12505.0 Vintage Wine Estates Girard Winery Use Permit Wastewater Feasibility Study September 9, 2015



Napa County Planning, Building, and Environmental Services (PBES) Attn: Kim Withrow 1195 3rd St., Room 201 Napa, Ca 94559

Project: Girard Winery Use Permit

1077 Dunaweal Ln. Calistoga, CA 94515 APN: 020-150-017

Copies Document Date Description

1 9/9/2015 Wastewater Feasibility Study and Attachments

Kim,

This letter and attached Wastewater Feasibility Study are provided in support of the sanitary sewage and winery process wastewater treatment and dispersal components of the Girard Winery Use Permit.

Winery process wastewater will be treated in two existing winery process wastewater ponds on the project parcel which currently treat the winery process wastewater from Clos Pegase Winery. Addition of the Girard winery process wastewater will include a pump station at Girard, connection into the existing forcemain to the rotary screen at the ponds, and addition of more aeration at the existing ponds. Treated effluent from the ponds is then discharged into an existing irrigation reservoir used for irrigation of vineyard and landscaping on the Close Pegase Winery and Girard Winery parcels. The existing ponds are sufficient in volume to provide greater than 100 days retention at the proposed process wastewater flows from both wineries combined. Specifics on aeration sizing, pond water balance, and irrigation reuse calculations are included in the attached study.

It is proposed to disperse of sanitary sewage from the proposed Girard Winery using a subsurface drip irrigation septic system and associated pretreatment system. The pretreatment system proposed shall be an AdvanTex Textile Filter or BioBarrier MBR system consisting of all below grade tanks which include a septic tank, recirculation tank (for AdvanTex only), a treatment tank (for BioBarrier only), and subsurface drip irrigation sump pump tank. The BioBarrier would also include use of a blower and effluent pump above grade and the AdvanTex would include an above grade AX100 Textile filter model. Specifics on sizing of the system components and subsurface drip irrigation sizing, site, and soil criteria are provided in the attached report.

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We trust that this letter and attached report are sufficient for review and to generate conditions of approval for the project which are satisfactory to the County. If you have any questions or comments with regards to this project, please feel free to contact me.

Sincerely,

Ben Monroe, P.E. Project Manager

Always Engineering, Inc.

Enclosures



Girard Winery

1077 Dunaweal Ln., Calistoga, CA 94515 APN: 020-150-017

USE PERMIT WASTEWATER FEASIBILITY STUDY



Project and Site Background

Vintage Wine Estates owns and operates the existing "Clos Pegase" Winery located at 1060 Dunaweal Ln in Calistoga, Ca (APN: 020-150-012). Vintage Wine Estates also owns the parcel across Dunaweal Ln., (1077 Dunaweal Ln., APN: 020-150-017), which has the existing process wastewater ponds and water well for Clos Pegase.

Vintage Wine Estates is proposing to construct a new winery and tasting room (the Girard Winery) on the above referenced parcel. A production capacity of 200,000 gal of wine annually is proposed for the new Girard Winery. With the Use Permit, it is proposed to also treat the process waste (PW) generated by Girard Winery using the existing Clos Pegase Pond Treatment system. A new collection system and transfer pump sump will be required for Girard Winery. A new aerator in the process waste ponds will also be required. A new sanitary sewage system on-site septic system is proposed to accommodate the winery employees, visitors, and events.

The parcel consists of existing vineyards, water supply well and treatment, an agricultural storage building, 2 PW treatment ponds and an irrigation storage pond. The parcel is generally flat, with a small flow line along the southern property line.

A site plan is provided in Enclosure B displaying the existing site and proposed wastewater system improvements.

SANITARY SEWAGE (SS)

Existing Site Evaluation

A site evaluation was performed by Ben Monroe, P.E. of Always Engineering and Peter Ex of Napa County on November 14, 2013. A total of 16 soil profiles were evaluated and 6 were logged for use. Test pits displayed a sandy clay loam surface soil which ranged in depth from 36" to 56" in depth. Soils were underlain by a sandy loam or loamy sand for a total permeable depth ranging from 49" to 60" in depth. All soil displayed a moderate to strong sub-angular blocky structure. Faint mottling was observed at 24" deep, with increasing intensity with depth below that. Prominent mottling was observed below 48" in all test pits. Additional groundwater monitoring



was required onsite to determine if the upper mottling is due to seasonal subsurface groundwater or heavy irrigation of the onsite vineyards.

Groundwater monitoring was performed onsite on February 9, February 10, and February 19, 2015 following receipt of 5.12 inches of rainfall on February 6 through February 9, 2015, as measured at the Napa County Rain Gauge at Dunaweal Lane and the Napa River. Approximately 1.62 inches of rain occurred on February 8 and the morning of February 9. This is far greater than the minimum 0.5 inches within a 48 hours which is required for groundwater monitoring which is required by Napa County Site Evaluation procedures. Groundwater readings on February 9, 2015 indicated a minimum of 24 inches to perched groundwater in all monitoring wells except for well #5, which is the lowest in elevation and will require a setback during design. Readings the following day indicated that groundwater elevations dropped by a minimum of 6 inches and had fallen an additional 37 inches minimum by February 19, 2015. All monitoring wells, except for #5 were dry on February 19. The monitoring revealed greater separation from groundwater in the northwestern area of testing and therefore the proposed primary septic system will be focused in this area. This monitoring, performed following substantial rains in a short period of time, and measured immediately following the cease of rain, is considered to represent a reasonably worst case scenario with respect to perched groundwater.

An interceptor drain is also proposed to ensure maximum separation to seasonal groundwater in the vicinity of septic dispersal. Surface drainage improvements for the winery will also be designed to increase diversion of surface water runoff away from the septic area and areas uphill of the dispersal system. The Napa County Site Evaluation procedures and table for Alternative Sewage Treatment System Soil Application Rates indicate a Sandy clay loam or sandy loam with moderate structure should be loaded at 0.75 to 1.0 gpd using pretreated effluent. A copy of the site evaluation and groundwater monitoring reports is included as an attachment to this report.

Proposed Wastewater Flows

The proposed onsite sanitary wastewater flow rate is entirely associated with the proposed Girard Winery. The use permit is requesting a similar level of use as Clos Pegase; an average number of 10 employees (15 gpcd) along with 75 visitors (3gpcd), and a peak number of 30 employees (15 gpcd) along with 100 visitors (3 gpcd). There will be one large event per year which will have 500 attendees. Portable toilets will be used for this event. All events will have fully catered food with all preparation and cleanup occurring off site. The proposed wastewater flows are estimated as follows:

Average

Employees

8	FT employees	X	15 gpd/employee	=	120 gpd
3	PT employees	X	7.5 gpd/employee	=	22.5 gpd

13530.0 Vintage Wine Estates_Girard Winery Wastewater Feasibility Study February 20, 2014

Revised: September 9, 2015



Tasting Room

42 tasting visitors x = 3 gpd/visitor = 126 gpd

Events

75 event visitors x 5 gpd/visitor = 375 gpd

TOTAL PROPOSED AVERAGE DESIGN FLOW = 643.5 GPD

Peak

Employees

20 FT employees x 15 gpd/employee = 300 gpd 10 PT employees x 7.5 gpd/employee = 75 gpd

Tasting Room

100 tasting visitors x = 300 gpd

Events

200 event visitors x $\frac{5 \text{ gpd}}{\text{visitor}}$ = $\frac{1,000 \text{ gpd}}{\text{cm}}$

TOTAL PROPOSED PEAK DESIGN FLOW

Proposed Sanitary Sewage Loading

It is proposed to design a subsurface drip irrigation system to accommodate all sanitary sewage dispersal. Sizing as follows:

Proposed Septic System Design Flow: 1,675 gpd

Proposed Pretreated Effluent Loading Rate: 0.6 gpd/sf (Moderate Strong Sandy Loam/Sandy

Clay loam)

This loading rate is within the suitable range for pretreated effluent in the onsite soil types and is more conservative than what is permissible for the onsite soils.

1,675 GPD

13530.0 Vintage Wine Estates_Girard Winery Wastewater Feasibility Study February 20, 2014

Revised: September 9, 2015



Proposed Sanitary Sewage Management System

With improvement to the site, the following tanks are proposed for the Girard Winery septic system. Because a pretreatment system is required for subsurface drip, a septic, recirculation, and sump tank are required for an AdvanTex pretreatment system. Other NSF Certified pretreatment systems may be reviewed at the time of Construction Drawings. Tank sizes are verified using the plumbing code commercial sizing formula.

V = 1,125 + 0.75 x Q = 1,125 + 0.75 x 1,675 gpd = 2,381.25 gallons

Septic Tank:

Recirculation Tank:

Sump/Dispersal Equalization Tank:

6,000 gallons (3.6 days retention time)

2,000 gallons (1.2 days retention time)

3,000 gallons (1.8 days retention time)

These tank volumes meet the minimum criteria for an AvanTex pretreatment system. Tank sizes may be revised if a different treatment system is selected, but all tanks associated with the septic system are proposed to be subsurface tanks of concrete or fiberglass construction. Whichever treatment system is selected, it will be required to have sufficient existing installations with satisfactory results for at least 5 years of operation, so as to avoid failures due to manufacturer's flaws in design.

Leachfield Sizing

The area required for a primary sanitary sewer drip system is as follows:

Area Required = Flow/Application Rate

= 1,675 gpd / 0.6 gpd/sf

= 2,792 sf

Reserve Area

200% reserve area, or 5,584 sf, is required for this site and is shown adjacent to the primary septic area on the Use Permit Site Plan.

Irrigation Reuse Alternative

Although groundwater monitoring has been performed and shown that the site can support a subsurface drip irrigation, mound, or at-grade type septic system it is also desired to have the ability to provide a pretreatment and irrigation reuse system, in the event that is desired to recycle the treated effluent for onsite irrigation of landscape. The Lyve Wastewaer System has been used at



Alpha Omega Winery in St. Helena to treat and reuse domestic wastewater for irrigation on their site landscape. For this project, if reuse is pursued, the treatment system shall be a Biomicrobics BioBarrier Membrane Bioreactor (MBR) which is NSF 350 certified for reuse of graywater and NSF40 certified for treatment of domestic wastewater and is capable of consistently producing effluent with BOD and TSS of less than 10 mg/L . A process wastewater BioBarrier is installed at Sinegal Winery in St. Helena and operating without issue. A design for a BioBarrier MBR would include the following physical components:

Septic Tank: 2,000 gallons
Processing Tank: 13,000 gallons
Treated Collection Sump: 1,500 gallons
Treated Storage Tank: 40,000 gallons

The system also includes an aeration system as well as various pumps for transfer of waste and may also require nutrient addition to provide proper chemical ratios required for biological cell growth and waste degradation. Sampling of the waste stream in use is required to identify nutrient deficiencies. Ultraviolet (UV) disinfection would be provided after treatment as well as between treated storage and final irrigation reuse. A storage tank would be provided for periods in the winter when irrigation reuse cannot occur. The storage tank would be the only above grade tank involved and could end up below grade, depending on final layout and available space in the treatment system area. As demonstrated in the process wastewater section of this study, more than sufficient vineyard is available onsite for irrigation dispersal of effluent, as well as the proposed landscape areas. Approximately 3 acres is required for process wastewater and a total of 18 acres vineyard is available onsite.

If treatment, irrigation, and reuse is proposed for construction of this project, the project must first obtain approval from the San Francisco Bay Regional Water Quality Control Board (SFBREWQCB) for this use. Prior to issuance of building permits, the RWQCB will need to approve of the proposal, and issue Waste Discharge Requirements including monitoring requirements for the reuse of the sanitary sewage. In this event, the RWQCB must also grant system approval prior to building permit issuance.

PROCESS WASTEWATER (PW)

Existing System

The existing on-site process wastewater system consists of 2 aerated facultative lagoons and an irrigation holding pond. This system is currently treating the process waste from the Clos Pegase winery located across Dunaweal Lane under the same ownership. No sanitary wastewater is discharged into the process wastewater system.



Before entering the process wastewater ponds, the entire flow of process wastewater is filtered through a rotary screen where suspended solids are collected and removed. Biological stabilization occurs in the facultative pond system. The total volume of the existing pond system is approximately 1.5 MG. There is a 10 hp aerator in Pond 1 and a 5 hp aerator in Pond 2. Clos Pegase is currently producing 200,000 gallons of wine with an average annual PW production of 920,000 gallons. This pond system is large enough to provide at least 200 days of retention time at current Clos Pegase average flow conditions. Treated PW is used for irrigation of the onsite vineyards.

Proposed System

The proposed PW system for the new Girard Winery will connect to the existing PW wastewater pond system. The new PW connection will include a pump sump and new aerators to accommodate the increase in flows.

Proposed Flow Calculations

The winery is currently proposing a production of 200,000 gallons of wine per year. Using a monthly PW distribution from multiple wineries and a PW generation rate of 4.6 gal PW per gal wine produced (from Clos Pegase data) flow rates are estimated as follows:

Winery Process Wastewater (PW)

Average Daily Flow = 2,521 gal PW/day

Average Harvest Day = 3,950 gal PW/day

Average Day, Peak Harvest Month = 5,060 gal PW/day

(See calculations spreadsheet)

The design flow proposed to the system is 10,120 gpd (5,060 gpd from Girard and 5,060 gpd from Clos Pegase). It should be noted that although the assumption of 4.6 gallons of process wastewater per gallon wine produced is used for sizing (as taken from existing Clos Pegase winemaking practices and assumed to be similar for Girard), actual water use data from the existing Girard operation in Sonoma indicates a water use rate of 3.0, 2.7, and 2.5 gallons process wastewater per gallon of wine produced for 2012, 2013, and 2014, respectively. Therefore, with a new water-efficient winery and closer contact with winemaking at Clos Pegase, the overall water use per gallon should be less than historically used at Clos Pegase.

Aerator Sizing

The Aerators have been sized using a BOD mass loading and the Aqua-Jet Surface Mechanical Aerator brochure specifications. Calculations (attached) show that a total of 22.5 hp of aerators is required for both ponds. It is proposed to add a second 10 hp aerator to Pond 1 for a total of 20



hp in Pond 1. This results in a power to volume (P/V) ratio of 0.21 hp per 1000 ft³. This is sufficient for surface mixing and aeration in Pond 1. Pond 2 has an (E) 5 hp aerator. This provided a P/V ratio of 0.05 hp per 1000 ft³. This is sufficient for surface mixing and to prevent odors in Pond 2. No aeration should be required in the irrigation pond due to dilution, level of treatment exiting Pond 2, and natural aeration from algae. In addition, an Anti-Erosion Assembly is recommended for both aerators, to minimize sediment mixing during periods of low liquid levels in the ponds.

Pond Sizing

The facultative ponds combined volume is roughly 1.5 MG. This provides for a retention time of >140 days at peak month flows (see calculations spreadsheet). Facultative pond systems are sized with a minimum of 60 days in the entire system, and at least 45 days in the first pond. Therefore, this system will have sufficient contact time for treatment before discharge. During the rainy winter months when irrigation needs are low the existing irrigation pond will be used as a detention system to hold excess effluent until the spring months when increased irrigation loading is appropriate.

Irrigation Reserve/Dispersal

A total of 7.5 acres of vineyard is required for dispersal of effluent to avoid ponding and concentration.

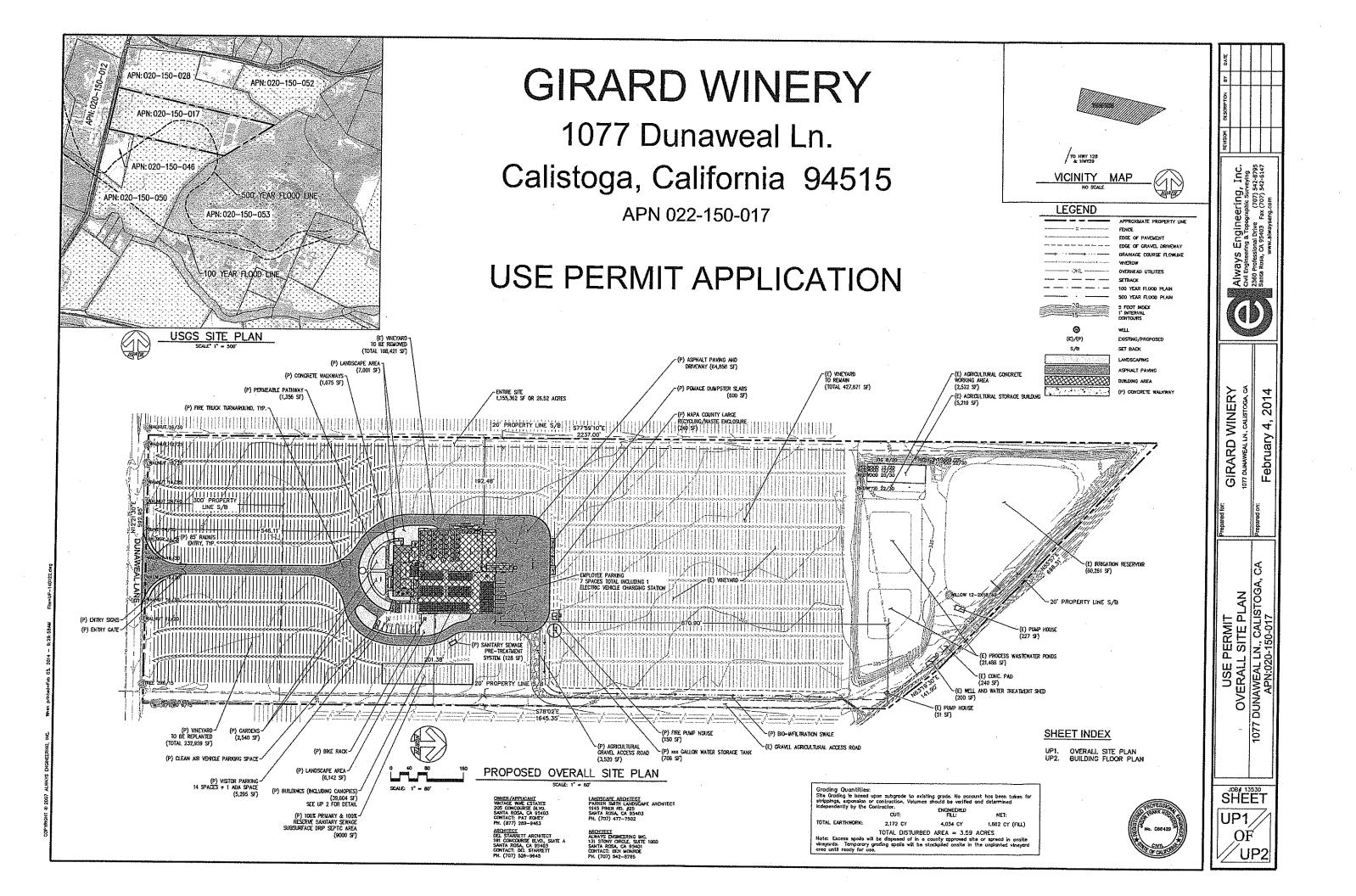
SUMMARY AND CONCLUSIONS

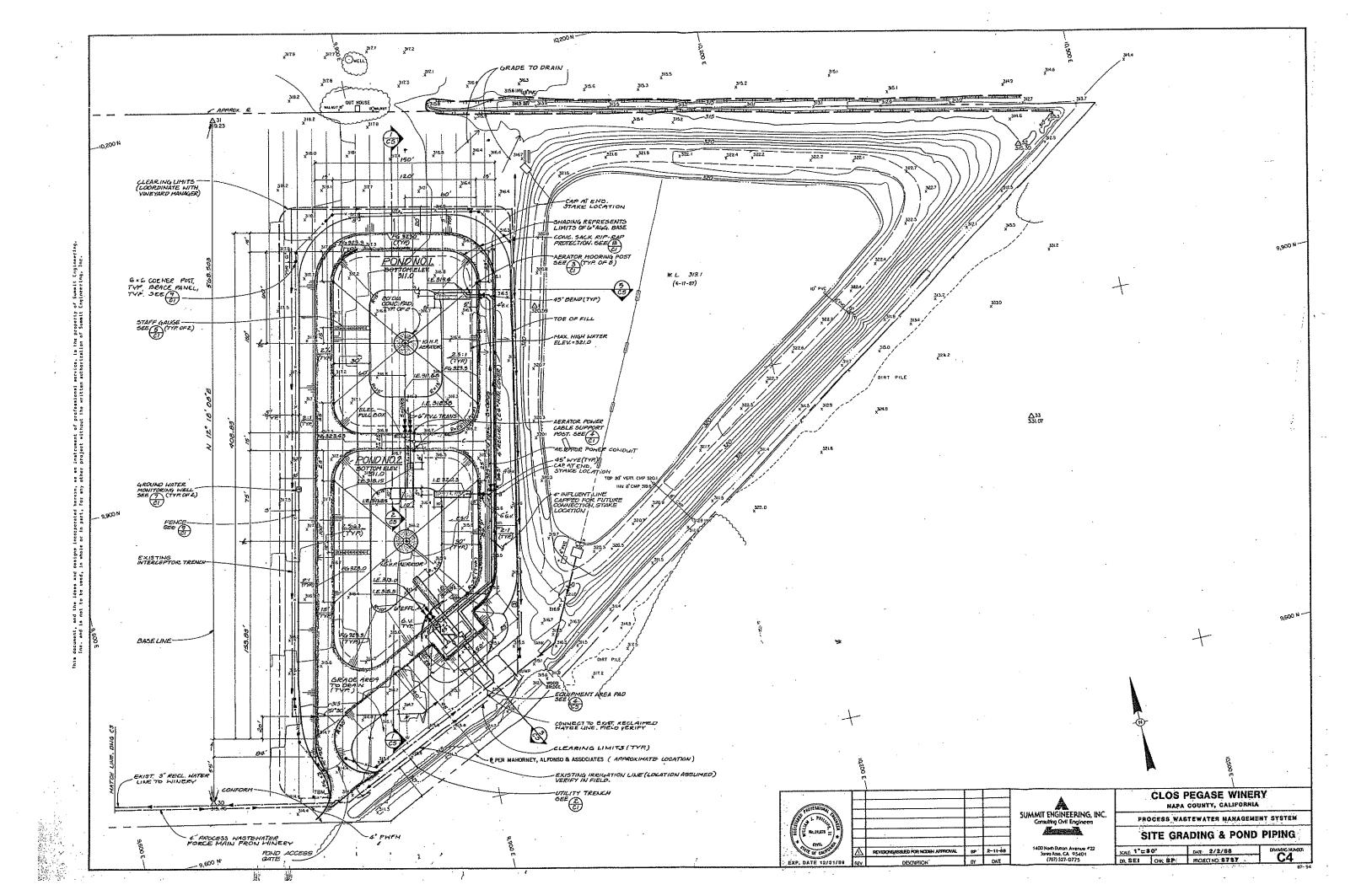
Sanitary Wastewater

With the proposed installation of a new sanitary management system, as discussed in this report, the site is capable of supporting the proposed sanitary sewage loads.

Process Wastewater

With the proposed installation of additional aerators and a collection system and pump station, the existing aerated facultative pond system is sufficient for the proposed Girard Winery PW flows in addition to the existing Clos Pegase Winery PW flows.





Designed By:

BM/RO - Always Engineering, Inc.

Project: Girard Winery Use Permit

Girard Winery

Annual Process Wastewater Flow

=

920,000 gallons PW/year

*Refer to the design calculations report for additional flow estimates.

<u> </u>	····		
Month	Percentage of Annual Flow (%)	Monthly Flow (MGal)	Days
January	6.50%	0.060	31
February	7.00%	0.064	28
March	8.00%	0.074	31
April	7.00%	0.064	30
May	6.50%	0.060	31
June	5.50%	0.051	30
July	6.00%	0.055	31
August	10.50%	0.097	31
September	16.50%	0.152	30
October	12.50%	0.115	31
November	7.50%	0.069	30
December	6.50%	0.060	31
Total	100.00%	0.920	365

Project: Girard Winery Use Permit

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Girard Winery PROCESS WASTEWATER

Annual Volume

Annual Production (projected)				=	1,212 ton/year
Wine Generation Rate (assumed) ^a				=	165 gal wine/ton
Wine Produced	1,212 ton/year	x	165 gal wine/ton	=	200,013 gal wine/year
Process Wastewater (PW) Generation Rate ^b	(assumed)			=	4.60 gal PW/gal wine
Annual PW Flow	200,013 gal wine/year	х	4.60 gal PW/gal wine	=	920,060 gal PW/year
Average Day Flow					
	920,060 gal PW/year	÷	365 days	=	2,521 gal PW/day
Average Harvest Day					
Total Harvest Flow ^c	920,060 gal PW/year	x	39.5%	=	363,424 gal PW/harvest
Average Harvest Flow (3 month harvest)	363,424 gal PW/harvest	÷	92 days	=	3,950 gal PW/day
Average Day, Peak harvest Month - Pond Design	<u>.</u>				
Total Peak Month Flow ^c	920,060 gal PW/year	×	16.5%	æ	151,810 gal PW/month
Average Day, Peak Month Flow	151,810 gal PW/month	÷	30 days	=	5.060 gal PW/day

a. 165 Gal wine per ton of grapes is used as a wine industr standard

b. 4.6 gal of PW per gallon wine produced over the course of 1 year is based on hisotrical data from Clos Pegase and existing Griard operations.

c. Percentage of PW produued during each month is based on the average flow distirubtion from 16 wineries

Project: Girard Winery Use Permit

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Clos Pegase Winery

Annual Process Wastewater Flow

920,000 gallons PW/year

*Refer to the design calculations report for additional flow estimates.

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June	5.50%	0.051	30
July	6.00%	0.055	31
August	10.50%	0.097	31
September	16.50%	0.152	30
October	12.50%	0.115	31
November	7.50%	0.069	30
December	6.50%	0.060	31
Total	100.00%	0.920	365

Project: Girard Winery Use Permit

Designed By:

BM/RO - Always Engineering, Inc.

Clos Pegase Winery PROCESS WASTEWATER

Annual Volume

Annual Production (projected)				=	1,212 ton/year
Wine Generation Rate (assumed) ^a				=	165 gal wine/ton
Wine Produced	1,212 ton/year	×	165 gal wine/ton	=	200,013 gal wine/year
Process Wastewater (PW) Generation Rate ^b	(assumed)			=	4.60 gal PW/gal wine
Annual PW Flow	200,013 gal wine/year	x	4.60 gal PW/gal wine	=	920,060 gai PW/year
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c. Percentage of PW produced during each month is based on the average flow distirubtion from 16 wineries



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Climate Data

Project: Girard Winery Use Permit

		Reference	Pan	Lake	Average	10-Year	100-year
Month	Days	Evapotranspiration ¹	Evaoporation	Evaporation	Precipitation	Precipitation	Precipitation
		(inches)	(inches)	(inches)	(inches)	(inches)	(inches)
January	31	1.0	1.5	1.2	9.0	12.9	17.6
February	28	1.5	2.2	1.7	5.6	8.0	11,0
March	31	2.9	3.8	2.9	5.7	8.1	11.2
Aprii	30	4.7	5.8	4.5	2.6	3.7	5.1
Мау	31	5.8	6.8	6.9	9.0	6.0	1.2
June	30	6.9	11.0	8.5	0,2	0.3	0.4
July	31	7.2	13.2	10.2	0.1	0.1	0.2
August	31	6.4	12.1	9.3	0.2	0.3	0.4
September	30	4.9	8.7	6.7	0.3	0.4	9.0
October	31	3.5	5.7	4.4	2.4	3,4	4.7
November	30	1.6	2.5	1.9	6.8	9.7	13.3
December	31	1.2	1.7	1.3	8.2	11.7	16.1
TOTAL	365.0	47.7	77.0	59.3	41.7	59.6	81.8

1 Reference Evapotranspiration data is for the Angwin FS obtained from the California Irrigation Management Information System See http://wwwcimis.water.ca.gov/cimis/monthlyEToReport.do

2 Average Monthly Pan Evaopration Rates observed at Berryessa Lake, Ca between 1957 and 1970.

3 Lake evaopration is pan evaporation multiplied by a 0.77 factor.

4 Average precipitation data is from TheWeatherChannel.com for Calistoga, CA See http://www.weather.com/weather/wxclimatology/monthly/94515

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Date: 02/20/2014 Project: Girard Winery Use Permit **Pond 1 Balance**

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	Volume		(Mgal)	0.293		0.137	0.137	0.000	0.137 0.000 0.000 -0.100	0.000 0.000 0.000 -0.100	0.137 0.000 0.000 -0.100 -0.200	0.137 0.000 0.000 -0.100 -0.200 0.000	0.137 0.000 0.000 -0.100 -0.200 0.000	0.137 0.000 0.000 -0.100 -0.200 0.000 -0.024	0.137 0.000 0.000 -0.106 -0.200 0.000 0.000	0.137 0.000 0.000 -0.100 -0.200 0.000 0.000 0.000
	Water Depth at	end of month	(feet)	8.7		10.0	10.0	10.0	10.0 10.0 10.0 9.1	10.0 10.0 10.0 9.1 8.0	10.0 10.0 10.0 9.1 8.0 5.7	10.0 10.0 10.0 9.1 8.0 5.7	10.0 10.0 10.0 9.1 8.0 5.7 5.7	10.0 10.0 10.0 9.1 8.0 5.7 5.7 5.7	10.0 10.0 10.0 9.1 8.0 5.7 5.7 5.7 5.4	10.0 10.0 10.0 9.1 8.0 5.7 5.7 5.7 5.4 5.4
	Volume at end of	Month	(Mgal)	0.593		0.730	0.730	0.730 0.730 0.730	0.730 0.730 0.730 0.630	0.730 0.730 0.730 0.630 0.524	0.730 0.730 0.730 0.630 0.524 0.324	0.730 0.730 0.730 0.630 0.524 0.324	0.730 0.730 0.730 0.630 0.524 0.324 0.324	0.730 0.730 0.730 0.630 0.524 0.324 0.324 0.324	0.730 0.730 0.730 0.630 0.524 0.324 0.324 0.324 0.320	0.730 0.730 0.730 0.630 0.524 0.324 0.324 0.320 0.300
out	Discharge to	Pond 2	(Mgal)	0.000	The state of the s	00,100	0,100	0.100 0.257 0.179	0.100° 0.257; 0.179 0.231	0.100 0.257 0.179 0.231 0.211	0,100 0,257 0,179 0,231 0,211	0.100 0.257 0.179 0.231 0.211 0.312	0.100 0.257 0.179 0.231 0.211 0.312 0.312	0.100 0.257 0.179 0.211 0.312 0.197 0.300	0.100 0.257 0.179 0.231 0.312 0.309 0.309 0.300	0.100 0.257 0.231 0.211 0.312 0.309 0.300 0.269
Output	Pond	Evaporation*	(Mgal)	600.0		0.015	0.015	0.015 0.027 0.042	0.015 0.027 0.042 0.061	0.015 0.027 0.042 0.061 0.070	0.015 0.027 0.042 0.061 0.070	0.015 0.027 0.042 0.061 0.070 0.072	0.015 0.027 0.042 0.061 0.070 0.072 0.059	0.015 0.027 0.042 0.061 0.070 0.072 0.059 0.042	0.015 0.027 0.042 0.061 0.070 0.072 0.059 0.042	0.015 0.027 0.042 0.061 0.070 0.072 0.059 0.042 0.027
	10 Year	Precipitation	(Mgal)	0.173		0.108	0.108	0.108 0.110 0.050	0.108 0.110 0.050 0.012	0.108 0.110 0.050 0.012 0.004	0.108 0.110 0.050 0.012 0.004	0.108 0.110 0.050 0.012 0.004 0.002	0.108 0.110 0.050 0.012 0.004 0.002 0.004	0.108 0.110 0.050 0.004 0.002 0.006 0.006	0.108 0.110 0.050 0.012 0.004 0.006 0.006 0.046	0.108 0.110 0.050 0.012 0.004 0.006 0.046 0.131
Input	Process	Wastewater In	(Mgal)	0.120		0.129	0.129	0.129 0.147 0.129	0.129 0.147 0.129 0.120	0.129 0.147 0.129 0.120 0.101	0.129 0.147 0.129 0.120 0.101	0.129 0.147 0.129 0.120 0.101 0.110	0.129 0.147 0.129 0.120 0.101 0.110 0.193	0.129 0.147 0.129 0.120 0.101 0.193 0.304	0.129 0.147 0.129 0.120 0.101 0.110 0.193 0.304 0.230	0.129 0.127 0.120 0.101 0.110 0.193 0.304 0.230 0.138
	Start	Volume	(Mgal)	0.300		0.593	0.593	0.593 0.730 0.730	0.593 0.730 0.730 0.730	0.593 0.730 0.730 0.730 0.630	0.593 0.730 0.730 0.630 0.524	0.593 0.730 0.730 0.630 0.524 0.324	0.593 0.730 0.730 0.630 0.524 0.324	0.593 0.730 0.730 0.630 0.524 0.324 0.324	0.593 0.730 0.730 0.630 0.524 0.324 0.324 0.324	0.593 0.730 0.730 0.630 0.524 0.324 0.324 0.324 0.300
		Month		January		repruary	rebruary March	March April	March April May	March March April May June	March April May June	March April May June July August	March April May June July August September	March April May June July August September October	March April May June July August September October	March April May June July August September October November December

Designed By: BM/RO - Always Engineering, Inc.

Date: 02/20/2014 Project: Girard Winery Use Permit Pond 2 Balance

_							_		·								
		Volume	Change	(Meal)	0.175	0.209	-0.082	-0.170	-0.057	-0.085	-0.086	-0.099	0.015	-0.003	-0.049	0.231	0000
THE PERSON NAMED IN COLUMN NAM			Water Depth	(feet)	9.1	10.8	10.2	8.7	8.2	7.4	6,5	5.4	5.6	5.5	5.0	7.5	
	Volume at	end of	Month	(Mgal)	0.705	0.915	0.833	0.662	0.605	0.520	0.434	0.335	0.350	0.347	0.299	0.530	
put	Discharge to	Irrigation	Pond	(Mgal)	0,000	0.000	0.450	0.400	0,300	0.300	.00.400	0.300	0.300	0.350	0,450	0.206	3.456
Output		Pond	Evaporation*	(Mgal)	0.011	0.017	0.031	0.044	0.062	0.073	0.082	0.068	0.047	0.031	0.013	0.010	0.489
. ب		10 Year	Precipitation	(Mgal)	0.175	0.109	0.111	0.051	0.012	0.004	0.002	0.004	900'0	0.047	0.133	0.160	0.813
Input	Process	Wastewater In	From Pond 1	(Mgal)	0.000	0.100	0.257	0.179	0.231	0.211	0.312	0.197	0.309	0.300	0.269	0.278	2.643
		Start	Volume	(Mgal)	0.530	0.705	0.915	0.833	0.662	0.605	0.520	0,434	0.335	0.350	0.347	0.299	
			Month		January	February	March	April	May	June	July	August	September	October	November	December	Total

Designed By: BM/RO - Always Engineering, Inc.

Project: Girard Winery Use Permit

Landscape

0.5 acres

Vineyard =

2.5 acres 0 acres

Pasture =

Soil perc rate =

1 inches/hour

Month	Days	Reference Evapotranspiration ¹	Landscape Crop Coefficient	Pasture Crop Coefficient	Vineyard Crop Coefficient	Landscape E T	Pasture ET	Vineyard ET	Precipitation	Landscape Den	_	1	Irrigation and	Vineyard Dem	-	Irrigation Days per Month	Perco Capa		Dispers	Capacity	F	Efficient to	
1	24	(inches)				(inches)	(inches)	(inches)	(inches)	(inches)	(Mgal)	(inches)	(Mgal)	(inches)	(Mgal)	(days)	(in)	(Mgai)	(in)	(Mgal)	(in)	on Pond	Capacity '
January	31	1.0	0.8	0.8	0.0	0.8	0.8	0.0	9.0	0.0	0.000	0.0	0.000	0.0	0.000	5	0.0	0.000	0.0			(Mgal)	(Mgal)
February	28	1.6	0.8	0.8	0.0	1.3	1.3	0.0	5.6	0.0	0.000	0.0	0.000	0.0	0.000	5.0				0.000	0.000	0.000	0.000
March	31	3.0	0.8	0.8	0.0	2.4	2.4	0.0	5.7	0.0	0.000	0.0	0.000	0.0	0.000		0.0	0.000	0.0	0.000	0.000	0.000	0.000
April	30	4.6	0.9	0.9	0.2	4.2	4.2	0.9	2.6	1.6	0.021	1.5	0.021	1	i	12.0	5.8	0.474	5.8	0.474	0.460	0.450	0.024
May	31	6.0	0.9	0.9	0.6	5.4	5.4	3.6	0.6	4.8	0.065			0.0	0.000	13.0	9.9	0.805	13.0	0.848	0.409	0.400	0.448
June	30	7.0	0.9	0.9	0.7	6.3	6.3	4.9	0.2			4.8	0.065	3.0	0.041	16.0	14.8	1.202	27.3	1.373	0.307	0.300	1.073
July	31	8.0	0.9	0.9	0.6	7.2	7.3	1	1	5.1	0.083	6.1	0.083	4.7	0.064	17.0	16.1	1.313	33.0	1.543	0.307	0.300	1.243
August	31	7.0	0.9	0.9	0.5		7.2	4.8	0.1	7.1	0.096	7.1	0.096	4.7	0.064	30.0	28.7	2.338	47.6	2.594	0.409	0.400	2.194
September	30	5.2	0.9	1	1	6.3	6.3	3.5	0.2	6.1	0.083	6.1	0.083	3.3	0.045	. 31.0	29.6	2.408	45.1	2.519	0.307	0.300	2.319
October	31	3.4		0.9	0.3	4.7	4.7	1.6	0.3	4.4	0.059	4.4	0.059	1.3	0.017	30.0	28.5	2.322	38.5	2.457	0.307	0.300	2.157
		i i	0.9	0.9	0.1	3.0	3.0	0.3	2.4	0.6	0.008	0.6	800.0	0.0	0.000	16.0	13.0	1.056	14.2	1.073	0.358	0.350	0.723
November	30	1.4	0.8	0.8	0.0	1.1	1.1	0.0	6.8	0.0	0.000	0.0	0.000	0.0	0.000	14.0	5.5	0.541	6.6	0.541			
December	31	0.9	0.8	8.0	0.0	0.7	0.7	0.0	8.2	0.0	0.000	0.0	0.000	0.0	0.000	5.0	0.0				0.460	0.450	0.091
TOTAL	365.0	49.1				43.4	43.4	19.6	41.7	30.7	0.4	30.7	0.4	16.9	5.500	189.0	152.9	0.000	0.0 231.2	0.000 13.520	0.211 3.536	0.206 3.456	-0.205

- 1 Average monthly reference evapotranspriation rates, refer to Climate spreadsheet.
- 2 Pasture coefficient from Table 5-1, "Irrigation with Reclaimed Municipal Wastewater A Guideance Manual," Californal State Water Resources Control Board, July 1984 (San Juaquin Valley)
- 3 Vineayrd coefficient from Table 5-12, "Irrigation with Reclaimed Municipal Wastewater A Guideance Manual," Californai State Water Resources Control Board, July 1984 (5an Juaquin Valley)
- 4 Crop coefficient times the reference evapotranspiration.
- 5 Precipitation for a 10-yr event, refer to the Climate Spreadsheet.
- 6 Irrigation demand is the evapotrasppiration minus the precipitation
- 7 Residual capacity estimates irrigation/percolation capacity with the assumption that all PW discharged from Pond 2 is used for irrigation. Effluent is actually discharged into the irrigation pond for use during spring and summer vineyard irrigation.

Designed By: BM/RO - Always Engineering, Inc. **Aeration Calculations**

Project: Girard Winery Use Permit

= Estimated Average Daily Flow Design Flow

10,120 gal/day 0.010 Mgal/day 38 m^3/day 38,294 liters/day

BOD MASS LOADING - Amount of Biochemical Oxygen Demand (BOD) Based on Amount of Organics in Wastewater

= 7700 mg/L **BOD** into Pond (Table 4-12 & 4-14 of Small and Decentralized Wastewater Management Systems)

BOD Mass Load 38 m^3/day 7700 mg BOD/L 1000 mL/m^3 x 0.000001 kg/mg

294.9 kg BOD/day 648.7 lb BOD/day

OXYGEN REQUIREMENTS - The amount of oxygen requiremed to breakdown the waste in the water

O2 Requirement

Number if cells

648.7 lb BOD/day

973.1 lbs O2/day

HORSEPOWER REQUIREMENTS - The horsepower of aeration required to provide the necessary amount of oxygen

Oxygen Transfer Efficiency 1.8 lbs O2/Hp*hr (3.4 assumes a VBT aerator, model 100)

1.8 lbs O2/Hp*hr ÷ 24 hr/day 973.1 lbs O2/day Horsepower Requirement

22.5 Hp required

POWER TO VOLUME RATIO (Hp/10⁻³ ft⁻³) - This is used to estimate the amount of mixing which will occur in a pond due to aeration

Pond Volume 0.723 Mgal

722,797 gallons 96,631 ft^3 2

Ratio of first to second cell 2 Volume in Pond 1 722,797 gallons 96,631 ft^3

Volume in Pond 2 803,995 gallons 107,486 ft^3

Horsepower in Pond 1; cell 1 20. Hp

Pond 1 Power to Volume Ratio 20 Hp 1000 ft^3 96,631 ft^3 1000 ft^3

0.21 Hp/1000 ft^3

5 Hp Horsepower in Pond 1, cell 2 ÷ 107,486 ft^3 1000 ft^3 1000 ft^3

Pond 2 Power to Volume Ratio 5 Нр

0.05 Hp/1000 ft^3 (Page 463 of Small and Decentralized Wastewater Management)

Complete Mix = 0.75 - 1.5 Hp/1000 ft^3 Hp/1000 ft^3 Partial Mix = 0.4 - 0.75

Facultative = 0.1 - 0.4 Hp/1000 ft^3

Pond 1

Retention Time (t)/ Estimated Effluent

Cn Effluent BOD Со 7700 mg/L

= 1 for single cell pond n

0.276 d^(-1) = k * 71.4 days 372 mg/L Cn = Effluent BOD 372 mg/L

Pond 2 Pond 1

Retention Time (t)/ Estimated Effluent

Cn ≈ Effluent BOD Co 372 mg/L ==

1 for baffled pond n =

0.276 d^(-1) = k = 71.4 days 18 mg/L Cn = Effluent BOD 18 mg/L

SITE EVALUATION REPORT

Page_1_of_3

Please attach an 8.5" x 11" plot map showing the locations of all test pits triangulated from permanent landmarks or known property corners. The map must be drawn to scale and include a North arrow, surrounding geographic and topographic features, direction and % slope, distance to drainages, water bodies, potential areas for flooding, unstable landforms, existing or proposed roads, structures, utilities, domestic water supplies, wells, ponds, existing wastewater treatment systems and facilities.

Permit #: E13-00744		
APN: 020-150-017		
(County Use Only) Reviewed by:	Date:	 **************************************

PLEASE PRINT OR TYPE ALL INFORMATION

Property Owner Vintage Wine Estates dba Girard Winery			x New Construction	on Addition	☐ Remodel ☐ Relo	cation
Property Owner Mailing Address 205 Concourse Blvd			☐ Residential - #	of Bedrooms:	Design Flow:	gpd
City State Santa Rosa CA Site Address/Location 1077 Dunaweal Lane Calistoga, CA 94515	95403		Sanitary Waste	Type: Winery dom : 500-1675 gpd	Process Waste:	0 gpd
Evaluation Conducted Dv			Sanitary Wast	e: gpd 	Process Waste:	gpd
Evaluation Conducted By: Company Name	Evaluator's Name			Signatuse (Civil	Engineer, R.E.H.S. Geologist, So	I Scientist\
Always Engineering, Inc.	Ben Monroe, P.E.	RIE	70012	1	Nwe	- ocemsty
Mailing Address: 131B Stony Circle, Sutie 1000				Telephone Nur (707) 542-879		
City Santa Rosa, Ca 95401	State	Zip		Date Evaluatio 11/14/2013	n Conducted	

Primary Area	Expansion Area
Acceptable Soil Depth: 24-48 in. Test pit #'s: TP1-TP6	Acceptable Soll Depth: 24-48 in. Test pit #'s: TP1-TP6
Soil Application Rate (gal. /sq. ft. /day): 0.75 to 1.0 gpd/sf	Soil Application Rate (gal. /sq. ft. /day):0.75 to 1.0 gpd/sf
System Type(s) Recommended: PD, drip – pending gw	System Type(s) Recommended: PD, drip – pending gw
Slope: 3-5 %. Distance to nearest water source: 1000 ft.	Slope: 3-5 %. Distance to nearest water source: 1000 ft.
Hydrometer test performed? No	Hydrometer test performed? No
Bulk Density test performed?	Bulk Density test performed? No
Percolation test performed? No	Percolation test performed? No
Groundwater Monitoring Performed? Pending Rain	Groundwater Monitoring Performed? Pending Rain

Site constraints/Recommendations:

- Existing well
- Groundwater monitoring to be performed to identify perched groundwater level due to presence of mottling at less than 24 inches deep.
- Interceptor drain and surface drainage to divert away from septic area recommended.
- Proposed drainage features and grading will need to avoid.
- Additional test pits near wastewater ponds showed signs of significant seasonal saturation and lesser depths of permeable soils. Pits on map but not logged due to time onsite.

Test Pit # 1

PLEASE PRINT OR TYPE ALL INFORMATION

Horizon	Boundary	%Rock	Texture	Structure	C	onsistenc	:e		···	Mottling
Depth (Inches)					Side Wall	Ped	Wet	Pores	Roots	
34	D/G	15-20	SCL	SAB,3	FR	S	S	3,C	1,M	1,VF
48	D/G	35	SCL	SAB,3	VF	S	SS	3,M	1,M	1,F
60+		<10	SCL	SAB,2	D/L	М	М	1,VF	1,M	2,P
									: 	
	:						~~~~~~~			
		ļ								

Test Pit #2

	Boundary	%Rock	Texture	Structure	C	onsistenc	e			Mottling
Horizon Depth (Inches)					Side Wall	Ped	Wet	Pores	Roots	
24	D/G	15-20	SCL	SAB,3	FR	S	S	3,C	1,M	1,VF
56	D/G	35	SCL	SAB,3	VF	S	SS	3,M	1,M	1,F
65+		<10	SCL.	SAB,2	D/L	М	М	1,VF	1,M	2,P
				•						
										m-u-room manorom

Test Pit # 3

Horizon		%Rock	Texture	Structure	C	onsistenc	е			Mottling
Depth (Inches)	Boundary				Side Wall	Ped	Wet	Pores	Roots	
28	D/G	15-20	SCL	SAB,3	FR	S	S	3,C	1,M	1,VF
60	D/G	15-20	SL/LS	SAB,3	F	М	SS	3,M/F	1,M	1,F
70+		<10	SCL	SAB,2	D/L	M	М	1,VF	1,M	2,P
***************************************								}		
		<u> </u>								

Test Pit # 4

PLEASE PRINT OR TYPE ALL INFORMATION

Horizon			Texture		C	onsistenc	е			Mottling
Depth (Inches)	Boundary	%Rock		Structure	Side Wall	Ped	Wet	Pores	Roots	
24	D/G	15-20	SCL	SAB,3	FR	S	S	3,C	1,M	1,VF
49	D/G	25	SCL	SAB,3	FR	F	S	2,M	1,M	2,F
60+	*** *** *** *** *** *** *** *** *** **	<10	SCL	SAB,2	D/L	L	М	1,VF	1,M	2,P
***************************************						***************************************				
1	<u> </u>	<u> </u>					***			

Test Pit #5

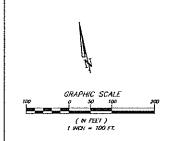
Uariasa	Boundary	%Rock	Texture	Structure	(Consistenc	е			Mottling
Horizon Depth (Inches)					Side Wall	Ped	Wet	Pores	Roots	
24	D/G	15-20	SCL	SAB,3	FR	S	S	3,C	1,M	1,VF
49	D/G	25	SCL	SAB,3	F	M/FR	SS	2,F	1,F	1,F
54+		>50%			· ·					

].									

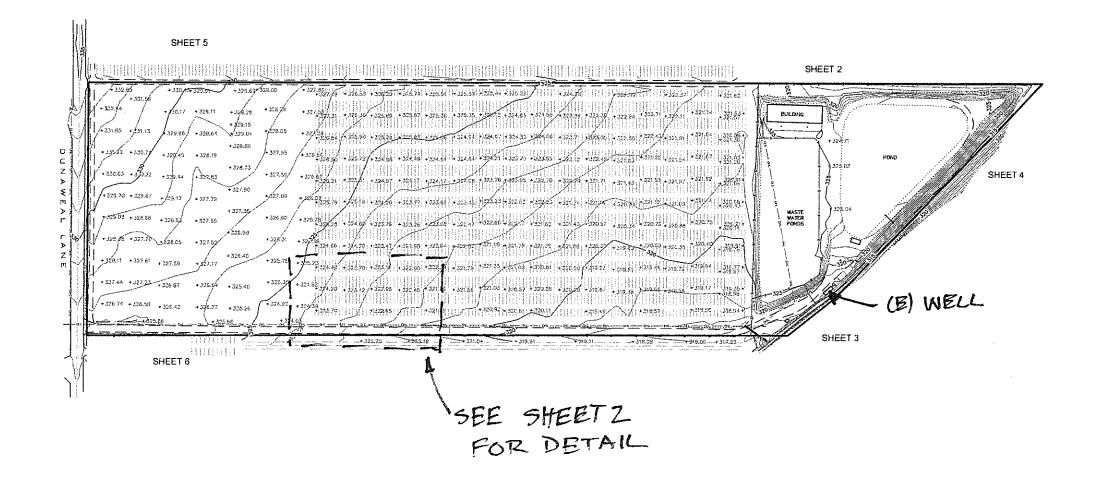
Test Pit # 6

Uautaan	Boundary	%Rock	Texture	Structure	C	onsistenc	e		***************************************	Mottling
Horizon Depth (Inches)					Side Wall	Ped	Wet	Pores	Roots	
36	D/G	15-20	SCL	SAB,3	FR	S	S	3,C	1,M	1,VF
55	D/G	25	SL	G/B,2	L	L	SS	2,C	1,M	1,D
70+		>50%							A.,	
Windows										

SHEET 1 OF Z



SITE EVALUATION 11/14/13 E13-00744



LEGEND:

ELECTRICAL
PHISWED PLOOR
MATER
REGEATION CONTROL VALVE BOX
JONT FOLIA
PRISWED PLOOR
PRISWED PLOOP
WHITE OAL
WHITE OAL
WHITE OAL
WHITE OAL
WHITE OAL
APPROXIMATE, PROPERTY LINE; SEE DRAWING MOTES
BUILDING LINE
EDGE OF MATERIAL
EDGE OF ASPHALT/CONCRETE PAVEMENT
FINITE OF CREEK OR DRAINAGE BITCH
OVERHAD POWER AND/OR TELEPHONE LINE
WHEROW

ALBION SURVEYS, INC.
CONSULTING LAND SURVEYORS
1113 HUNT AVENUE
ST. HELENA, CA 94574
(707) 963-1217
FAX (707) 963-1829

DRAWING NOTES

THE SHAP IS NOT A REMOVER SERVEY.

THE NAME IS NOT A REMOVED SERVEY.

FOR PROPISED TO LOCATE THE PROPISED SERVEY ROOS,
STREET AND NOT TO CARRANTEE ANY FASTI
MINISTER AND NOT TO CARRANTEE ANY FASTI
MINISTER ON PROSPECT OF CARRANTEE AND TO THE CARRANTEE ANY FASTI
A FALL SHAPEY SHOULD BE FRATERIAD FROM TO ANY
CERTAIN DEED NOSC. CONSTRUCTION OF CONNEXTANCE.
RESIDENTS MAY AFFICE THES PREPAIR.

THES SHAPCHE AREA HOT PROPISED ANY STORMATION
RECARDING EASTERNING BY THE CARRANTEE.

SITE INFORMATION

APN: 020~150~017

ADDRESS: 1077 DUNAWEAL LANE CAUSTOGA, CA 94515

MAP OF TOPOGRAPHY
OF A PORTION OF THE LANDS OF
CLOS PEGASE
COUNTY OF NAPA STATE OF CALFORNIA

REVISIONS & ADDITIONS FR: 877 ± 674 PG: 5-8 51-56

CONTOUR INTERVAL = 1" VIRTICAL DATUM BASED ON NAVO 88'

ORECTION OF NORTH BASED ON NAD 83" CALIFORNIA STATE PLANE ZONE :

LAUSTOGA, CA APN: 020-150-017

SHEET 2 OF 2 SITE EVALUATION 11/14/13 E13-00744 <u> — ОН</u>L — ОН<u>L — ОНL — ОНL — ОНL, — ОН</u>L, — ОН<u>L — ОНL, — ОНL, — ОНL — ОН</u>L.

> 1=50' N 0 10 20 30 4050 100

13530.0 Vintage Wine Estates Dunaweal Winery Groundwater Monitoring Report March 3, 2015



Napa County Planning, Building, and Environmental Services 1195 3rd Street, 2nd floor Napa, Ca 94559

Project:	1077 Dunaweal Ln
	Calistoga, CA 94515
	APN: 020-150-017

Copies	Document Date	Description
1	3/3/2015	Groundwater Monitoring Data
1	2/05/2015	Groundwater Monitoring Site Map
1		Napa County Dunaweal Rain Gauge

To whom it may concern,

This letter is provided as additional information for the Site Evaluation for the project located at 1077 Dunaweal Lane in Calistoga. This letter is a summary of the Groundwater Monitoring performed on the above referenced property.

On February 5, 2015 I installed eight (8) groundwater monitoring wells per the Napa County Instructions for Performing Site Evaluations. The holes were installed using 3" perforated pipes to a depth ranging from 48" to 58".

Monitoring was performed after the rains events occurring on 2/6 (accumulated total of 3.5") and 2/8-2/9 (accumulated total of 1.62"). Attached is rain data from the Napa County Dunaweal rain gauge. Three (3) separate sets of monitoring data were collected all within ten (10) days of this qualifying rain event and are attached to this letter.

The results of this monitoring can be found on the attached Groundwater Monitoring Data sheet. The most restrictive measurements will be used for septic system design. GW#5 was found to have groundwater at 13", making the area in the vicinity of this hole unsuitable for septic dispersal. ½ of the distance between this hole and passing holes should be used as a limit of suitable area. The remaining 7 holes (GW#1.4 & GW#6-7) all showed depths to groundwater ranging from 24.125" to 48.625", making this area suitable for a pre-treated subsurface drip irrigation system.

If there are questions please feel free to contact me.

Sincerely,

Ben Monroe, P.E. Always Engineering, Inc. Project Site: 1077 Dunaweal Lane Calistoga CA

APN: 020-150-017

Groundwater Monitoring Data



G	roundwate	r Hole Id:	GW#1	GW#2	GW#3	GW#4	GW#5	GW#6	GW#7	GW#8	
	en Hole e in Profile ell										
	Top of Pi	pe to Surface (Inches) =	4/8	1 2/8	2.5	2	2	4/8	3	3 6/8	
Ву	Weather	Date		Depth	from g	round to	groun	dwater	(GW) ir	inches	
ВМ	sunny	2/9/2015	33 4/8	32 6/8	24 1/8	31 2/8	13	43 6/8	46 3/8	49 5/8	
ВМ	sunny	2/10/2015	40 2/8	44	30 6/8	42 4/8	19 2/8	48 2/8	50 4/8	56 6/8	
ВМ	sunny	2/19/2015*	58	52	55	53 4/8	50 4/8	55 2/8	58	58	
		asurements hich did still									
		Thorr did out	navo	ground	water	100011	t at the	11110	7 1110111	toring.	

Created: 2/19/2015 Revised: 3/03/2015 1077 DUNAWEAL LN CALISTOGA, CA APN: 020-150-017

SHEET ZOFZ SITE EVALUATION 11/14/13 E13-00744 GW8 250

> 1=50' 0 1020304050 10

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National Weather Forcast for Napa
Precipitation
Stream Levels
Precipitation Map (24hr accumulation)
Napa River Flood Forecast
Live Doppler Storm Tracker
Napa County
City of Napa
City of St. Helena
OneRain Corporate

Napa River at Dunaweal Ln:Precipitation accumulation

Site:	Napa River at Dunaweal Ln
Site ID:	42

1 to 100 of 136 Report(s)

Reported ▼	Reading
2015-02-09 16:47:14	23.56 in
2015-02-09 10:36:19	23.56 in
2015-02-09 07:00:39	23.52 in
2015-02-09 05:14:37	23.48 in
2015-02-09 04:49:44	23.44 in
2015-02-09 01:04:34	23.44 in
2015-02-09 00:59:09	23.40 in
2015-02-09 00:54:34	23.36 in
2015-02-09 00:50:07	23.32 in
2015-02-09 00:45:57	23.28 in
2015-02-09 00:17:14	23.24 in
2015-02-08 22:34:32	23.20 in

	(,
2015-02-08 22:30:09	23.16 in
2015-02-08 21:36:09	23.13 in
2015-02-08 21:30:42	23.09 in
2015-02-08 21:24:57	23.05 in
2015-02-08 21:14:02	23.01 in
2015-02-08 21:09:44	22.97 in
2015-02-08 17:29:39	22.93 in
2015-02-08 17:13:57	22.89 in
2015-02-08 16:52:14	22.85 in
2015-02-08 12:28:04	22.85 in
2015-02-08 11:52:42	22.81 in
2015-02-08 11:42:42	22.77 in
2015-02-08 11:26:49	22.73 in
2015-02-08 11:10:22	22.69 in
2015-02-08 11:02:57	22.65 in
2015-02-08 10:58:37	22.61 in
2015-02-08 10:50:32	22.57 in
2015-02-08 10:42:39	22.53 in
2015-02-08 10:17:47	22.49 in
2015-02-08 09:48:17	22.46 in
2015-02-08 09:37:27	22.42 in
2015-02-08 09:15:34	22.38 in
2015-02-08 08:49:29	22.34 in
2015-02-08 08:43:09	22.30 in
2015-02-08 08:36:17	22.26 in
2015-02-08 08:25:49	22.22 in
2015-02-08 08:14:09	22.18 in
2015-02-08 08:03:19	22.14 in
2015-02-08 07:52:29	22.10 in
2015-02-08 07:38:14	22.06 in
2015-02-08 07:29:34	22.02 in
2015-02-08 06:51:14	21.98 in
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2015-02-08 04:54:59	21.94 in
2015-02-07 16:57:17	21.94 in
2015-02-07 04:59:34	21.94 in
2015-02-06 23:56:19	21.94 in
2015-02-06 23:30:49	21.90 in
2015-02-06 22:25:42	21.86 in
2015-02-06 22:18:24	21.83 in
2015-02-06 22:15:44	21.79 in
2015-02-06 22:10:19	21.75 in
2015-02-06 21:54:07	21.71 in
2015-02-06 21:32:02	21.67 in
2015-02-06 21:26:37	21.63 in
2015-02-06 21:09:39	21.59 in
2015-02-06 20:32:59	21.55 in
2015-02-06 20:13:59	21.51 in
2015-02-06 20:03:52	21.47 in
2015-02-06 19:30:14	21.35 in
2015-02-06 19:14:07	21.31 in
2015-02-06 18:46:19	21.27 in
2015-02-06 18:20:24	21.23 in
2015-02-06 18:07:54	21.19 in
2015-02-06 17:45:39	21.16 in
2015-02-06 17:39:42	21.12 in
2015-02-06 17:26:09	21.08 in
2015-02-06 17:02:14	21.04 in
2015-02-06 17:00:32	21.04 in
2015-02-06 16:25:52	21.00 in
2015-02-06 16:15:07	20.96 in
2015-02-06 16:08:34	20.92 in
2015-02-06 16:02:07	20.88 in
2015-02-06 15:57:42	20.84 in
2015-02-06 15:54:24	20.80 in

16/2010	Si. Napa Niver at Bahawaa En(2000)
2015-02-06 15:50:14	20.76 in
2015-02-06 15:48:02	20.72 in
2015-02-06 15:43:04	20.68 in
2015-02-06 15:29:47	20.64 in
2015-02-06 15:20:07	20.60 in
2015-02-06 15:12:14	20.56 in
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2015-02-06 14:47:04	20.45 in
2015-02-06 14:42:44	20.41 in
2015-02-06 14:38:57	20.37 in
2015-02-06 14:28:04	20.33 in
2015-02-06 14:20:39	20.29 in
2015-02-06 14:14:39	20.25 in
2015-02-06 13:48:37	20.21 in
2015-02-06 13:36:54	20.17 in
2015-02-06 13:27:07	20.13 in
2015-02-06 13:15:52	20.09 in
2015-02-06 13:10:07	20.05 in
2015-02-06 13:06:52	20.01 in
2015-02-06 13:03:59	19.97 in
2015-02-06 13:01:54	19.93 in
2015-02-06 13:00:27	19.89 in
2015-02-06 12:58:52	19.86 in

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Live Doppler Storm Tracker
Napa County
City of Napa
City of St. Helena
OneRain Corporate

Napa River at Dunaweal Ln:Precipitation accumulation

Site:	Napa River at Dunaweal Ln
Site ID:	42

2010			
Sensor:	Precipitation accumulation (2368) ▼		
Sensor ID:	2368		
	23.56 in		
Latest Danart	2015-02-19 16:00:09		
Latest Report:	0.00 in		
	Precipitation increment		
	7 DAY 23.8		
7 DAY Graph	23.6		
	23.4		
	23.2		
	2015-02-23 2015-02-25 2015-02-25 2015-02-25 2015-02-25 2015-02-25		
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Reported •	Reading
2015-02-06 12:55:02	19.82 in
2015-02-06 12:50:39	19.78 in
2015-02-06 12:48:34	19.74 in
2015-02-06 12:46:12	19.70 in
2015-02-06 12:39:04	19.66 in
2015-02-06 12:30:27	19.62 in
2015-02-06 12:19:44	19.58 in
2015-02-06 12:10:39	19.54 in
2015-02-06 12:03:24	19.50 in
2015-02-06 12:00:34	19.46 in
2015-02-06 11:57:27	19.42 in
2015-02-06 11:54:02	19.38 in

313,2313	on in tapa in the fact of all ballethodic En (2000)
2015-02-06 11:50:22	19.34 in
2015-02-06 11:46:12	19.30 in
2015-02-06 11:42:44	19.26 in
2015-02-06 11:39:12	19.22 in
2015-02-06 11:35:19	19.19 in
2015-02-06 11:29:44	19.15 in
2015-02-06 11:25:07	19.11 in
2015-02-06 11:18:32	19.07 in
2015-02-06 11:12:49	18.99 in
2015-02-06 11:07:57	18.95 in
2015-02-06 10:58:44	18.91 in
2015-02-06 10:51:04	18.87 in
2015-02-06 10:43:09	18.83 in
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2015-02-06 05:04:49	18.40 in
2015-02-05 17:07:29	18.40 in
2015-02-05 05:09:49	18.40 in
2015-02-04 17:12:32	18.40 in
2015-02-04 05:15:09	18.40 in

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