Specific
Well and Spring Interference	No
Groundwater/Surface Water Interaction	No
Screening Tier	Tier 1

As summarized in Table 1, the subject parcel is partially located in AP and AW Zoning Districts. Per the PBES WAA-Guidance Document dated May 12, 2015 the water use criteria for a parcel located in the Napa Valley Floor and/or All Other Areas that are not designated as a groundwater deficient area without any well or spring interference must follow Tier 1 requirements. The water use criteria for the area of the project zoned AP is defined as 1 acre-feet per acre per year. The water use criteria for the area of the project zoned AP is considered in relation to the average annual recharge available to the project property.

# WATER DEMAND

# Estimated Water Use

The total water demand for the existing and proposed uses for the project is calculated below based on the *Guidelines for Estimating Residential and Non-residential Water Use* from the WAA Guidance Document (2015):



TABLE 2A: EXISTING WATER DEMAND						
Description	Estimated Water Usage (acre-feet/year)					
Winery (120,000 gallons per year)						
Process Water	2.58					
Domestic and Landscaping Water	0.60					
Tasting Room and Marketing Plan <sup>1</sup>	0.47					
Vineyard (30.4± acres)						
Irrigation	15.2					
Heat and Frost Protection	15.2					
Total Existing Water Demand =	34.05					

TABLE 2B: PROPOSED WATER DEMAND	
Description	Estimated Water Usage (acre-feet/year)
Winery (120,000 gallons per year)	
Process Water	2.58
Domestic and Landscaping Water	0.60
Tasting Room and Marketing Plan <sup>1</sup>	0.54
Vineyard (30.4± acres)	
Irrigation	15.2
Heat and Frost Protection	15.2
Total Proposed Water Demand =	34.12

As shown in Table 2A and Table 2B, the water demand is estimated to slightly increase from 34.05 acre feet per year to 34.12 acre feet per year as part of the proposed staffing and marking plan modification. Refer to the attached Table I and Table II for existing and proposed water demand calculations.

# SOURCE WATER INFORMATION

The subject parcel currently sources water from an existing spring as well as three (3) existing wells. A description of each water source is summarized below:

• The "winery well" is located on the subject parcel southwest of the existing winery and currently supplies domestic water to the existing office, tasting room and winery buildings.

<sup>&</sup>lt;sup>1</sup>The water demand is assumed to be equal to sanitary wastewater generated by the tasting room and marketing plan; refer to the Wastewater Feasibility Study prepared by Bartelt Engineering and submitted with the Use Permit Application for wastewater calculations.



- The "vineyard well" is located north of the existing winery on the neighboring parcel referenced as Parcel 3 per the pending Lot Line Adjustment (#W15-00140) and currently supplies irrigation and reserve domestic water.
- "Well 2" is located east of the existing winery on the neighboring parcel (APN 027-100-038) and provides irrigation water to the subject parcel.
- The spring is located on the subject parcel south of the existing winery and currently supplies irrigation water.

Prior to use, domestic water is proposed to be stored in two (2) 10,500 gallon storage tanks and irrigation water is stored in two (2) existing reservoirs. Furthermore, fire protection water is stored in two (2) proposed 10,500 gallon storage tanks as well as three (3) existing 10,000 gallon storage tanks (50,000 gallon total storage capacity).

The project proposes to use the "winery well" as the main project water source capable of meeting the water demand shown in Table 2B. The "vineyard well" is proposed to provide irrigation water and reserve (emergency) domestic water.

# Well Description

Per the Well Completion Report (Permit #E15-00851), the "winery well" was constructed in 2015 by Huckfeldt Well Drilling, Incorporated and has a recorded state well number of e020736. The well is reported to be constructed of 8 inch diameter PVC F480 casing to a completed depth of 617 feet with a 55 foot cement annular seal. Refer to the attached Well Completion Report for more information.

Per the Well Completion Report (Permit #E15-00755), the "vineyard well" was constructed in 2016 by Huckfeldt Well Drilling, Incorporated and has a recorded state well number of e020739. The well is reported to be constructed of 8 inch diameter PVC F480 casing to a completed depth of 700 feet with a 67 foot cement annular seal. Refer to the attached Well Completion Report for more information.

# <u>Yield Test</u>

A yield test was performed on the "winery well" by LGS Drilling, Incorporated in January 2016. Prior to the start of the yield test, static water level was recorded at 93 feet below surface. A sustained yield of 75 gallons per minute (gpm) was recorded after eight (8) hours of continuous pumping. Static water levels recovered to 109.50 feet below surface after 18 hours and 45 minutes of rest. Following completion of the yield test, a 50 gpm well pump was installed. Refer to the attached well yield test results for more information.

A yield test was performed on the "vineyard well" by LGS Drilling, Incorporated in March 2016. Prior to the start of the yield test, static water level was recorded at 173.3 feet below surface. A sustained yield of 325 gpm was recorded after eight (8) hours of continuous pumping. Static water levels recovered to 194.5 feet below surface after 30 minutes of rest. Following completion of the yield test, a 200 gpm well pump was installed. Refer to the attached well yield test results for more information.



# Water System Classification

Per PBES guidelines, the water system may be regulated as a transient non-community (TNC) public water system (PWS). A TNC public water system is identified as a water system that has less than five (5) connections, serves less than 25 yearlong residents<sup>2</sup> and serves 25 people per day at least 60 days per year. Refer to the Technical, Managerial and Financial (TMF) Capacity Worksheet included with the Use Permit Application for further information regarding the PWS.

# Neighboring Water Source(s)

Based on review of neighboring property records at Napa County PBES and discussions with PBES staff, there does not appear to be any neighboring wells located within 500 feet of the proposed project well. Refer to the associated "Use Permit Drawings" prepared by Bartelt Engineering for location of the existing onsite wells, neighboring wells and nearby creeks.

# Water Quality

A water quality analysis was performed on the existing wells in 2016 by CalTest Analytical Laboratory. The water analysis for the "winery well" showed good water quality with primary constituents (Arsenic and Fluoride) testing below the Maximum Containment Levels (MCLs) set by the EPA Safe Drinking Water Act for a regulated PWS. Iron levels were non-detectable, however Manganese levels were reported above the secondary MCL. Elevated Manganese levels can cause aesthetic issues in and around the water system as well as near areas of use. Manganese removal is therefore recommended to be incorporated into the water treatment system. The water analysis does not reflect a full analysis of all required constituents for a PWS. Refer to the attached water quality results for more information.

# **GROUNDWATER OVERVIEW**

According to the Napa County Watershed Information & Conservation Council (WICC), the subject parcel is partially located in the St. Helena Groundwater Subarea and the Western Mountains Groundwater Subarea of Napa County.

The St. Helena Subarea located in the Napa Valley Floor is reported to have geology primarily consisting of alluvial sediments, such as clay, silt and sand. Groundwater levels in the wells monitored by WICC were observed to be frequently very shallow at less than 10 feet below the ground surface during the spring season. Declines of about 20 feet were observed between the spring and fall seasons. Groundwater quality was observed to be generally good with some well samples exceeding constituent standards including various metals and minerals.

The Western Mountain Subarea includes some volcanic rocks with additional exposures of the sedimentary Great Valley Sequence and metamorphic Franciscan Complex. The Napa County Groundwater Monitoring Program tested wells in this area in 2014 and 2015. The observed groundwater depth in these wells ranged from 44 feet to 240 feet below ground surface. Ground elevations range from 390 feet to 1,660 feet, mean sea

<sup>&</sup>lt;sup>2</sup> Yearlong resident is considered an individual served by the water system for 183 or more days annually.



level. The groundwater quality available in this subarea is reported to be generally of good quality. Elevated levels of iron and manganese occur, along with lower than average pH indicating more acidity than the Napa Valley Floor.

# **GEOLOGICAL FEATURES**

The attached "Geological Site Location Map" prepared by Bartelt Engineering shows the parcel boundary, approximate well locations and surrounding geologic materials. The background for the exhibit is sourced from the "USGS Geological Map and Map Database of Eastern Sonoma and Western Napa Counties, California" by Graymer et al. (2007). The prominent geological materials in the project area appear to be predominantly Surficial Deposits (map unit Qf and Qls) and Sonoma Volcanics (map unit Tsr)

*Figure 5-3 Cross Section A-A' Northern NVF-St. Helena Subarea, Napa County, CA* from "Updated Hydrogeologic Conceptualization and Characterization of Conditions" by Luhdorff and Scalamini (L&S) in 2013 shows the subsurface geology along Zinfandel Lane. Side A of the cross section is in the proximity of the subject parcel location and existing wells. The cross-section is based on review of well completion reports along the cross-section location. The geological materials in the cross-section and geological maps show a fault line near the subject parcel. Refer to the attached Cross-Section A-A' for more information.

Per the Napa County Baseline Data Report (2005), Sonoma Volcanics consist of dacite, rhyolite and andesite rock types. These rocks are exposed over much of Napa Valley and are the second most commonly exposed rocks in Napa County. In terms of groundwater resources, tuffaceous units within the Sonoma Volcanics host significant volumes of groundwater under both confined and unconfined conditions. Furthermore, surficial deposits consist of the formation of stream channel deposits, alluvium, terrace deposits, alluvial fan deposits, landslide deposits, basing deposits, bay mud, and artificial fill. In term of groundwater resources, surficial deposits are reported to be typical pathways for groundwater recharge and, depending on the properties and depths of the surficial deposits, may hold groundwater to varying capacity. Within the Napa Valley Floor, the majority of the groundwater is hosted within these deposits.

# NAPA VALLEY FLOOR ALLOWABLE WATER ALLOTMENT

Per *Table 2A: Water Use Criteria* from the WAA Guidance Document (2015), the water use criteria for a parcel located in the Napa Valley Floor is defined as 1 acre-feet per acre per year. The area of the parcel zoned AP ( $32.7\pm$  acres) is assumed to be located in the Napa Valley Floor. The remainder of the parcel ( $136.1\pm$  acres) is zoned AW and assumed to be located in All Other Areas. This assumption is based on USGS topographic information and the Napa County General Plan mapping. The allowable water allotment for the applicable area is calculated below.

Allowable Water Allotment (acre-ft/yr) =

Napa Valley Floor parcel area (acres) x Water use criteria (acre-ft/acre-yr)

= 32.7 acres x 1 acre-ft/acres-yr = 32.7 acre-ft/yr



The allowable water allotment for the area of the subject parcel located in the Napa Valley Floor is estimated to be 32.7 acre feet per year.

# ALL OTHER AREAS ESTIMATED GROUNDWATER RECHARGE RATE

The allowable water allotment for the area of the parcel located in All Other Areas is determined by estimating groundwater recharge. Groundwater recharge can be estimated by understanding the soil properties and geological materials present and their ability to percolate groundwater to the saturated zone of the aquifer. Water flowing into the ground consists primarily of recharge from precipitation, surface water seepage and artificial recharge. Water flowing out of the ground primary involves extraction from wells, spring discharge and evapotranspiration. In Napa County, precipitation has been primarily established as the primary source of groundwater (Kunkel and Upson, 1960). Since the subject parcel is partially located in the St. Helena and Western Mountains Groundwater Subarea with no surrounding creeks located in the proximity of the project area, direct infiltration from rainfall is likely to be the most significant factor for groundwater, this analysis models groundwater recharge as a percent of rainfall. The amount of rainfall that is estimated to recharge groundwater is impacted by a number of factors. Some of these factors include precipitation, soil properties and underlain geological materials.

# **Precipitation**

Precipitation, or rainfall, data used in this analysis is taken from two (2) sources: the PRISM Climate Group at Oregon State University and the National Climate Data Center (NCDC). The PRISM Climate Group provides spatial climate datasets for selected 800 meter or 400 kilometer (km) grid cell(s). The average annual recorded rainfall data from 1981-2010 (30-year normals) for the project location selected from two (2) 800 spatial grid cells and averaged is 36.5 inches. The NCDC rainfall data collected rainfall from a cooperative weather station in St. Helena from 1961-1990. The average recorded rainfall over this time period was 34.9 inches.

Average rainfall data from PRISM recorded over the past ten (10) years provides more recent rainfall data and shows variation between drought, dry and wet years. The 10-year average (2014 to 2004) from a 400 km spatial grid cell which includes the project location is shown in the following table.



TABLE 3: 10-YR AVERAGE RAINFALL					
Month	PRISM Rainfall (inches)				
2014	42.2				
2013	7.8				
2012	47.6				
2011	35.8				
2010	55.2				
2009	29.3				
2008	29.2				
2007	22.0				
2006	43.7				
2005	53.9				
2004	38.6				
AVERAGE	36.8				

Based on the rainfall data shown in the above table, it appears rainfall outside of the normal trend occurred in 2013 as a drought year and in 2005 as a very wet year. A typical dry year occurred in 2007 with 22.0 inches of recorded rainfall and a typical wet year occurred in 2012 with 47.6 inches of recorded rainfall.

For estimating groundwater recharge, this analysis uses the most conservative rainfall data series which in this case is the 30-yr normal average rainfall amount recorded from the NCDC Cooperative Weather Station in St. Helena (34.9 inches). Refer to the attached Rainfall (Table III) for a summary of rainfall data from all sources.

# Hydrologic Soil Groups

Per the USDA, hydrologic soil groups (HSG) are based on estimated potential for runoff. Soils are assigned four (4) groups (A, B, C and D) depending on the ability of water to infiltrate the soil. Group A soils have a high infiltration rate (low runoff potential) and group D has very slow infiltrative rates (high runoff potential). The infiltration rate is also affected by site slopes; higher slopes limit the time water is available for infiltration.

A custom soils report was generated by the NRCS Web Soil survey for the subject parcel. The survey shows that several soil types, HSGs and land slopes are present. Applying a weighted total to the infiltrative properties, the subject parcel has an overall "slow" infiltrative rate of 0.11 inches per hour and a corresponding "C" HSG. Refer to the attached Custom Soil Report for more information regarding soil properties.

# Average Year Groundwater Recharge Rate

Based on review of several groundwater publications and WAA prepared for similar type projects, a percent of precipitation is assumed to be available for groundwater recharge. These publications include studies for City of Santa Rosa watersheds as well as Environmental Impact Reports (EIR) for large scale projects. Below is a summary of these



references and comparison to the geological materials and HSGs present on the merged subject parcel:

- The "Groundwater Study" for the 2009 Napa Pipe Project EIR prepared by others, estimates 10.5% of precipitation is available for groundwater recharge in Sonoma Volcanics.
- The "Santa Rosa Plan Watershed Groundwater Management Plan 2014" prepared by the Santa Rosa Plan Basin Advisor Panel includes a specified yield of 0-15% for Sonoma Volcanics. Specified yield refers to the amount of water contained in the saturated zone that flows by gravity and is available to wells (Johnson 1967).
- WAA prepared for the Wools Ranch Winery by L&S dated 2014 includes a 10% recharge rate for a parcel with primarily slow and some moderate infiltrative soil properties.

Based on the methodology utilized in these studies, a conservative groundwater recharge could be 10% of annual precipitation. A conservative estimate for the project site recharge area is assumed to be equal to the area of the subject parcel located in All Other Areas as well as underlain with Sonoma Volcanics. Of the 136.1 $\pm$  acres designated as All Other Areas, approximately 56.1 $\pm$  acres appear to be underlain with Sonoma Volcanics<sup>3</sup>. The volume of rainwater that is estimated to be available for groundwater recharge in this area is calculated below:

Annual recharge (acre-ft/yr) = Recharge area (acres) x Precipitation (ft) X Recharge rate

= 56.1 acres x (34.9 in x 1 ft/12 in) x 10%

= 16.3 acre-ft/yr

The estimated annual recharge for the area of the subject parcel zoned AW and located in All Other Areas is estimated to be 16.3 acre-feet per year.

# Dry Year Recharge Rate(s)

When modeling groundwater recharge as a percentage of rainfall, dry rainfall years should also be evaluated. A drought year occurred in 2013 with only 7.8 inches of recorded precipitation near the project area according to the PRISM Database (see Table 3). This is a significantly low rainfall year and is not considered to represent historical rainfall patterns. Applying the recharge rate to the recharge area discussed above as a percentage of rainfall, the potential groundwater available during a typical dry year (2013) is 10.3 acre-feet per year.

# SUMMARY

The available water for the subject parcel is the combination of the allowable water allotment for the area of the subject parcel located in the Napa Valley Floor as well as the estimated groundwater recharge for the area located in All Other Areas and underlain with Sonoma Volcanics. The available water for the subject parcel is estimated to be between

<sup>&</sup>lt;sup>3</sup> Refer to the attached "Geological Site Map" for map of geological materials reported to be present at the merged subject parcel.



49.9 acre-feet per year and 49.0 acre-feet per year during average rainfall years. During dry rainfall years the estimated groundwater recharge could reduce to 43.0 acre-feet per year.

### CONCLUSION

The groundwater demand generated as a result of the proposed staffing and marketing plan increase for the existing winery is estimated to slightly increase from 34.05 acre-feet per year (see Table 2A) to 34.12 acre-feet per year (see Table 2B). Groundwater is proposed to be sourced from the existing onsite "winery well" which has a reported pumping rate of 50 gpm. The existing "vineyard well", which has a reported pumping rate of 200 gpm, is proposed to continue providing irrigation water and reserve (emergency) domestic water to the subject parcel. The estimated available water for the project area is estimated to be around 49.0 acre-feet per year on average. Even during a dry rainfall year, the estimated available water of 43.0 acre-feet per year.

The above analysis shows that the increase in groundwater demand can feasibly be sourced by the existing project wells. Furthermore, the estimated available water for the subject parcel satisfies the Tier 1 Water Use Criterion of the Napa County Water Availability Analysis.

### **ATTACHMENTS**

Geological Site Map

Geological Cross-Section Location Map

Cross Section A-A' Northern NVF-St. Helena Subarea

Table I – Existing Water Demand

Table II – Proposed Water Demand

Table III – Rainfall

Table IV – Soil Group Properties

Table V – Water Availability

Well Completion Reports & Yield Test Results

Water Quality Data

Custom Soil Report

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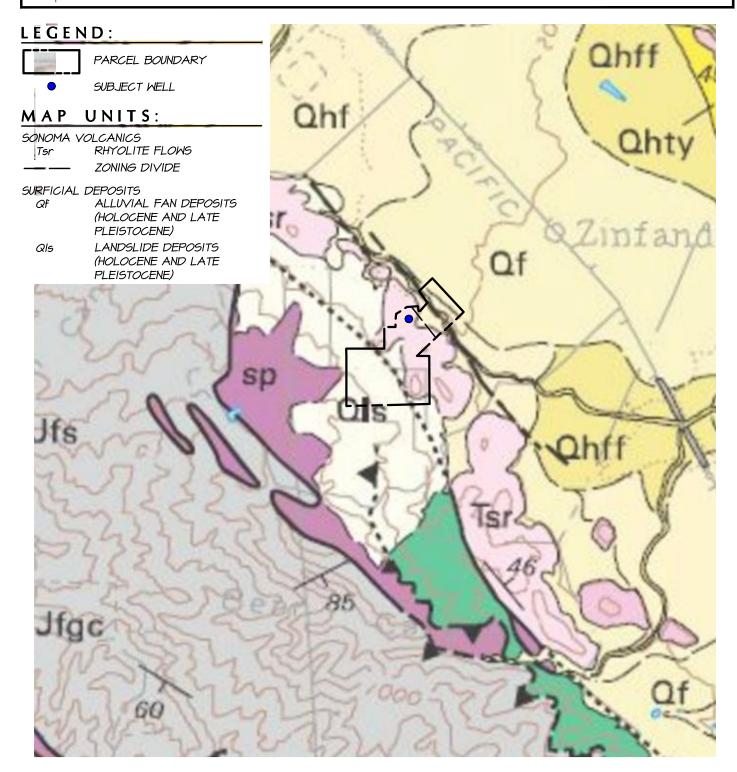


# References

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# GEOLOGICAL SITE MAP FROM USGS GEOLOGICAL MAP AND MAP DATABASE OF EASTERN SONOMA AND WESTERN NAPA COUNTIES, CALIFORNIA

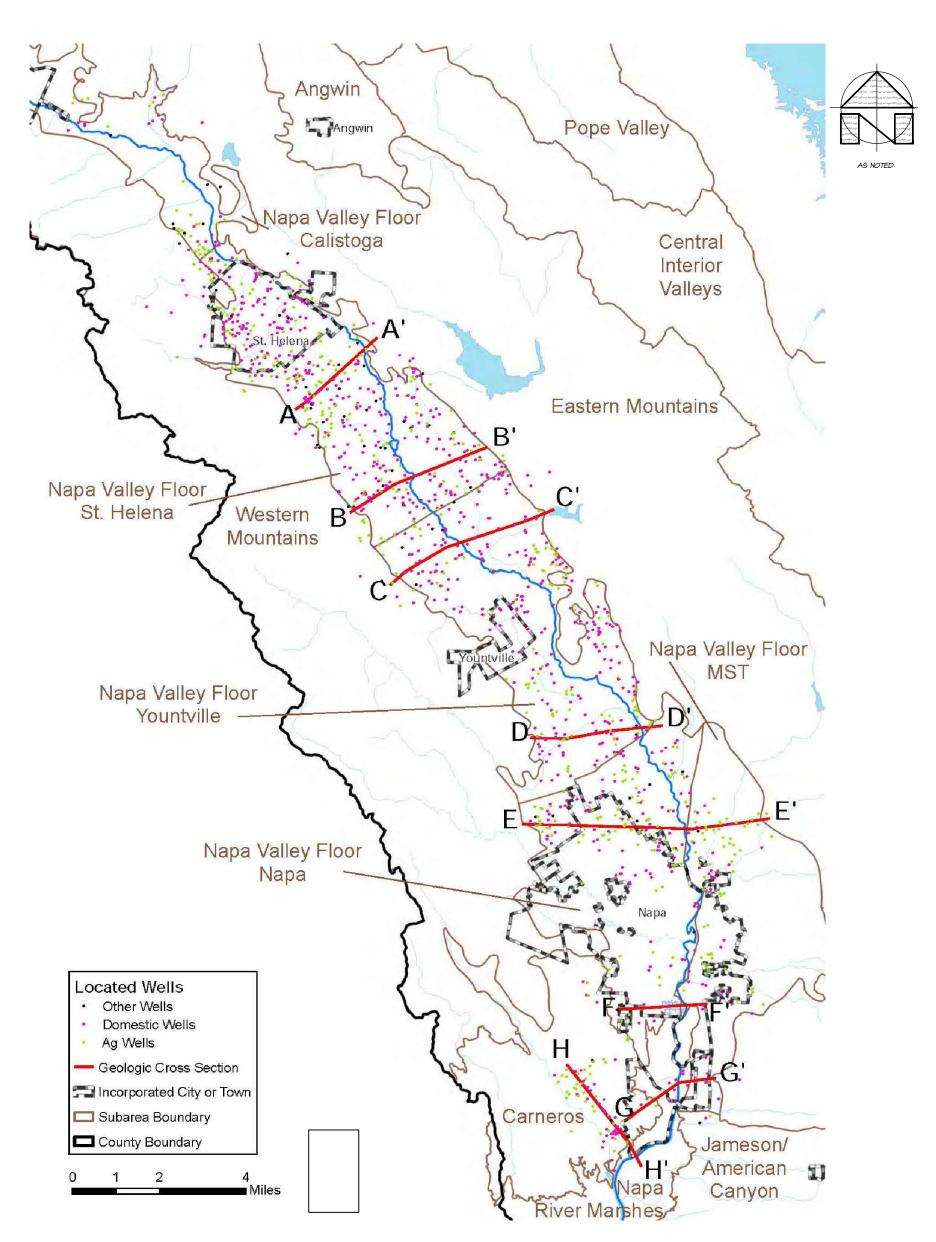
Scale: 1" = 3000'





Flora Springs Winery 1978 West Zinfandel Lane St. Helena, California "Parcel 4" Job No. 96-19

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# GEOLOGICAL CROSS SECTION LOCATION MAP

SCALE: AS NOTED

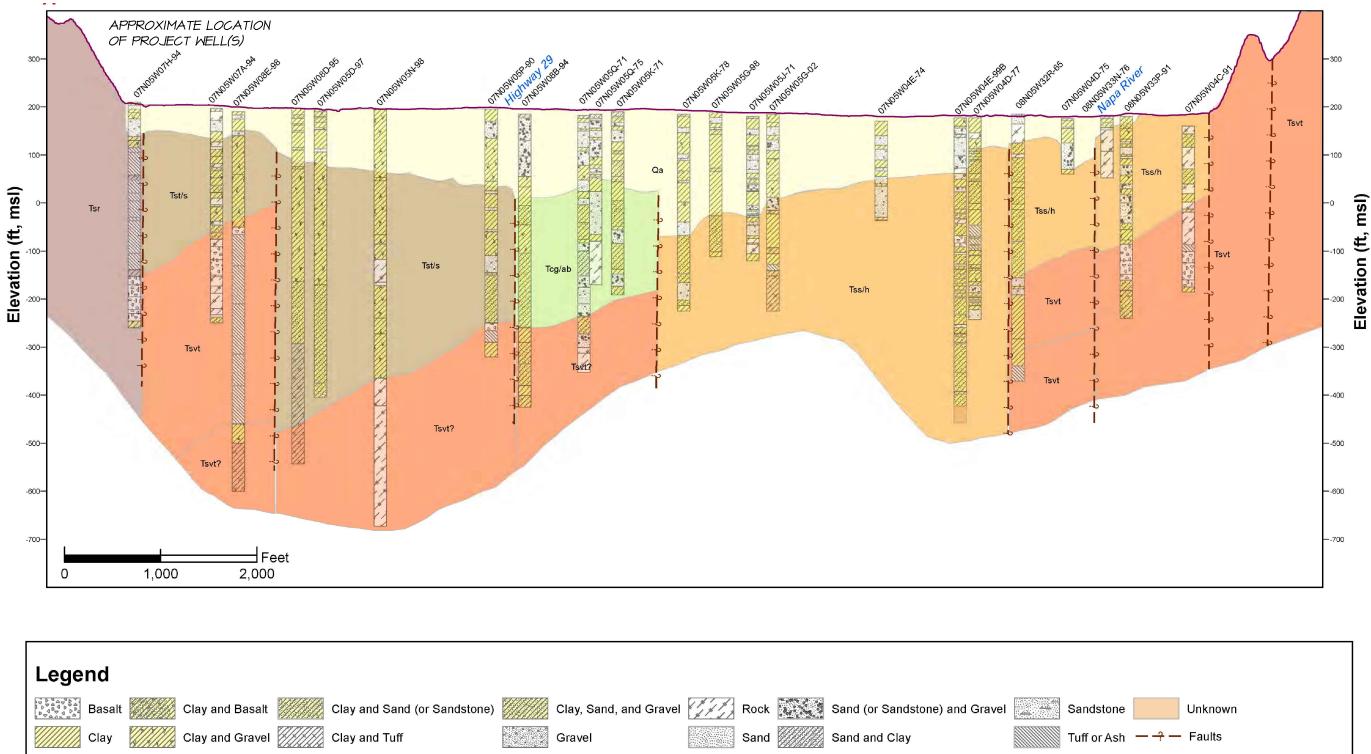
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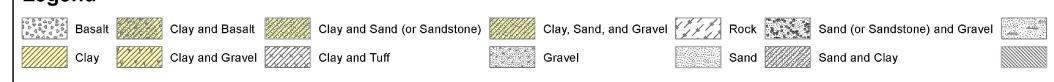
THE MAP USED AS A BASE FOR THIS EXHIBIT WAS REFERENCED FROM LUHDORFF & SCALMANINI CONSULTING ENGINEERS AND MBK ENGINEERS UPDATED HYDROGEOLOGICAL CONCEPTUALIZATION AND CHARACTERIZATION OF CONDITIONS PREPARED FOR NAPA COUNTY (JANUARY 2013).



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# CROSS SECTION A-A' NORTHERN NVF-ST. HELENA SUBAREA

SCALE: |" = 1,000'

# NOTE:

CROSS SECTION A-A' USED AS A BASE FOR THIS EXHIBIT WAS REFERENCED FROM LUHDORFF & SCALMANINI CONSULTING ENGINEERS AND MBK ENGINEERS UPDATED HYDROGEOLOGICAL CONCEPTUALIZATION AND CHARACTERIZATION OF CONDITIONS PREPARED FOR NAPA COUNTY (JANUARY 2013).

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# Flora Springs Winery Existing Water Demand Table I



Winery Production Limit: Vineyard Area:

#### 120,000 gallons/year 30.4 acres

EXISTING WATER DEMAND					
Description	Water Usage Rate <sup>1</sup>	Water Demand (acre-feet/year)			
Residential					
Primary Residence	0.75 acre-feet/acre-year	-			
Secondary Residence or					
Farm Labor Dwelling	0.5 acre-feet/acre-year	-			
Agricultural					
Vineyards					
Irrigation Only	0.5 acre-feet/acre-year	15.20			
Heat Protection	0.25 acre-feet/acre-year	7.60			
Frost Protection	0.25 acre-feet/acre-year	7.60			
Irrigated Pastures	4 acre-feet/acre-year	-			
Orchards	4 acre-feet/acre-year	-			
Livestock (sheep or cows)	0.01 acre-feet/acre-year	-			
Winery					
Process Water	2.15 acre-feet/100,000 gallon of wine	2.58			
Domestic & Landscaping	0.5 acre-feet/100,000 gallon of wine	0.60			
Tasting Room and Marketing Plan <sup>2</sup>		0.47			
Industrial					
Food Processing	31 acre-feet/employee-year	-			
Printing/Publishing	0.06 acre-feet/employee-year				
Commercial		-			
Office Space	0.01 acre-feet/employee-year	-			
Warehouse	0.05 acre-feet/employee-year	-			

Estimated Existing Water Demand (acre-feet/year):34.05Estimated Existing Water Demand (gallons/year):11,095,227

1) Water usage rates referenced from *Appendix B: Estimated Water Use of Specified Land Use* from Napa County WAA-Guidance Document (2015)

2) Water demand is assumed to equal wastewater generation rates; refer to the Wastewater Feasibility Study prepared by Bartelt Engineering and submitted with the Use Permit Application for calculations May 2016 Job No. 96-19

# Flora Springs Winery Proposed Water Demand Table II



Winery Production Limit: Vineyard Area: 120,000 gallons/year 30.4 acres

#### PROPOSED WATER DEMAND Water Demand Description Water Usage Rate<sup>1</sup> (acre-feet/year) Residential **Primary Residence** 0.75 acre-feet/acre-year Secondary Residence or Farm Labor Dwelling 0.5 acre-feet/acre-year <u>Agricultural</u> Vineyards Irrigation Only 0.5 acre-feet/acre-year 15.2 Heat Protection 0.25 acre-feet/acre-year 7.6 **Frost Protection** 0.25 acre-feet/acre-year 7.6 **Irrigated Pastures** 4 acre-feet/acre-year Orchards 4 acre-feet/acre-year Livestock (sheep or cows) 0.01 acre-feet/acre-year <u>Winery</u> **Process Water** 2.15 acre-feet/100,000 gallon of wine 2.58 0.5 acre-feet/100,000 gallon of wine Domestic & Landscaping 0.6 Tasting Room and Marketing Plan<sup>2</sup> 0.54 <u>Industrial</u> **Food Processing** 31 acre-feet/employee-year Printing/Publishing 0.06 acre-feet/employee-year <u>Commercial</u> Office Space 0.01 acre-feet/employee-year Warehouse 0.05 acre-feet/employee-year

Estimated Proposed Water Demand (acre-feet/year):34.12Estimated Proposed Water Demand (gallons/year):11,118,036

1) Water usage rates referenced from *Appendix B: Estimated Water Use of Specified Land Use* from Napa County WAA-Guidance Document (2015)

2) Water demand is assumed to equal wastewater generation rates; refer to the Wastewater Feasibility Study prepared by Bartelt Engineering and submitted with the Use Permit Application for calculations

Flora Springs Winery
Water Balance

Proposed Water Demand



AVERAGE MONTHLY RAINFALL RATES						
	PRISM	NCDC				
	Rainfall <sup>1</sup>	Rainfall <sup>2</sup>				
Month	(inches)	(inches)				
September	0.3	0.4				
October	1.8	2.1				
November	4.3	5.5				
December	7.4	5.9				
January	6.8	7.9				
February	7.4	5.9				
March	5.2	4.7				
April	2.0	1.9				
May	1.1	0.4				
June	0.2	0.1				
July	0.0	0.0				
August	0.1	0.1				
TOTALS	36.5	34.9				

1) PRISM 30-year normall rainfall data from 1981-2010 averaged from two (2) 800  $\textrm{m}^2$ 

spatial grids that emcompass the total project area; see http://prism.oregonstate.edu/

2) Site rainfall from St. Helena, CA (NCDC Cooperative Stations 1961-1990);

see www.worldclimate.com

10-YR AVERAGE RAINFALL				
	PRISM			
	Rainfall <sup>1</sup>			
Year	(inches)			
2014	42.2			
2013	7.8			
2012	47.6			
2011	35.8			
2010	55.2			
2009	29.3			
2008	29.2			
2007	22.0			
2006	43.7			
2005	53.9			
2004	38.6			
AVERAGE	36.8			

1) PRISM yearly rainfall data from 2007-2014 from one (1) 400 km

spatial grids which emcompass the total project area; see http://prism.oregonstate.edu/

May 2016 Job No. 96-19

# Flora Springs Winery Soil Group Properties Table IV



Map Unit	Map Unit Name	Slope Range	Hydrologic Rating Group	Acres in AOI	Percent of AOI	Infiltrat	on Rate	Estimated Infiltration Rate	Weighted Infiltration Rate
				(acres)	(%)	(in/	′hr)	(in/hr)	(in/hr)
138	Forward gravelly loam	2-9%	В	0.3	0.1%	Moderate	0.15-0.30	0.23	0.0002
139	Forward gravelly loam	9-30%	В	7.0	4.2%	Moderate	0.15-0.30	0.23	0.0097
140	Forward gravelly loam	30-75%	В	44.7	26.5%	Moderate	0.15-0.30	0.23	0.0610
151	Hambright-Rock outcrop complex	2-30%	D	0.8	0.5%	Very Slow	< 0.05	0.05	0.0003
154	Henneke gravelly loam	30-75%	D	67.5	40.0%	Very Slow	< 0.05	0.05	0.0200
161	Maxwell clay	2-9%	D	24.4	14.5%	Very Slow	< 0.05	0.05	0.0073
166	Montara clay loam	5-30%	D	5.5	3.3%	Very Slow	< 0.05	0.05	0.0017
169	Perkins gravelly loam	5-9%	С	6.7	4.0%	Slow	0.05-0.15	0.10	0.0040
170	Pleasanton loam	0-2%	С	11.8	7.0%	Slow	0.05-0.15	0.10	0.0070

1) Hydrologic Soil Groups (HSGs) are based on USDA/NRCS Web Soil Survey for the project Area of Interest (AOI)

2) Infiltration Rates for each HSG is referenced from the USDA Urban Hydrology for Small Watersheds, Technical Release 55, June 1986.

Flora Springs Winery Water Balance

# Flora Springs Winery Water Availability Table V



Total Parcel Size:

Napa Valley Floor Parcel Size (zoned AP) All Other Areas Parcel Size (zoned AW) 168.8 acres 32.7 acres 136.1 acres

ALLOWABLE WATER ALLOTMENT - NAPA VALLEY FLOOR						
Applicable Parcel Size Water Use Criteria Water Allotment						
(acres) (acre-feet/acre-year) (acre-feet/year)						
32.7	32.7					

GROUNDWATER RECHARGE - ALL OTHER AREAS								
Scenario	Sonoma Volcanics Recharge Area <sup>2</sup>	Sonoma Volcanics Recharge Rate	Estimated Recharge					
	(inches)	(feet)	(acres)	(%)	(acre-ft/year)			
10-year Average	36.8	3.1	56.1	10%	17.2			
NCDC 30-year Average	34.9	2.9	56.1	10%	16.3			

1) Refer to Table I - Rainfall Data

2) Portion of All Other Areas that appears to be underlain with Sonoma Volcanics, refer to attached Geological Site Location Map for more information

TOTAL WATER AVAILABILITY								
Estimated								
	Water Allotment	Recharge	Total Water	<sup>•</sup> Availability				
Scenario	(acre-feet/year)	(acre-ft/year)	(acre-ft/year)	(gallons/year)				
10-year Average	32.7	17.2	49.9	16,266,946				
NCDC 30-year Average	32.7	16.3	49.0	15,971,831				
Typical Dry Year (2007)	32.7	10.3	43.0	13,999,088				

ORIGINAL	The second second							STAT	ΕO	F CAL	IFORN			[	DWR USE	ONLY	<u> </u>	DO M	NOT FILL IN
File with D	WR					WI		COM					POR	T   💷					
Page 1 of 1								Refer to							ST	ATE WE	ELL NO./	STATIC	N NO.
Owner's V	Vell No.	1-2015							No.	02	07	36							
Date Work	Began _1	1/3/201	5		,	Ende	12/16/2	2015						<b></b>	LATITUDE		1	LON	IGITUDE
Local Pe	ermit Ag	ency Na	apa (	Cou	nty	Enviro	nmenta	al Mgm	t					-   []				11	
Permit	No. E1	5-00581					Permit	Date	1/3	8/201	5					API	N/TRS/O	THER	
		(	GEO	LOC	GIC	LOG				10			/	-	WELL O	WNER	· —		
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195		FRACT											1.027	Page <u>1</u>	00	Danaal	037		
210	and the second se	GRAY \		In Concession, Name of Street, or other				and the state of t		GERS	S A	APN BOO	K UZ I	Page <u>1</u>	00	Parcer	001		
270		MIXED									- 1			Range		Section		1	
280		TAN, G						+ STRI	NG	FRS		Latitude _	DEG. N	VIN. SE	C.		C	DEG.	MIN. SEC.
320		TAN SA	State of the second second										- LO	CATION S					TIVITY (⊻) —
330		RED SA												NORTH				N	EW WELL
335		RED VO				OCK								$\wedge$					CATION/REPAIR
		FRACT					CANIC	c							\				<ul> <li>Deepen</li> <li>Other (Specify)</li> </ul>
350		BROW					CANIC	3					/	/					
360													/		$\backslash$			DE	ESTROY (Describe rocedures and Materials inder "GEOLOGIC LOG"
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555		HARD									5				and "				TEST WELL
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600	620	WHITE	SAN	<b>IDA</b>	VO	LCAN	IIC ASH	1					f	OND-1	1 7			н	EAT EXCHANGE
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556		BLANK		PVC											durate a construction of the				
576	596	SCREE	EN P	vVC	8"	.032	SLOT							R LEVEL					
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												DEPTH OF	STATIC 70	9				12/16	/2015
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TOTAL DE					1-	,	(Feet)												
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	ATTACH - Geologic		(⊻)	-			the under	signed occ	16, 1	at this	report in			ATION ST ate to the best			heliof		
	-	nstruction D	iagram	1			NAME -	IUCKFE	ELD	T WE	LL DF	RILLING,	INC.		St my knowle	-90 and	56/101.		
	A (8)	cal Log(s)								OR COR	PORAT	TION) (TYPE	ED OR PR		lanc			~^	04550
	<ul> <li>Soil/Wate</li> <li>Other</li> </ul>	r Chemical	Analy	/SIS			2110 Pe ADDRESS	any Lai	ie -	1.1		Mad	IAL		Napa CITY			CA STATE	94559 ZIP
ATTACH AD			ON, IF	IT EXI	STS.		Signed			W	W	NWM	MA			2/29/1		4	139-746
DWR 188 REV												REPRESEN		NUMBERED		TE SIG	NED		C-57 LICENSE NUMBER
				/			J. HULI		-10,	JUL IN									

Tradition of Stewardship			Planning, Build	ling & Environmental Service 1195 Third Street, Suite 2 Napa CA 945 www.countyofnapa.c (707) 253-44 David Morrise Direct
Application Type: Permit Number: Parcel Number:	Environmental / EM E15-00581 027-100-037-000	Permits / Water Wells	/ Class I Applied Date Issued Date Expiration Date	: 11/3/2015
Site Address: Owner: Address: Applicant:	1978 W Zinfandel Lr JMK-A LLC ETAL ATTN JOHN KOME Don Huckfeldt		Phor	Energy Andrewski andre
Business Name: Project Type:	HUCKFELDT WEL	DRILLING INC		nse #: 439746
Proposed Use: Use: Well To Service T	his Parcel Only?:	Private Yes	Name of Public Water System:	
Water Supply: Septic Setbacks M Actual Approved S Emergency Exem	Setback:	Yes	Well Located in Flood Zone?: Hazmat Site Within 1500 feet?:	No No
Reason For Emerg	gency Exemption:			
Specifications: Casing Diameter:		8.00 ln.	Method of Seal Placement:	Pump
Boring Diameter: Annular Seal:		15.00 ln. 3.00 ln.	Minimum Seal Depth: Material:	50.00 Ft. Concrete

Any work performed or operations conducted under the auspices of this permit constitutes acceptance of all conditions, inspections and comments contained in the this permit, and the incorporation of all requirements as set forth jn the permit application.

15

11



11-Mar-16

Sean P. Garvey 1889 West Zinfandel Lane St. Helena, CA 94574

Att. Sean Garvey

R.E. Komes - Garvey Well Development & Pump Testing of Well #2 - 700' deep

Well #2 at Flora Springs was developed and a pump test @ 325 GPM was preformed.

The well was mechanically developed by airlift swabbing and the use of a 10' isolation tool to remove mud from the well screens, a total of 30 hours were required to clean 480 feet of screens. Aprox. 100,000 gallons were removed by airlift / swabbing.

Pumping development was done by a 50 hp pump set at 495 feet, the pump was surged turned off to let back-wash into screens, Aprox 315,000 Gallons were pumped during pump development.

The well was pumped at a constant rate of 325 GPM for 8 hours, the final draw down was 215 feet. The estimated draw down after 24 hours would be 275 feet. A water sample was taken to Cal Test.

Given the pumping data I would recommend the following:

- A. Set the permanent pump at 490'
- B. A 25 hp 200 gpm pump like a 2308-250-9 Grundfos would be a good choice for a permanent pump, curve included.
- C. Static (non pumping) water levels were lower every day after pumping, it may be necessary to monitor pumping levels during a full season of pumping and adjust pumping rates accordingly.

Please feel free to call me with any questions. 530-681-2012

Scott Smith

LGS Drilling, Inc.



а	Date:3-9-16				Job No: Flora Springs #2
1	WELL ID: 201		Remarks:		Sheet 1 of 1
	VVELL ID. 201	10-2	Well Depth		Observers
	GPS:		Pump Set	495	
	0/ 0.	and the second secon		50 hp / 325 g	
			It dilip th	TYPE OF TE	ST
				ate @ 325 gpi	
	Time	Elapsed		Depth below	Remarks
	of Day	Time	water from	static level.	
		min. sec.		(ft)	T=27,774,800
9-Mar	6:30		173.3	0	325 GPM
	6:35		191.9		
	6:45		193.7		
	7:00		194.6		
	7:30		195.6		
	8:30		195.8		325 GPM
	9:30 10:30		197.6 199.8		
	11:30		203.3		Sample Taken 80*
	12:30		207.2		Gample Taken oo
	13:30		211.2		325 GPM
	14:30		215.4		T=27,930,800
					Land Land Land Land Land Land Land Land
recovery	14:40		197.8		
-	15:00		194.5		
3/11/16			168.3		
3/14/16	9:00		160.5		Static on 2-29-16 before pumping 158.0
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# PERFORMANCE CURVES

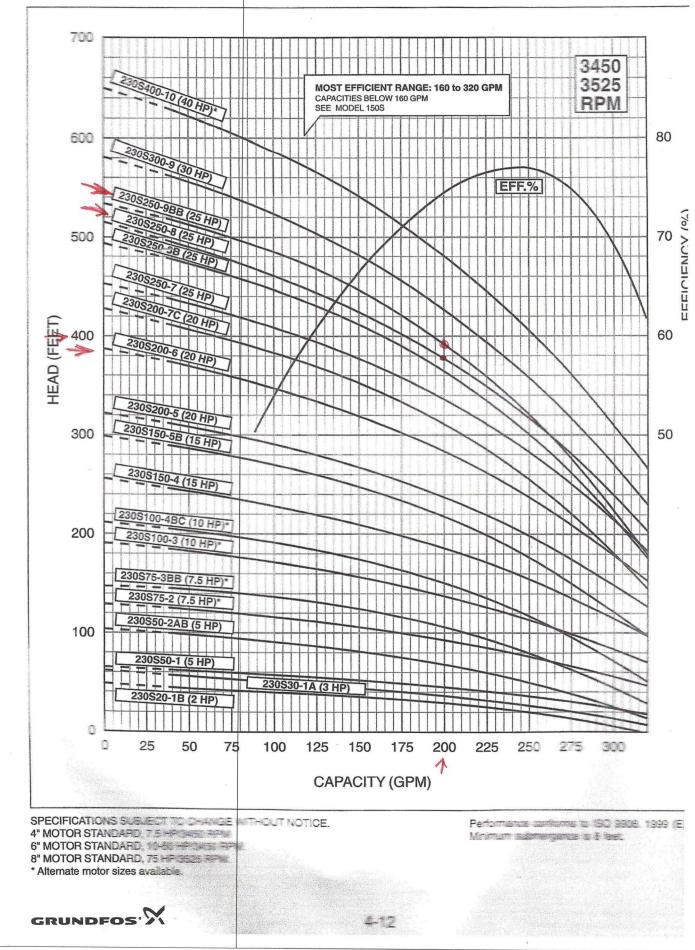
# 230 GPM

# MODEL 2

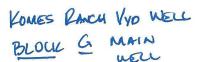


**OUTLET SIZE: 3" NPT** 

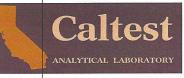
### NOMINAL D



### NELAP/ORELAP Certification 4036



Lab Order: R030478 Project ID: FLORA SPRINGS #2-2016



#### ENVIRONMENTAL ANALYSES

#### ANALYTICAL RESULTS

							n kala shekara ka asala na anga dan sebaga ya kananga a sa Mana ya kananga na kananga ka kananga k	
Lab ID R030478001	Date Collected	3/9	2016 11:45	Matrix	Water			
Sample ID FLORA SPRINGS #2-2016	Date Received	3/9	2016 12:31					
Parameters	Result Units		R. L.	DF Prepared	Batch	Analyzed	Batch	Qual
pH, Electrometric Analysis	Analytical Method:	SM	4500-H+ B-00			Analyzed by:	MN	
pH	7.4 pH Unit	ts		1		03/10/16 10:39	BIO 16256	
Colouistian Adjusted CAD		0-				An also al la co		
Calculation, Adjusted SAR Adj. Sodium Adsorption Ratio	Analytical Method: 1.1 units	Ud	lculation	1		Analyzed by: 03/25/16 10:11	MFK	
Auj. Soulum Ausorption natio	1.1 units			I		03/23/10 10.11	UALO	
Calculation, Hardness	Analytical Method:	Ca	lculation			Analyzed by:	LM	
Hardness Calculation	230 mg/L		0.5	1		03/18/16 16:05	CALC	
Calculation, Total Anions	Analytical Method:	Ca	lculation			Analyzed by:	MYS	
Total Anions	6.1 meg/L	ou		1		03/10/16 07:49		
Calculation, Total Cations	Analytical Method:	Ca	lculation			Analyzed by:		
Total Cations	5.9 meq/L			1		03/18/16 16:05	CALC	
Metals by ICPMS, Collision Mode,	Prep Method:	EP	A 200.8	Prep by:	UKS			
Total	•							
	Analytical Method:	EP	A 200.8	-an east-powerstate-table states devices in the		Analyzed by:		
Calcium	39 mg/L		0.50	2 03/17/16 18:15		03/18/16 16:05		
Magnesium	31 mg/L		0.50	2 03/17/16 18:15		03/18/16 16:05		
Sodium	33 mg/L		1.0	2 03/17/16 18:15	MPR 14230	03/18/16 16:05	MMS 7953	
Metals by ICPMS, Collision Mode,	Prep Method:	EP	A 200.8 (filtrate)	Prep by:	UKS			
Diss								
	Analytical Method:	EP	A 200.8 (filtrate)			Analyzed by:	LM	
Arsenic	0.0026 mg/L		0.0020	4 03/15/16 00:00		03/16/16 18:57		
Boron Iron	ND mg/L		0.10	4 03/15/16 00:00		03/16/16 18:57		
Manganese	ND mg/L 0.19 mg/L		0.10 0.0050	4 03/15/16 00:00 4 03/15/16 00:00		03/16/16 18:57 03/16/16 18:57		
Silica (as SiO2)	88 mg/L		1.0	4 03/15/16 00:00		03/16/16 18:57		
Zinc	0.069 mg/L		0.020	4 03/15/16 00:00		03/16/16 18:57		
	0.000 mg/L		0.020	4 00/10/10 00:00	WII 11 14210	00,10,10,10,00	11110 7 0 40	
Turbidity Analysis	Analytical Method:	EP	A 180.1-93			Analyzed by:	BCP	
Turbidity	0.5 NTU		0.05	1		03/09/16 15:29	WET 8478	
Electrical Conductance Analysis	Analytical Method:	SM	2510 B-97			Analyzed by:	CLM	
Conductivity	560 umhos/		10	1		03/10/16 10:36		
Tetel Disselved Only 1 to 1	A	~	0540.0.00				5 45 F	
Total Dissolved Solids Analysis	Analytical Method:	SN	2540 C-97	-		Analyzed by:		
Total Dissolved Solids	380 mg/L		10	1		03/15/16 13:28	WGR 6046	
Anions by Ion Chromatography	Analytical Method:	EP	A 300.0			Analyzed by:	MYS	
Sulfate (as SO4)	6.2 mg/L		0.5	1		03/10/16 07:49	WIC 5281	
Chloride	6.9 mg/L		1	1		03/10/16 07:49	WIC 5281	
Nitrate, as NO3	ND mg/L		0.5	1		03/10/16 07:49		
Fluoride	ND mg/L		0.1	1		03/10/16 07:49	WIC 5281	
Alkalinity, Total by Standard Methods	Analytical Method:	SM	2320 B-97			Analyzed by:	CLM	
Alkalinity, Total (as CACO3)	287 mg/L	5.1	10	1		03/10/16 14:53		
Carbonate (as CO3)	ND mg/L		6	1		03/10/16 14:53		
-								
3/25/2016 12:16	KEPORI		T LABUHAIO	RY ANALYSIS			Page 4 c	of 13

#### REPORT OF LABORATORY ANALYSIS

Page 4 of 13



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ENVIRONMENTAL ANALYSES

### ANALYTICAL RESULTS

Lab Order: R030478 Project ID: FLORA SPRINGS #2-2016

Lab ID R030478001	Date Collected		/2016 11:45	Matr	ix Water			
Sample ID FLORA SPRINGS #2-2016	Date Received	3/9	/2016 12:31					
Parameters	Result Units		R. L.	DF Prepared	Batch	Analyzed	Batch	Qu
Hydroxide (as OH) Bicarbonate (as HCO3)	ND mg/L 350 mg/L		2 12	1 1		03/10/16 14:53 03/10/16 14:53		
					2			
			a.					
3/25/2016 12:16	REPORT		FLABORATO	RY ANALYSIS			Page 5	of 13



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ORIGINAL			TE OF CALIFC		DWR USE	E ONLY	DO NOT FILL	
File with D	WR		<b>APLETIC</b>					
Page 1 of 1		5	o Instruction 1		ST	ATE WELL NO	J STATION NO.	
Owner's W			<sup>No.</sup> e02	0739				
Date Work I	Began _	1/25/2016 , Ended 2/23/2016			LATITUDE		LONGITUDE	
Local Per	mit Ag	gency Napa County Environmental Mgr	nt			APN/TRS/		
Permit	No. <u>E1</u>	15-00755 Permit Date	11/20/2015				omen	
		GEOLOGIC LOG	,		WELL O	WNER —	28 ALW, 1	
ORIENTATIO	ON (⊻)	VERTICAL HORIZONTAL ANGLE						
DEPTH FF	ROM	METHOD ROTARY FLUID B	ENTONITE	Mailing Address 1	889 West Zinfar	ndel Lane	CA 94	574
SURFAC	E	DESCRIPTION Describe material, grain, size, color	eptc	St. Helena				
Ft. to		BROWN CLAY	, си.	Address 1978 We	t Zinfandel LO	CATION-		
12		SAND & GRAVEL		City St. Helena C		<u> </u>		
16		GRAY CLAY		City Ot. Helena Of County Napa	1			
30		SAND & GRAVEL			n 100	D 1 027		
60		TAN, RED SANDY ASH	a ang mangana sa kana ang mangana kana kana kana kana kana kana kan	APN Book 027				
115		GREEN VOLCANIC ROCK		Township	0	Section		and the second second
125		BLACK, RED & GREEN VOLCANICS		Latitude				EC.
220	and the second s	BROWN, TAN SANDY ASH			TION SKETCH-		ACTIVITY (	⊻) <u> </u>
285		HARD BLACK, GRAY VOLCANICS		-	NORTH			
310		BLACK, RED VOLCANICS		-	~		MODIFICATION/REP	AIR
320	410	HARD BLACK, GRAY VOLCANICS					Other (Sp	pecify)
410	420	RED VOLCANIC ROCK			120-			
420	470	HARD BLACK VOLCANICS	and a second second second second	WI	ELL-		DESTROY (De Procedures and Under "GEOLO	J Materials
470	475	BLACK, TAN VOLCANICS			In IN		PLANNED USI	
475	480	BLACK, RED VOLCANICS			155		WATER SUPPLY	
480	490	SOFT GRAY, TAN VOLCANICS		MEST .		EAST	✓ Domestic →	Public Industrial
490	550	HARD GRAY VOLCANICS		\$   W	INERY_5		MONITOR	
550	555	GRAY VOLCANICS WITH TAN ASH			Ľ	/	TEST W	
555	570	HARD GRAY VOLCANICS				/	CATHODIC PROTECT	FION
570	575	RED SANDY ASH			/	/	HEAT EXCHAI	
575		HARD BLACK, RED VOLCANICS			/		DIRECT P	
620		RED VOLCANIC ROCK					VAPOR EXTRACT	10N
640	700	GREEN, GRAY VOLCANIC ROCK		L				SING
		CONTINUED CASING LAYOUT		- Illustrate or Describe Dist	- SOUTH	Ruildings	REMEDIAT	10N
400		SCREEN PVC 8" .032 SLOT		Fences, Rivers, etc. and att necessary. PLEASE BE	ach a map. Use additiona	al paper if	OTHER (SPEC	;IFY)
480		BLANK PVC 8"		-				
500		SCREEN PVC 8" .032 SLOT			LEVEL & YIELD			1
600		BLANK PVC 8"		DEPTH TO FIRST WA		LOW SURFAC	E	1
620	and the second se	SCREEN PVC 8" .032 SLOT		DEPTH OF STATIC WATER LEVEL 158	(Ft.) & DATE		2/23/2016	
680	700	BLANK PVC 8"		ESTIMATED YIELD *				anna (Canadana) ann a
TOTAL DEI	PTH OF	BORING 700 (Feet)		TEST LENGTH 2				
		COMPLETED WELL 700 (Feet)			entative of a well's l			
		C + C + C + C + C + C + C + C + C + C +				T		
DEDT	u 1	CASING	r (S)			ANN	ILAR MATERIAL	6

DEPT		BORE -			_		C.	ASING	(S)			DEPT			ANNU	ILAR	MATERIAL
FROM SUF	RFACE	HOLE	Т	YPE	( /	)						FROM SUF	FACE			TY	PE
Ft. to	Ft.	DIA. (Inches)	BLANK	SCREEN	CON- DUCTOR	FILL PIP	MATERIAL / GRADE	INTERN DIAME (Inches	ER	GAUGE OR WALL THICKNESS	SLOT SIZE IF ANY (Inches)	Ft. to	Ft.	CE- MENT (⊥)	BEN- TONITE (⊻)	FILL (⊻)	FILTER PACK (TYPE/SIZE)
0	700	15										0	67	$\checkmark$			10 SK SAND
0	120		$\checkmark$	1			PVC F480		8	SDR-21		67	700			$\checkmark$	#6 SAND
120	240			$\checkmark$			PVC F480		8	SDR-21	.032						
240	280		$\checkmark$				PVC F480		8	SDR-21							
280	380			~			PVC F480		8	SDR-21	.032	1					
380	400		$\checkmark$	1			PVC F480		8	SDR-21							
	<ul> <li>Geologic</li> <li>Well Co</li> <li>Geophys</li> </ul>	Log Instruction D lical Log(s)		am			NAME HI	JCKFE SON, FIR	LD M, C	T WELL DRIL	mplete and accurat	RINTED)	my knowled			~ *	
1	- Other	er Chemical				STS.	- 2 <u>110 Per</u> ADDRESS Signed WEI			WHAN HI	M. MA	Na	CITY	2/29/1	16		94559 ZIP 439-746 C-57 LICENSE NUMBER
DWR 188 REV.	11-97			1	FAD	DDIT	IONAL SPACE IS	NEEDE	ED, I	USE NEXT CON	SECUTIVELY N	NUMBERED F	ORM				



A Tradition of Stewardship A Commitment to Service Planning, Building & Environmental Services

1195 Third Street, Suite 210 Napa CA 94559 www.countyofnapa.org (707) 253-4417

> David Morrison Director

# Well Permit

JO

**B**SET

			2 C	•	
Application Type:	Environmental / EM	Permits / Water Well	s / Class I	Applied Date:	9/18/2015
Permit Number:	E15-00755			Issued Date:	11/20/2015
Parcel Number:	027-100-037-000			Expiration Date	: 11/19/2017
Site Address:	1978 W Zinfandel L	n, St Helena			
Owner:	JMK-A LLC ETAL			Phone	: (000) 000-0000
Address:	ATTN JOHN KOME	S			
Applicant:	Don Huckfeldt			Phone	e: (707) 255-7923
Business Name:	HUCKFELDT WEL	L DRILLING INC		Licens	se #: 439746
Project Type:	Environmental / EM	l Permits / Water We	lls / Class I		
Proposed Use:					
Use:		Public	×	Name of Public Water System:	Komes Ranch
Well To Service T	his Parcel Only?:	Yes			
Water Supply:					
Septic Setbacks N	let?:	Yes		Well Located in Flood Zone?:	No
Actual Approved S	Setback:		×	Hazmat Site Within 1500 feet?:	No
Emergency Exem	otion Granted?:	No			
Reason For Emerg	gency Exemption:				
Specifications:					
Casing Diameter:		8.00 ln.		Method of Seal Placement:	Pump
Boring Diameter:		15.00 ln.		Minimum Seal Depth:	50.00 Ft.
Annular Seal:		3.00 In.		Material:	Concrete

#### TO PERMITEE:

Any work performed or operations conducted under the auspices of this permit constitutes acceptance of all conditions, inspections and comments contained in the this permit, and the incorporation of all requirements as set forth in the permit application.

Staff Signature: Date:

Napa County Code Chapter 16.04

# PERMIT No. ENF15-00119



A Tradition of Stewardship A Commitment to Service Planning, Building & Environmental Services

1195 Third Street, Suite 210 Napa, CA 94559 www.countyofnapa.org

> David Morrison Director

# NAPA COUNTY DEPARTMENT OF PLANNING, BUILDING & ENVIRONMENTAL SERVICES FLOODPLAIN MANAGEMENT PERMIT

Applicant Name: Huckfeldt Well Drilling Owner Name: JMK-A LLC		Phone: (707) 255-7923 Phone: (707) 963-1688
Poject Site Address: 1978 W. Zinfandel Avenu	е	APN: 027-100-037
Application Received By: <u>NG</u> Fee Paid: <u>\$171.87</u> Receiv	ot No.: 111139 Date:	Date: 11/16/2015
Project Located In: 🗹 Floodplain 🗌	Floodway 🛛 🗌 Riparian Zone	(Check all that apply)
Base Flood Elevation (BFE): Zone A	Community Map No.	06055C 0377E
Engineer's Findings and Comments: <i>This floc</i> 1. <i>The well casing shall be sealed at minimum</i> 2. <i>The well shall be capped with a water tight se</i>	' above grade and 25' below grade.	t 10 ette managemente de Constant et de Const
PERMIT EXPIRES	ONE YEAR FROM DATE BELC	DW
THIS PERMIT IS HEREBY GRANTED SUBJECT T THIS PERMIT IS HEREBY DENIED. Engineer's Signature: Mather A. Malan	O COMPLIANCE WITH CONDITIONS	Date: 11-17-15
I HEREBY CERTIFY THAT I HAVE READ, UND REQUIREMENTS AND CONDITIONS.	ERSTAND AND AGREE TO THE A	BOVE AND/OR ATTACHED
Owner Signature:	1	Date:
Applicant Signature:	Ø.	Date:
OFFICE USE ONLY	Final Inspection By:	Date:



11-Mar-16

Sean P. Garvey 1889 West Zinfandel Lane St. Helena, CA 94574

Att. Sean Garvey

R.E. Komes - Garvey Well Development & Pump Testing of Well #2 - 700' deep

Well #2 at Flora Springs was developed and a pump test @ 325 GPM was preformed.

The well was mechanically developed by airlift swabbing and the use of a 10' isolation tool to remove mud from the well screens, a total of 30 hours were required to clean 480 feet of screens. Aprox. 100,000 gallons were removed by airlift / swabbing.

Pumping development was done by a 50 hp pump set at 495 feet, the pump was surged turned off to let back-wash into screens, Aprox 315,000 Gallons were pumped during pump development.

The well was pumped at a constant rate of 325 GPM for 8 hours, the final draw down was 215 feet. The estimated draw down after 24 hours would be 275 feet. A water sample was taken to Cal Test.

Given the pumping data I would recommend the following:

- A. Set the permanent pump at 490'
- B. A 25 hp 200 gpm pump like a 2308-250-9 Grundfos would be a good choice for a permanent pump, curve included.
- C. Static (non pumping) water levels were lower every day after pumping, it may be necessary to monitor pumping levels during a full season of pumping and adjust pumping rates accordingly.

Please feel free to call me with any questions. 530-681-2012

Scott Smith

LGS Drilling, Inc.



а	Date:3-9-16				Job No: Flora Springs #2
1	WELL ID: 201		Remarks:		Sheet 1 of 1
	VVELL ID. 201	10-2	Well Depth		Observers
	GPS:		Pump Set	495	
	0/ 0.	and the second secon		50 hp / 325 g	
			It dilip th	TYPE OF TE	ST
				ate @ 325 gpi	
	Time	Elapsed		Depth below	Remarks
	of Day	Time	water from	static level.	
		min. sec.		(ft)	T=27,774,800
9-Mar	6:30		173.3	0	325 GPM
	6:35		191.9		
	6:45		193.7		
	7:00		194.6		
	7:30		195.6		
	8:30		195.8		325 GPM
	9:30 10:30		197.6 199.8		
	11:30		203.3		Sample Taken 80*
	12:30		207.2		Gample Taken oo
	13:30		211.2		325 GPM
	14:30		215.4		T=27,930,800
					Land Land Land Land Land Land Land Land
recovery	14:40		197.8		
-	15:00		194.5		
3/11/16			168.3		
3/14/16	9:00		160.5		Static on 2-29-16 before pumping 158.0
			44		
			++		
			+		U
E					
				-	
					E.
			<u> </u>		
			<u> </u>		
			+		
			++		
			+		
1		LL	l		

# PERFORMANCE CURVES

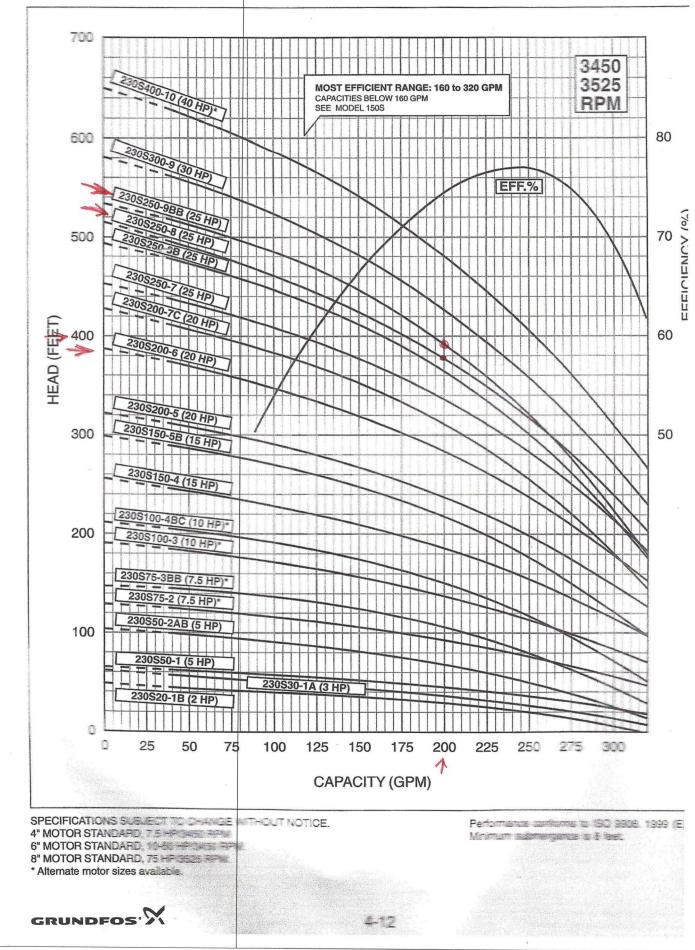
# 230 GPM

# MODEL 2

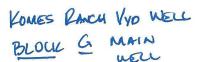


**OUTLET SIZE: 3" NPT** 

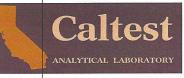
### NOMINAL D



### NELAP/ORELAP Certification 4036



Lab Order: R030478 Project ID: FLORA SPRINGS #2-2016



#### ENVIRONMENTAL ANALYSES

#### ANALYTICAL RESULTS

							n kala shekara ka asala na anga dan sebaga ya kananga a sa Mana ya kananga na kananga ka kananga k	
Lab ID R030478001	Date Collected	3/9	2016 11:45	Matrix	Water			
Sample ID FLORA SPRINGS #2-2016	Date Received	3/9	2016 12:31					
Parameters	Result Units		R. L.	DF Prepared	Batch	Analyzed	Batch	Qual
pH, Electrometric Analysis	Analytical Method:	SM	4500-H+ B-00			Analyzed by:	MN	
pH	7.4 pH Unit	ts		1		03/10/16 10:39	BIO 16256	
Colouistian Adjusted CAD		0-				An also al la co		
Calculation, Adjusted SAR Adj. Sodium Adsorption Ratio	Analytical Method: 1.1 units	Ud	lculation	1		Analyzed by: 03/25/16 10:11	MFK	
Auj. Soulum Ausorption natio	1.1 units			I		03/23/10 10.11	UALO	
Calculation, Hardness	Analytical Method:	Ca	lculation			Analyzed by:	LM	
Hardness Calculation	230 mg/L		0.5	1		03/18/16 16:05	CALC	
Calculation, Total Anions	Analytical Method:	Ca	lculation			Analyzed by:	MYS	
Total Anions	6.1 meg/L	ou		1		03/10/16 07:49		
Calculation, Total Cations	Analytical Method:	Ca	lculation			Analyzed by:		
Total Cations	5.9 meq/L			1		03/18/16 16:05	CALC	
Metals by ICPMS, Collision Mode,	Prep Method:	EP	A 200.8	Prep by:	UKS			
Total	•							
	Analytical Method:	EP	A 200.8	-an east-powerstate-tate states strates is like		Analyzed by:		
Calcium	39 mg/L		0.50	2 03/17/16 18:15		03/18/16 16:05		
Magnesium	31 mg/L		0.50	2 03/17/16 18:15		03/18/16 16:05		
Sodium	33 mg/L		1.0	2 03/17/16 18:15	MPR 14230	03/18/16 16:05	MMS 7953	
Metals by ICPMS, Collision Mode,	Prep Method:	EP	A 200.8 (filtrate)	Prep by:	UKS			
Diss								
	Analytical Method:	EP	A 200.8 (filtrate)			Analyzed by:	LM	
Arsenic	0.0026 mg/L		0.0020	4 03/15/16 00:00		03/16/16 18:57		
Boron Iron	ND mg/L		0.10	4 03/15/16 00:00		03/16/16 18:57		
Manganese	ND mg/L 0.19 mg/L		0.10 0.0050	4 03/15/16 00:00 4 03/15/16 00:00		03/16/16 18:57 03/16/16 18:57		
Silica (as SiO2)	88 mg/L		1.0	4 03/15/16 00:00		03/16/16 18:57		
Zinc	0.069 mg/L		0.020	4 03/15/16 00:00		03/16/16 18:57		
	0.000 mg/L		0.020	4 00/10/10 00:00	WII 11 14210	00,10,10,10,00	11110 7 0 40	
Turbidity Analysis	Analytical Method:	EP	A 180.1-93			Analyzed by:	BCP	
Turbidity	0.5 NTU		0.05	1		03/09/16 15:29	WET 8478	
Electrical Conductance Analysis	Analytical Method:	SM	2510 B-97			Analyzed by:	CLM	
Conductivity	560 umhos/		10	1		03/10/16 10:36		
Tetel Disselved Only 1 to 1	A	~	0540.0.00				5 45 F	
Total Dissolved Solids Analysis	Analytical Method:	SN	2540 C-97	-		Analyzed by:		
Total Dissolved Solids	380 mg/L		10	1		03/15/16 13:28	WGR 6046	
Anions by Ion Chromatography	Analytical Method:	EP	A 300.0			Analyzed by:	MYS	
Sulfate (as SO4)	6.2 mg/L		0.5	1		03/10/16 07:49	WIC 5281	
Chloride	6.9 mg/L		1	1		03/10/16 07:49	WIC 5281	
Nitrate, as NO3	ND mg/L		0.5	1		03/10/16 07:49		
Fluoride	ND mg/L		0.1	1		03/10/16 07:49	WIC 5281	
Alkalinity, Total by Standard Methods	Analytical Method:	SM	2320 B-97			Analyzed by:	CLM	
Alkalinity, Total (as CACO3)	287 mg/L	5.1	10	1		03/10/16 14:53		
Carbonate (as CO3)	ND mg/L		6	1		03/10/16 14:53		
-								
3/25/2016 12:16	KEPORI		T LABUHAIO	RY ANALYSIS			Page 4 c	of 13

#### REPORT OF LABORATORY ANALYSIS

Page 4 of 13



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ENVIRONMENTAL ANALYSES

### ANALYTICAL RESULTS

Lab Order: R030478 Project ID: FLORA SPRINGS #2-2016

Lab ID R030478001	Date Collected		/2016 11:45	Matr	ix Water			
Sample ID FLORA SPRINGS #2-2016	Date Received	3/9	/2016 12:31					
Parameters	Result Units		R. L.	DF Prepared	Batch	Analyzed	Batch	Qu
Hydroxide (as OH) Bicarbonate (as HCO3)	ND mg/L 350 mg/L		2 12	1 1		03/10/16 14:53 03/10/16 14:53		
					2			
			a.					
3/25/2016 12:16	REPORT		FLABORATO	RY ANALYSIS			Page 5	of 13



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9-Jan-16

Sean P. Garvey 1889 West Zinfandel Lane St. Helena, CA 94574

Att. Sean Garvey

R.E. Komes - Garvey Well Development & Pump Testing

The well at Flora Springs was developed and a pump test @ 75 GPM was preformed.

The well was mechanically developed by airlift swabbing and the use of a 10' isolation tool to remove mud from the well screens, a total of 28 hours were required to clean 420 feet of screens. Aprox. 100,000 gallons were removed by airlift / swabbing.

Pumping development was done by a 30 hp pump set at 465 feet, the pump was surged turned off to let back-wash into screens. Aprox 112,000 Gallons were pumped during pump development.

The well was pumped at a constant rate of 75 GPM for 8 hours, the final draw down was 409 feet. The estimated draw down after 24 hours would be 425 feet. A water sample was taken to Cal Test.

Given the pumping data I would recommend the following:

- A. Set the permenter pump at 560'
- B. A 10 hp 50 gpm pump like a FPS F6P50x20 would be a good choice for a permanent pump, curve included.
- C. Static (non pumping) water levels were lower every day after pumping, it may be necessary to monitor pumping levels during a full season of pumping and adjust pumping rates accordingly.

Please feel free to call me with any questions. 530-681-2012

Scott Smith

LGS Drilling, Inc.

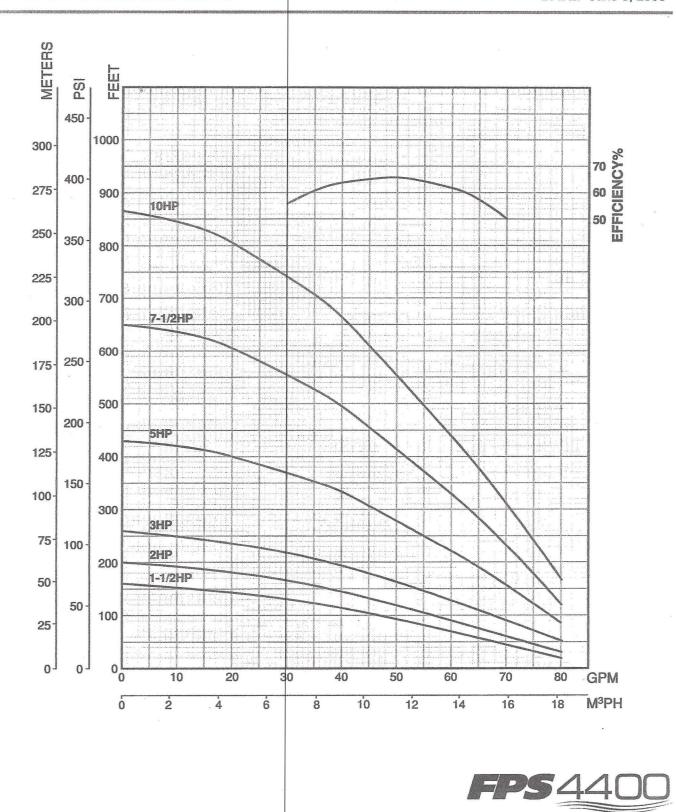


	Date:1-7-16							Job No:	Flora Spi	rings /	Komes	<u>s - G</u> arve
	WELL ID: 2015-A Remarks: W					ell Depth:	616	Sheet	1	of	1	
	WELL ID. 20			l'indirito.		mp Intake:		Observers				
	GPS:					mp;	30 hp					
				1		ising:	8" PVC					
						PE OF TE					olandi na Sifusikan di	
				Developme	ent 8	& Test Pum	ping					
	Time	Elapse	d	Depth to		pth below			Remarks			
	of Day	Time		water from	sta	tic level.						
		min.	sec.	R.P. (ft)	(ft)							
4-Jan	13:00			93.00		0.00		Water Leve			ng	
									2,535,400			
								Develop Pu			rty	
5-Jan	and the second se			94.70					2,541,100			
	13:00							Develop Pu			rty	
<b>.</b> .	17:30			400 70					bid at Surg			
6-Jan		-		102.70					2,579,850			
	17:00				$\vdash$			Devel	lop Pumpi	ng		
7 1	40.40			100.00	$\vdash$			т,	0.044.040			
7-Jan	10:10 10:15			106.00 146.80					2,611,940 PM 8 hr T		and the second	
	10:15			177.50				75 G		est		
	10:20			228.50				CARGO CONTRACTOR OF				
	10:30			258.40								
	11:00			298.00								
	11:40			314.65			100000 (0.000 (0.000))		1			
	12:10			318.35			V	Vater Samp	le Taken	- Cal-T	est	
	13:10			333.10								
	14:10			365.25								
	15:10			405.20								
	16:10			406.60								
	17:10			407.90					an a			
	18:10			408.40				T=2,647	7,940 75	GPM		
recovery	18:15			238.40								
	18:20			206.80					Served Control Served Serve			
<u> </u>	18:25			126.40				ti da stali a stali a da stali a stali				
8-Jan	9:30			110.60								
	13:00			109.50						****	an a	
					$\vdash$			water and the second second second				
			eleven y me an areas an				and the second					
					$\vdash$			1919-1919-1919-1919-1919-1919-1919-191				
										and the second secon		
						1	ander of the second					
							********					
		I				l			an a san an an a san an an a san a			

# **Submersible Pumps**

## **6" High Capacity** 50 GPM Performance Curve

PAGE: SP-105 DATE: June 5, 2006



## **Submersible Pumps**

# **6" High Capacity** 50 GPM Performance Chart

### **Capacities in U.S. Gallons per Minute**

							NED	тнт	0 PU	MDIN	G MI	TED	1 E\/E			- 1NI I	delett.						
HP	PSI					SH			EASI									ICE					
		40	60	80	100	120	140	160	180	200	250	300	350	400	450	500	550	600	650	700	750	800	
	0	73	65	57	48	39	26	T										partonega anda					1
	20	54	46	36	20																1		Shut-off 158 ft.
1-1/2	30	45	34	18																			140
	40	32	13																				14
	50																						ц В
· · ·	0	75	69	63	57	50	43	34	23			1											
	20	62	55	48	41	32	18		1														8 11
	30	54	47	39	30	15			-										d.				119
2	40	46	38	28																			Shut-off 198 ft.
	50	37	26																				shu
	60	24																					G
	0	-	78	73	68	63	58	52	46	40	13	1			1						1		
	20	71	66	61	56	50	44	37	29	16													10
	30	66	61	55	49	43	36	27	14			1		1									26
3	40	60	54	48	42	35	25																fo
	50	53	47	41	34	23																	Shut-off 260 ft.
	60	46	40	32	22				-														07
	0	-	0	0	78	75	72	69	66	63	55	46	36	21									åt.
	20	-	-	74	71	68	65	62	59	56	47	37	23										434
5	40	73	70	67	64	61	58	54	51	47	48	24											off
	50	70	67	64	61	57	54	51	47	43	32												Shut-off 434 ft.
	60	66	65	61	57	54	50	47	43	39	25												ŝ
	0	-	-	-	-	-	79	77	75	73	68	63	58	52	46	40	31	21					
	20	-	-	-	-	-	74	72	70	68	63	58	53	47	40	33	22						Shut-off 650 ft.
7-1/2	30	-	-	-	-	74	72	70	68	66	61	56	50	44	37	28							11 61
1-1/2	40	-	-	-	74	72	70	68	66	64	59	53	47	41	33	23							10-1
	50	-	-	73	71	69	68	66	64	62	56	51	45	38	29	16							Shu
	60	-	74	72	70	68	65	63	61	59	54	48	41	34	24								
FGP50x20	0	-	-	-	-	-	-	-	-	78	74	70	67	63	59	55	51	46	41	36	30	21	
101JACO	20	-	-	-	-	-	-	-	-	74	71	67	63	59	55	51	47	42	36	30	22	8	Shut-off 865 ft.
40	30	-	-	-	-	-	-		74	73	69	65	61	57	53	49	44	39	34	27	17		11 86
10	40	-	-	-	-	-	-	74	72	71	67	63	59	55	51	47	42	37	30	22			1-01
	50	-	-	~	-	75	73	72	70	69	65	61	57	53	49	45	40	34	27	18			Shu
	60	-	-	-	-	74	72	71	69	67	63	59	55	51	47	43	37	31	12				

Discharge tapping 3" FNPT.

Notes: 1. Performance shown does not include friction loss in the drop pipe.

2. All performance data is based on rated motor nameplate voltage.



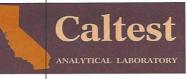
### NELAP/ORELAP Certification 4036



Lab Order: R010299 Project ID: FLORA SPRINGS 2015A

R010299001

Lab ID



#### ENVIRONMENTAL ANALYSES

#### ANALYTICAL RESULTS

Matrix

Water

1/7/2016 13:00

Date Collected

Lab ID R010299001	Date Collected	1/7	2016 13:00	IVIALITX	water			
Sample ID FLORA SPRINGS 2015A	Date Received	1/7	/2016 13:47					
Describert	Desult Links				Datab	Analyzad	Datab	Oud
Parameters	Result Units		R. L.	DF Prepared	Batch	Analyzed	Batch	Qual
pH, Electrometric Analysis	Analytical Method:	SM	4500-H+ B-00			Analyzed by:	CCZ	
pH	6.9 pH Uni	its		1		01/16/16 13:49	BIO 16060	
Calculation, Adjusted SAR	Analytical Method:	Ca	culation			Analyzed by:	MFK	
Adj. Sodium Adsorption Ratio	1.1 units			1		01/24/16 21:03	CALC	
Onlawlation Handrage	Amelatical Mathead	0.	loulation			Analyzed by	L N/L	
Calculation, Hardness	Analytical Method:	Ua	culation			Analyzed by:		
Hardness Calculation	130 mg/L		0.5	1		01/14/16 23:36	CALC	
Calculation, Total Anions	Analytical Method:	Ca	culation			Analyzed by:	CLM	
Total Anions	3.7 meg/L			1		01/18/16 15:29		
Total / mons	0.7 mog/L					01/10/10 10.20	0/120	
Calculation, Total Cations	Analytical Method:	Ca	culation			Analyzed by:	LM	
Total Cations	3.9 meg/L			1		01/14/16 23:36	CALC	
Metals by ICPMS, Collision Mode,	Prep Method:	EP	A 200.8	Prep by:	UK			
Total	Amphalact		000 0			Analyzed br	1.5.4	
Outrien	Analytical Method:	EP	A 200.8	40.04/44/40.00.00	MDD 44050	Analyzed by:		
Calcium	33 mg/L		0.50	10 01/11/16 00:00	MPR 14058	01/14/16 23:36		
Magnesium	12 mg/L		0.50	10 01/11/16 00:00	MPR 14058	01/14/16 23:36		
Sodium	28 mg/L		1.0	10 01/11/16 00:00	MPR 14058	01/14/16 23:36	MMS 7868	
Metals by ICPMS, Collision Mode,	Prep Method:	FP	A 200.8 (filtrate)	Prep by:	UK			
Diss	Fiep Method.			Fieb by.	UK			
	Analytical Method:	EP	A 200.8 (filtrate)			Analyzed by:	LM	
Arsenic	ND mg/L		0.0020	1 01/13/16 00:00	MPR 14063	01/14/16 21:37	MMS 7871	
Boron	ND mg/L		0.10	1 01/13/16 00:00		01/14/16 21:37		
Iron	ND mg/L		0.050	1 01/13/16 00:00		01/14/16 21:37		
Manganese	0.096 mg/L		0.0050	1 01/13/16 00:00		01/14/16 21:37		
Silica (as SiO2)	74 mg/L		1.0	2 01/13/16 00:00		01/18/16 12:58		
Zinc	0.84 mg/L		0.020	4 01/13/16 00:00		01/18/16 12:52		
Zinc	0.64 mg/L		0.020	4 01/13/10 00.00	MFN 14003	01/10/10 12.52	101013 707 1	
Turbidity Analysis	Analytical Method:	EP	A 180.1-93			Analyzed by:	BCP	
Turbidity	5.1 NTU		0.05	1		01/08/16 12:22		
Electrical Conductance Analysis	Analytical Method:	SM	2510 B-97			Analyzed by:	CLM	
Conductivity	400 umhos	/cm	10	1		01/18/16 11:09	WET 8409	
Total Dissolved Collida Avaluate	Analytical Matter 1	01	0540.0.07			Analyzed	MANI	
Total Dissolved Solids Analysis	Analytical Method:	SI	2540 C-97			Analyzed by:		
Total Dissolved Solids	310 mg/L		10	1		01/12/16 15:32	WGR 5982	
Anions by Ion Chromatography	Analytical Method:	FP	A 300.0			Analyzed by:	MYS	
Nitrate, as NO3	26 mg/L		0.5	1		01/08/16 15:44		
Fluoride	ND mg/L		0.1	1		01/08/16 15:44		
Sulfate (as SO4)	23 mg/L		0.5	1		01/08/16 15:44		
Chloride			10			01/08/16 15:44		
Onionue	19 mg/L		10	10		01/00/10 18:02	WIC 3221	
Alkalinity, Total by Standard Methods	Analytical Method:	SM	2320 B-97			Analyzed by:	CLM	
Alkalinity, Total (as CACO3)	115 mg/L	2.1	10	1		01/18/16 15:29		
Bicarbonate (as HCO3)	140 mg/L		12	1		01/18/16 15:29		
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1/25/2016 05:09

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### NELAP/ORELAP Certification 4036



ENVIRONMENTAL ANALYSES

### ANALYTICAL RESULTS

Lab Order: R010299 Project ID: FLORA SPRINGS 2015A

FIDELID. FLORA SFRINGS 2013A		27					
Lab ID R010299001 Sample ID FLORA SPRINGS 2015A	Date Collected Date Received	/2016 13:00 /2016 13:47	Matr	ix Water			
Parameters	Result Units	R. L.	DF Prepared	Batch	Analyzed	Batch	Qua
Carbonate (as CO3) Hydroxide (as OH)	ND mg/L ND mg/L	6 2	1 1		01/18/16 15:29 01/18/16 15:29		

1/25/2016 05:09



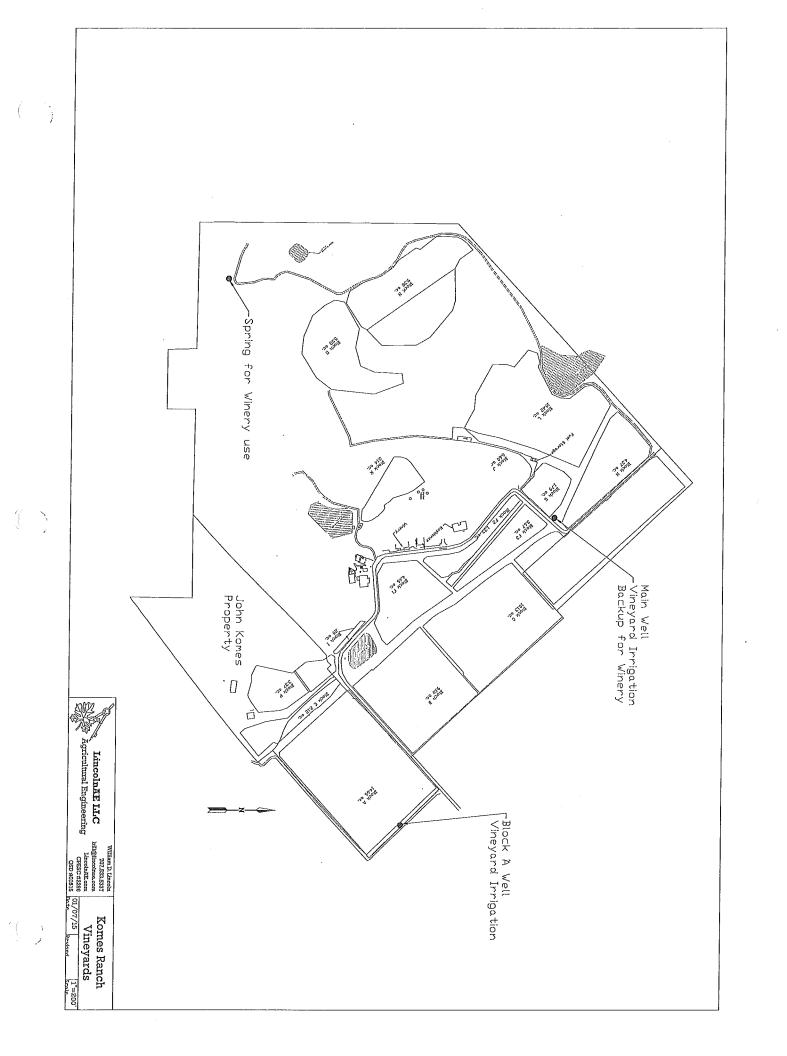
Page 5 of 13

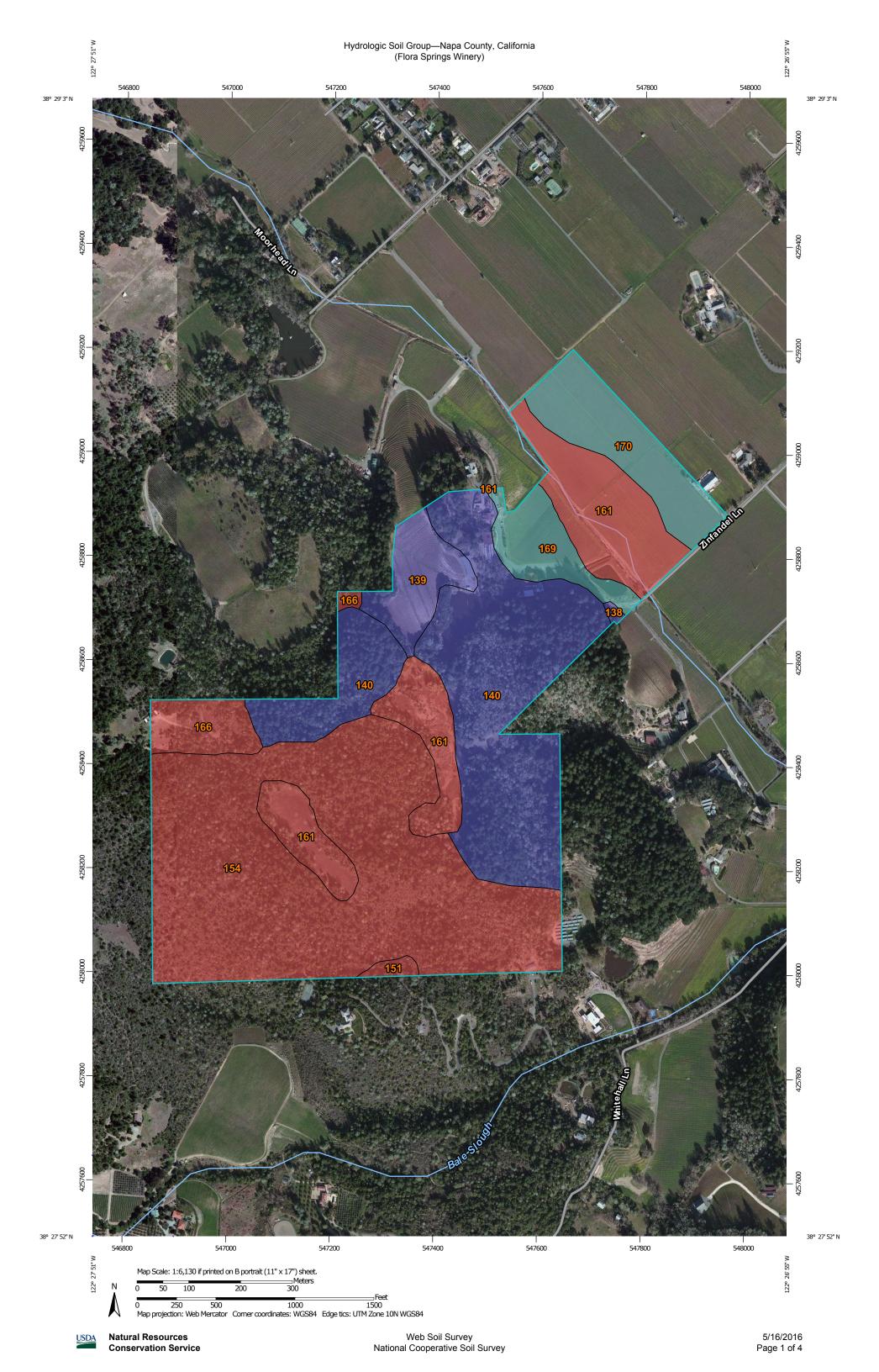


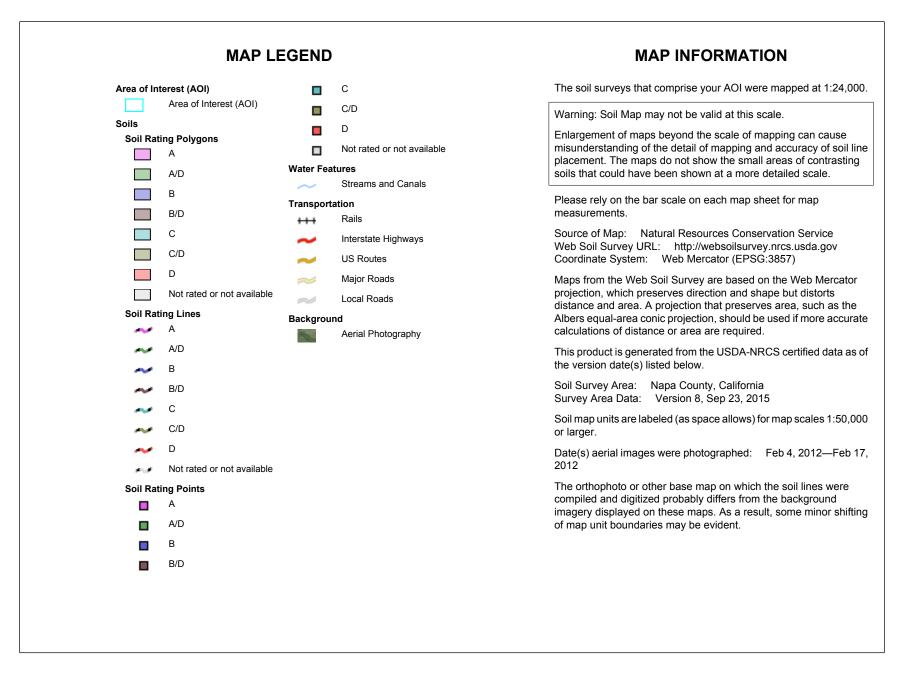
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# Hydrologic Soil Group

Hydrologic Soil Group— Summary by Map Unit — Napa County, California (CA055)								
Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI				
138	Forward gravelly loam, 2 to 9 percent slopes	В	0.3	0.1%				
139	Forward gravelly loam, 9 to 30 percent slopes	В	7.0	4.2%				
140	Forward gravelly loam, 30 to 75 percent slopes	В	44.7	26.5%				
151	Hambright-Rock outcrop complex, 2 to 30 percent slopes	D	0.8	0.5%				
154	Henneke gravelly loam, 30 to 75 percent slopes	D	67.5	40.0%				
161	Maxwell clay, 2 to 9 percent slopes	D	24.4	14.5%				
166	Montara clay loam, 5 to 30 percent slopes	D	5.5	3.3%				
169	Perkins gravelly loam, 5 to 9 percent slopes	С	6.7	4.0%				
170	Pleasanton loam, 0 to 2 percent slopes	С	11.8	7.0%				
Totals for Area of Inte	rest	168.7	100.0%					

## Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

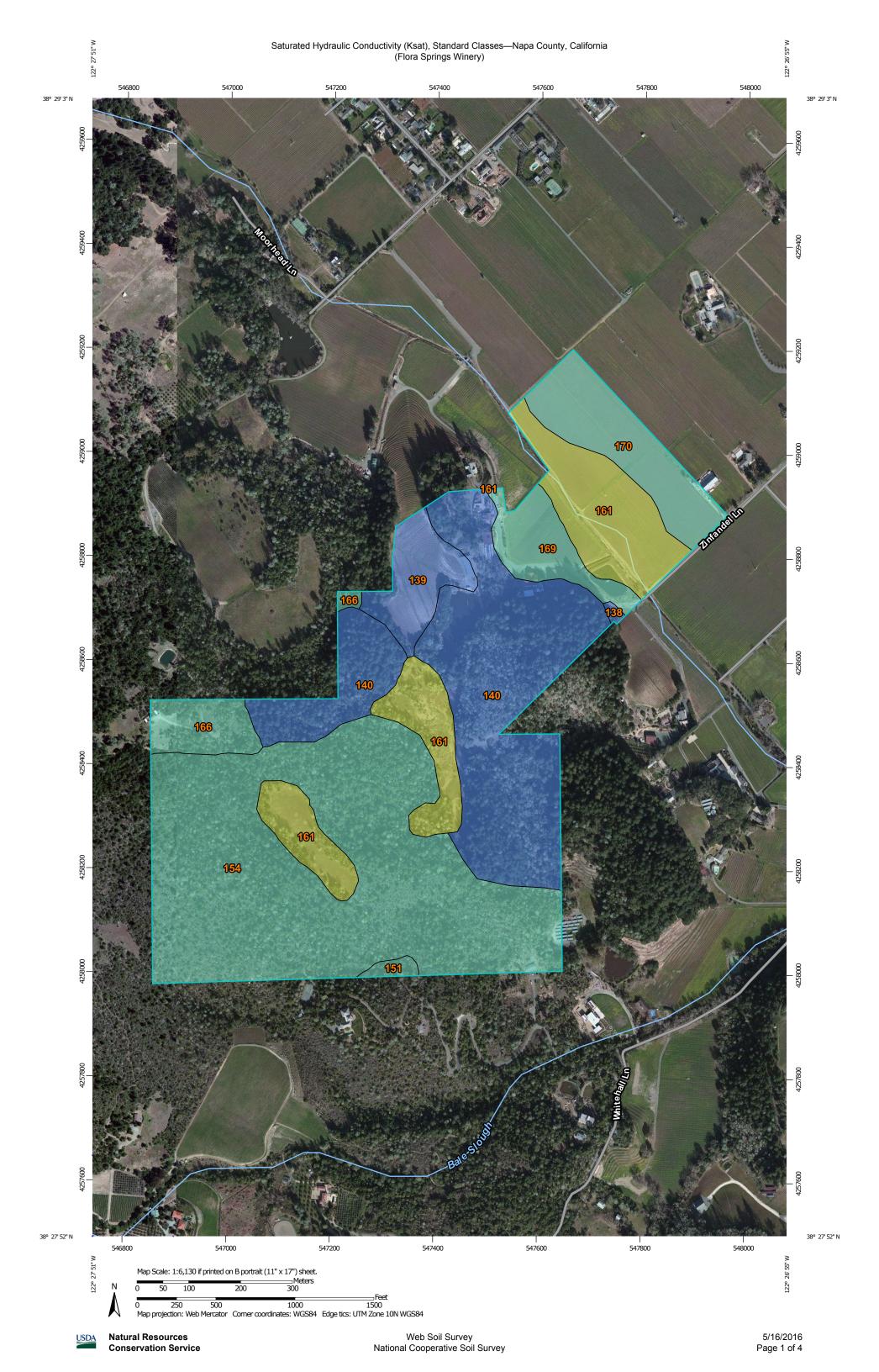
Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

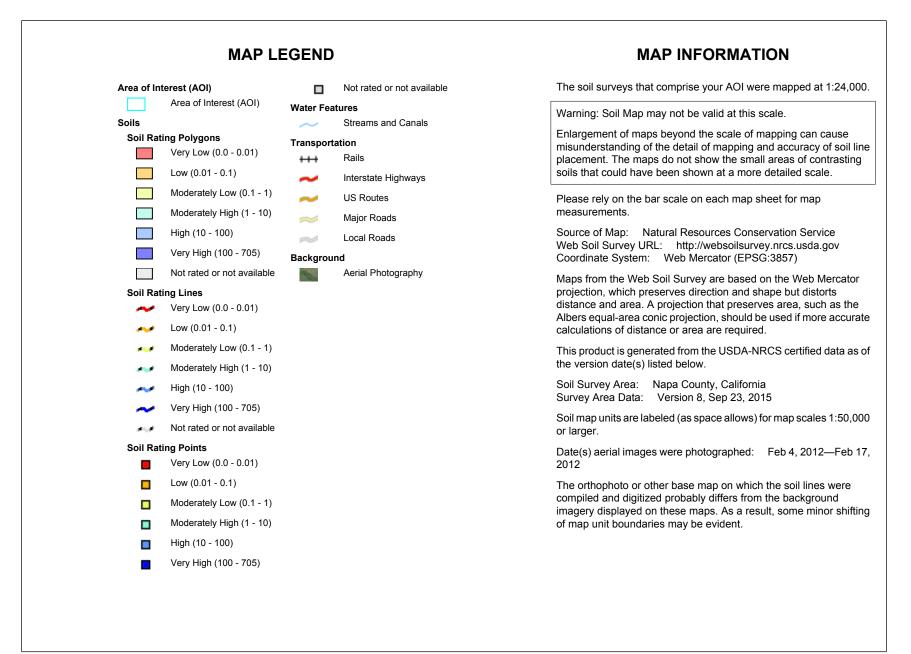
Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

## **Rating Options**

Aggregation Method: Dominant Condition Component Percent Cutoff: None Specified Tie-break Rule: Higher





# Saturated Hydraulic Conductivity (Ksat), Standard Classes

Saturated Hydraulic Conductivity (Ksat), Standard Classes— Summary by Map Unit — Napa County, California (CA055)							
Map unit symbol	Map unit name	Rating (micrometers per second)	Acres in AOI	Percent of AOI			
138	Forward gravelly loam, 2 to 9 percent slopes	28.0000	0.3	0.1%			
139	Forward gravelly loam, 9 to 30 percent slopes	28.0000	7.0	4.2%			
140	Forward gravelly loam, 30 to 75 percent slopes	28.0000	44.7	26.5%			
151	Hambright-Rock outcrop complex, 2 to 30 percent slopes	9.0000	0.8	0.5%			
154	Henneke gravelly loam, 30 to 75 percent slopes	9.0000	67.5	40.0%			
161	Maxwell clay, 2 to 9 percent slopes	0.2150	24.4	14.5%			
166	Montara clay loam, 5 to 30 percent slopes	2.7000	5.5	3.3%			
169	Perkins gravelly loam, 5 to 9 percent slopes	9.0000	6.7	4.0%			
170	Pleasanton loam, 0 to 2 percent slopes	9.0000	11.8	7.0%			
Totals for Area of Inte	rest		168.7	100.0%			

## Description

Saturated hydraulic conductivity (Ksat) refers to the ease with which pores in a saturated soil transmit water. The estimates are expressed in terms of micrometers per second. They are based on soil characteristics observed in the field, particularly structure, porosity, and texture. Saturated hydraulic conductivity is considered in the design of soil drainage systems and septic tank absorption fields.

For each soil layer, this attribute is actually recorded as three separate values in the database. A low value and a high value indicate the range of this attribute for the soil component. A "representative" value indicates the expected value of this attribute for the component. For this soil property, only the representative value is used.

The numeric Ksat values have been grouped according to standard Ksat class limits. The classes are:

Very low: 0.00 to 0.01 Low: 0.01 to 0.1 Moderately low: 0.1 to 1.0 Moderately high: 1 to 10 High: 10 to 100 Very high: 100 to 705

### **Rating Options**

Units of Measure: micrometers per second Aggregation Method: Dominant Component Component Percent Cutoff: None Specified Tie-break Rule: Fastest Interpret Nulls as Zero: No Layer Options (Horizon Aggregation Method): Surface Layer (Not applicable)