13530.0 Vintage Wine Estates Girard Winery Wastewater Feasibility Study February 20, 2014 Revised: May 5, 2014

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Girard Winery

1077 Dunaweal Ln., Calistoga, CA 94515 APN: 020-150-017

USE PERMIT WASTEWATER FEASIBILITY STUDY



Project and Site Background

Vintage Wine Estates owns and operates the existing "Clos Pegase" Winery located at 1060 Dunaweal Ln in Calistoga, Ca (APN: 020-150-012). Vintage Wine Estates also owns the parcel across Dunaweal Ln., (1077 Dunaweal Ln., APN: 020-150-017), which has the existing process wastewater ponds and water well for Clos Pegase.

Vintage Wine Estates is proposing to construct a new winery and tasting room (the Girard Winery) on the above referenced parcel. A production capacity of 200,000 gal of wine annually is proposed for the new Girard Winery. With the Use Permit, it is proposed to also treat the process waste (PW) generated by Girard Winery using the existing Clos Pegase Pond Treatment system. A new collection system and transfer pump sump will be required for Girard Winery. A new aerator in the process waste ponds will also be required. A new sanitary sewage system on-site is proposed to accommodate the winery employees, visitors, and events.

The parcel consists of existing vineyards, water supply well and treatment, an agricultural storage building, 2 PW treatment ponds and an irrigation storage pond. The parcel is generally flat, with a small flow line along the southern property line.

A site plan is provided in Enclosure B displaying the existing site and proposed wastewater system improvements.

SANITARY SEWAGE (SS)

Existing Site Evaluation

A site evaluation was performed by Ben Monroe, P.E. of Always Engineering and Peter Ex of Napa County on November 14, 2013. A total of 16 soil profiles were evaluated and 6 were logged for use. Test pits displayed a sandy clay loam surface soil which ranged in depth from 36" to 56" in depth. Soils were underlain by a sandy loam or loamy sand for a total permeable depth ranging from 49" to 60" in depth. All soil displayed a moderate to strong sub-angular blocky structure. Faint mottling was observed to 24" deep, with increasing intensity with depth below that. Prominent mottling was observed below 48" in all test pits. Additional groundwater monitoring is required onsite to determine if the upper mottling is due to subsurface groundwater or heavy irrigation of the onsite vineyards. At the time of preparation of this study, there has not been sufficient rainfall

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to perform groundwater monitoring and therefore, it is assumed that a minimum of 24" suitable soil is available for septic system design. An interceptor drain is also proposed with this feasibility study to ensure we have the required separation to seasonal groundwater. The Napa County Site Evaluation procedures indicate a Sandy clay loam or sandy loam with moderate structure should be loading at 0.75 to 1.0 gpd using pretreated effluent.

Proposed Wastewater Flows

The proposed onsite sanitary wastewater flow rate is entirely associated with the proposed Girard Winery. The use permit is requesting a similar level of use as Clos Pegase; an average number of 10 employees (15 gpcd) along with 75 visitors (3gpcd), and a peak number of 30 employees (15 gpcd) along with 100 visitors (3 gpcd). There will be one large event per year which will have 500 attendees. Portable toilets will be used for this event. All events will have fully catered food with all preparation and cleanup occurring off site. The proposed wastewater flows are estimated as follows:

<u>Average</u>
Employees

	8 FT employees 3 PT employees	X X	15 gpd/employee 7.5 gpd/employee		120 gpd 22.5 gpd
Tasti	ng Room				
	42 tasting visitors	x	3 gpd/visitor	strano Anada	126 gpd
Event	ts .				
	75 event visitors x	5 gpd,	/visitor	=	375 gpd
TOTA	L PROPOSED AVER	AGE D	DESIGN FLOW	=	643.5 GPD
<u>Peak</u> Empl	oyees				
	20 FT employees 10 PT employees		15 gpd/employee 7.5 gpd/employee	=	300 gpd 75 gpd
Tastii	ng Room				
	100 tasting visitors	x	3 gpd/visitor	=	300 gpd

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Events

200 event visitors x

5 gpd/visitor

= 1,000 gpd

TOTAL PROPOSED PEAK DESIGN FLOW <u>Proposed Sanitary Sewage Loading</u>

= 1,675 GPD

It is proposed to design a subsurface drip system to accommodate all sanitary sewage dispersal. Sizing as follows:

Proposed Septic System Design Flow:

1,675 gpd

Proposed Pretreated Effluent Loading Rate:

0.6 gpd/sf (Moderate -Strong Sandy

Loam/Sandy Clay loam)

This loading rate is within the suitable range for pretreated effluent in the onsite soil types. Because there has not been sufficient rainfall to perform ground water monitoring

Proposed Sanitary Sewage Management System

With improvement to the site, the following tanks are proposed for the Girard Winery septic system. Because a pretreatment system is required for subsurface drip, a septic, recirculation, and sump tank are required for an AdvanTex pretreatment system. Other NSF Certified pretreatment systems may be reviewed at the time of Construction Drawings. Tank sizes are verified using the plumbing code commercial sizing formula.

 $V = 1,125 + 0.75 \times Q$

= 1,125 + 0.75 x 1,675 gpd

= 2,381.25 gallons

Septic Tank:

6,000 gallons (3.6 days retention time)

Recirculation Tank:

2,000 gallons (1.2 days retention time)

Sump/Dispersal Equalization Tank:

3,000 gallons (1.8 days retention time)

These tank volumes meet the minimum criteria for an AvanTex pretreatment system.

Leachfield Sizing

The area required for a primary sanitary sewer drip system is as follows:

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Area Required = Flow/Application Rate

= 1,675 gpd / 0.6 gpd/sf

= 2,792 sf

Reserve Area

200% reserve area, or 5,584 sf, is required for this site and is shown adjacneet to the primary septic area on the Use Permit Site Plan.

Irrigation Reuse Alternative

In the event that groundwater monitoring cannot occur prior to the application for construction permits, it is also desired to have the ability to provide a pretreatment and irrigation reuse system. The Lyve Wastewaer System has been used at Alpha Omega Winery to treat and reuse domestic wastewater for irrigation. Also, the Biomicrobics BioBarrier Membrane Bioreactor (MBR) is NSF 350 certified for reuse. A design for a BioBarrier MBR would include the following:

Septic Tank: 2,000 gallons
Processing Tank: 13,000 gallons
Treated Collection Sump: 1,500 gallons
Treated Storage Tank: 40,000 gallons

A storage tank would be provided for period in the winter when irrigation reuse cannot occur. As demonstrated in the process wastewater section of this study, more than sufficient vineyard is available onsite for irrigation dispersal of effluent. Approximately 3 acres is required for process wastewater and a total of 18 acres is available onsite.

If treatment, irrigation, and reuse is proposed for construction of this project, the project must first obtain approval from the San Francisco Bay Regional Water Quality Control Board (SFBREWQCB) for this use. Prior to issuance of building permits, the RWQCB will need to approve of the proposal, and issue Waste Discharge Requirements for the reuse of the sanitary sewage. If future groundwater monitoring cannot occur in a time schedule appropriate for building permits, or does not provide at least 24 inches of separation to groundwater, treatment, irrigation, and reuse will be required for the project. In this event, the RWQCB must also grant system approval prior to building permit issuance.

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PROCESS WASTEWATER (PW)

Existing System

The existing on-site process wastewater system consists of 2 aerated facultative lagoons and an irrigation holding pond. This system is currently treating the process waste from the Clos Pegase winery located across Dunaweal Lane under the same ownership. No sanitary wastewater is discharged into the process wastewater system.

Before entering the process wastewater ponds, the entire flow of process wastewater is filtered through a rotary screen where suspended solids are collected and removed. Biological stabilization occurs in the facultative pond system. The total volume of the existing pond system is approximately 1.5 MG. There is a 10 hp aerator in Pond 1 and a 5 hp aerator in Pond 2. Clos Pegase is currently producing 200,000 gallons of wine with an average annual PW production of 920,000 gallons. This pond system is large enough to provide at least 200 days of retention time at current Clos Pegase average flow conditions. Treated PW is used for irrigation of the onsite vineyards.

Proposed System

The proposed PW system for the new Girard Winery will connect to the existing PW wastewater pond system. The new PW connection will include a pump sump and new aerators to accommodate the increase in flows.

Proposed Flow Calculations

The winery is currently proposing a production of 200,000 gallons of wine per year. Using a monthly PW distribution from multiple wineries and a PW generation rate of 4.6 gal PW per gal wine produced (from Clos Pegase data) flow rates are estimated as follows:

Winery Process Wastewater (PW)

Average Daily Flow = 2,521 gal PW/day

Average Harvest Day = 3,950 gal PW/day

Average Day, Peak Harvest Month = 5,060 gal PW/day (See calculations spreadsheet)

The **design flow proposed** to the system is **10,120 gpd** (5,060 gpd from Girard and 5,060 gpd from Clos Pegase).

Aerator Sizing

The Aerators have been sized using a BOD mass loading and the Aqua-Jet Surface Mechanical Aerator brochure specifications. Calculations (attached) show that a total of 22.5 hp of aerators is required for both ponds. It is proposed to add a second 10 hp

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aerator to Pond 1 for a total of 20 hp in Pond 1. This results in a power to volume (P/V) ratio of 0.21 hp per 1000 ft³. This is sufficient for surface mixing and aeration in Pond 1. Pond 2 has an (E) 5 hp aerator. This provided a P/V ratio of 0.05 hp per 1000 ft³. This is sufficient for surface mixing and to prevent odors in Pond 2. No aeration should be required in the irrigation pond due to dilution, level of treatment exiting Pond 2, and natural aeration from algae. In addition, an Anti-Erosion Assembly is recommended for both aerators, to minimize sediment mixing during periods of low liquid levels in the ponds.

Pond Sizing

The facultative ponds combined volume is roughly 1.5 MG. This provides for a retention time of >140 days at peak month flows (see calculations spreadsheet). Facultative pond systems are sized with a minimum of 60 days in the entire system, and at least 45 days in the first pond. Therefore, this system will have sufficient contact time for treatment before discharge. During the rainy winter months when irrigation needs are low the existing irrigation pond will be used as a detention system to hold excess effluent until the spring months when increased irrigation loading is appropriate.

Irrigation Reserve/Dispersal

A total of 7.5 acres of vineyard is required for dispersal of effluent to avoid ponding and concentration.

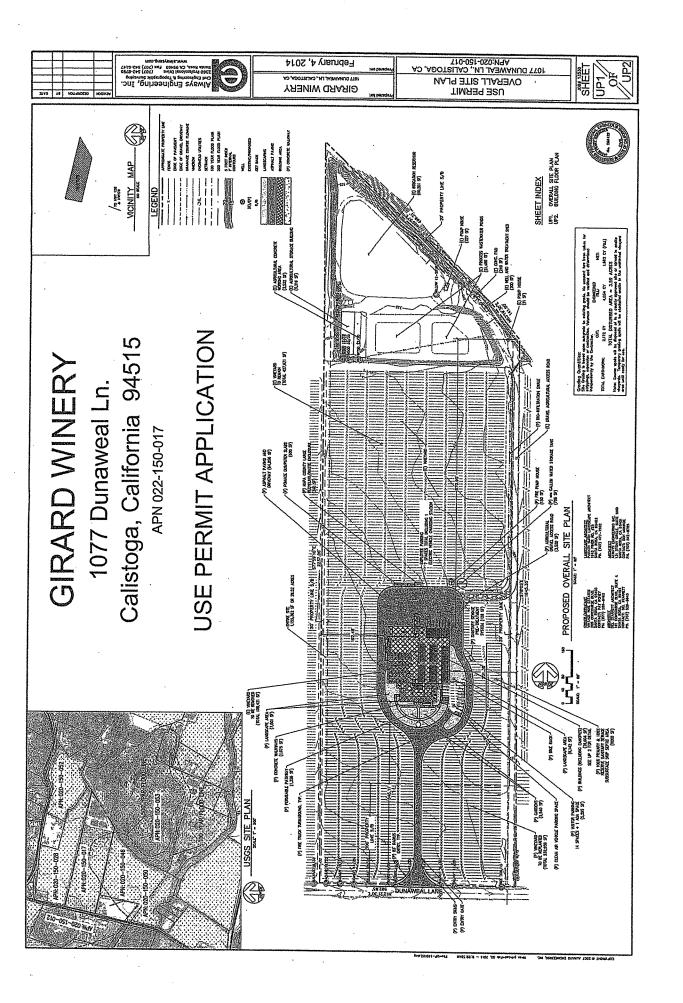
SUMMARY AND CONCLUSIONS

Sanitary Wastewater

With the proposed installation of a new sanitary management system, as discussed in this report, the site is capable of supporting the proposed sanitary sewage loads.

Process Wastewater

With the proposed installation of additional aerators and a collection system and pump station, the existing aerated facultative pond system is sufficient for the proposed Girard Winery PW flows in addition to the existing Clos Pegase Winery PW flows.



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Girard Winery

Annual Process Wastewater Flow

920,000 gallons PW/year

*Refer to the design calculations report for additional flow estimates.

			T
	Percentage of	Monthly	
Month	Annual Flow	Flow	Days
	(%)	(MGal)	
January	6.50%	0.060	31
February	7.00%	0.064	28
March	8.00%	0.074	31
April	7.00%	0.064	30
May	6.50%	0.060	31
June	5.50%	0.051	30
July	6.00%	0.055	31
August	10.50%	0.097	31
September	16.50%	0.152	30
October	12.50%	0.115	31
November	7.50%	0.069	30
December	6.50%	0.060	31
Total	100.00%	0.920	365

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Girard Winery PROCESS WASTEWATER

Annual Volume

Annual Production (projected)				=	1,212 ton/year
Wine Generation Rate (assumed) ^a				#	165 gal wine/ton
Wine Produced	1,212 ton/year	×	165 gal wine/ton	=	200,013 gal wine/year
Process Wastewater (PW) Generation Rateb	(assumed)			=	4.60 gal PW/gal wine
Annual PW Flow	200,013 gal wine/year	×	4.60 gal PW/gal wine	=	920,060 gai PW/year
Average Day Flow					
	920,060 gai PW/year	÷	365 days	=	2.521 gal PW/day
Average Harvest Day			•		
Total Harvest Flow ^c	920,060 gal PW/year	×	39.5%	r	363,424 gal PW/harvest
Average Harvest Flow (3 month harvest)	363,424 gal PW/harvest	÷	92 days	=	3.950 gal PW/day
Average Day, Peak harvest Month - Pond Design	<u>.</u>				
Total Peak Month Flow ^c	920,060 gal PW/year	×	16.5%	=	151,810 gal PW/month
Average Day, Peak Month Flow	151,810 gal PW/month	÷	30 days	=	5,060 gal PW/day

a. 165 Gal wine per ton of grapes is used as a wine industr standard

b. 4.6 gal of PW per gallon wine produced over the course of 1 year is based on hisotrical data from Clos Pegase and existing Griard operations.

c. Percentage of PW produced during each month is based on the average flow distirubtion from 16 wineries

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Clos Pegase Winery

Annual Process Wastewater Flow

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920,000 gallons PW/year

*Refer to the design calculations report for additional flow estimates.

	·		_
Month	Percentage of Annual Flow (%)	Monthly Flow (MGal)	Days
January	6.50%	0.060	31
February	7.00%	0.064	28
March	8.00%	0.074	31
April	7.00%	0.064	30
May	6.50%	0.060	31
June	5.50%	0.051	30
July	6.00%	0.055	31
August	10.50%	0.097	31
September	16.50%	0.152	30
October	12.50%	0.115	31
November	7.50%	0.069	30
December	6.50%	0.060	31
Total	100.00%	0.920	365

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Clos Pegase Winery PROCESS WASTEWATER

Annual Volume

Annual Production (projected)				=	1,212 ton/year
Wine Generation Rate (assumed) ^a				*	165 gal wine/ton
Wine Produced	1,212 ton/year	x	165 gal wine/ton	=	200,013 gal wine/year
Process Wastewater (PW) Generation Rate ^b	(assumed)			=	4.60 gal PW/gal wine
Annual PW Flow	200,013 gal wine/year	×	4.60 gal PW/gal wine	=	920,060 gal PW/year
Average Day Flow					
	920,060 gal PW/year	÷	365 days		2,521 gal PW/day
Average Harvest Day					
Total Harvest Flow ^c	920,060 gal PW/year	×	39.5%	=	363,424 gal PW/harvest
Average Harvest Flow (3 month harvest)	363,424 gal PW/harvest	+	92 days	=	3,950 gal PW/day
Average Day, Peak harvest Month - Pond Design	g <u>n</u>				
Total Peak Month Flow ^c	920,060 gal PW/year	×	16.5%	=	151,810 gal PW/month
Average Day, Peak Month Flow	151,810 gal PW/month	÷	30 days	=	5.060 gal PW/day

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b. 4.6 gal of PW per gallon wine produced over the course of 1 year is based on hisotrical data from Clos Pegase and existing Griard operations.

c. Percentage of PW produced during each month is based on the average flow distirubtion from 16 wineries



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Climate Data

			M11111	מונים כר המים				
								r
		Reference	Pan	Lake	Average	10.V	2	
Month	Days	Evapotranspiration ¹	Evapporation	Evaporation	Dracinitation	ביין בפון	TOU-Year	
		(inches)	(inchae)	100000000000000000000000000000000000000		recipitation	Precipitation	
		(2010)	(11101103)	(inches)	(inches)	(inches)	(inches)	
January	Ţ	o:i	17.	1.2	0.6	12.9	47.6	
February	78	1.5	2.2	1.7	u	2	0.71	-
March	31	2.9	ex cr	i c	, r	0.0	11.0	
Anril	20		2 6	6.3).'c	ದ.	11.2	
	3	7.4	5.8	4,5	2.6	7	л -	
May	31	5.8	8.9	6.9	90	. 0		
June	30	5 49	,	ı L	2 (9	7'7	
7		j t	0.11	۵,۵	0.2	0.3	0.4	
Sin ?	To	7.7	13.2	10.2	0.1	ç	,	
August	31	6.4	12.1	6	00	1 0	7.0	
September	30	0,4	× 7	1 1	, c		0.4	
October	3.1	u m		; ·		4.0	0.6	
Novembor	1 6	י ל	7.0	4,4	2.4	3,4	4,7	
IBOILIBAON	2	1.6	2.5	1.9	8.9	47	. 67	
December	31	1.2	1,7	"		, ,	C'CT	
TOTAL	365.0	7 17	27.0	201	0,4	11./	16.1	
		111	0.//	5,55	41.7	29.6	010	

1 Reference Evapotranspiration data is for the Angwin FS obtained from the California Irrigation Management Information System See http://www.cimis.water.ca.gov/cimis/monthlyEToReport.do

2 Average Monthly Pan Evaopration Rates observed at Berryessa Lake, Ca between 1957 and 1970.

3 Lake evaopration is pan evaporation multiplied by a 0.77 factor.

4 Average precipitation data is from TheWeatherChannel.com for Calistoga, CA

See http://www.weather.com/weather/wxclimatology/monthly/94515

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Date: 02/20/2014 Project: Girard Winery Use Permit Pond 1 Balance

Г						······			_								,			
	Volume	Change	(Mgal)	2000	0,433	0.137	0.000	0.000	-0.100	0.100	-0.106	-0.200	0000	0000	0.000	-0.024	0.000	0000	0,000	0000
	Water Depth at	end of month	(feet)	87	200	70.0	70.0	10.0	9.1		8.0	5.7	5.7	7.3	3.7	5.4	5.4	5.7	7	
	Volume at end of	Month	(Mgal)	0.593	0.730	07.00	0.730	0.730	0.630	0 53.8	0.524	0.324	0.324	0.324	1200	0.300	0.300	0.380)	
out	Discharge to	Pond 2	(Mgal)	0,000	00100	0.057		D. T.	0.231	S S S S S S S S S S S S S S S S S S S		0.5112	0.167	0.309	July Color	9	0.269	0.278	2 6/3	2.0-7
Output	Pond	Evaporation*	(Mgai)	0.009	0.015	7200	0.000	7+0.0	0.061	0.070	0.000	0.072	0.059	0.042	7600	2200	0.012	0.008	0.444	
4.2	10 Year	Precipitation	INIBAIJ	0.173	0.108	0.110	0.050	200	0.012	0.004	0000	7000	0.004	0.006	0.046	0.434	0.131	0.158	0.803	
Input	Process	wastewater in	(mgai)	0.120	0.129	0.147	0.129	0.400	0.120	0.101	0.110	2000	0,193	0.304	0.230	0.138	0000	0.120	1.840	
	Start	(Masl)	(100)	ກາດຄະດ	0.593	0.730	0.730	0.730	20,730	0.630	0.524	1000	0.324	0.324	0.324	0.300	0000	0.500		
	Month			January	February	March	April	May	, S	June	λnς	Aircinet	August	september	October	November	Docombor	חפרפווזתבו	Total	

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Date: 02/20/2014 Project: Girard Winery Use Permit Pond 2 Balance

_						_															
		Volume Change	,	(Mgal)	0.175	0.200	0.203	-0.082	-0.170	-0.057	1000	-0.085	2000	0.000	-0.099	0.015	-0.002	0.000	-0.049	0.231	0.000
		Water Depth		(reet)	9.1	10.8	200	7'01	8.7	8.2		7.4	עע	7 3	4,0	5.6	5.5		5.0	7.5	
	Volume at	Month	(8,600)	(Ivigal)	0.705	0.915	0 833	0.033	0.662	0.605	0000	0.520	0.434	0 225	0.00	0.350	0.347	0000	0.233	0.530	
Output	Discharge to	Pond	(Mgall)	(IVISAI)	00000	0000	USPU		0.400	0.300	0000	nne a	0.400	00000		0000	0.350	שיעשייי		00700	3.456
Out	Pond	Evaporation*	(Meal)	7.00	0.011	0.017	0.031	7700	440.0	0,062	0.073	2,0,0	0.082	0.068	7700	7500	0.031	0.013	0.010	OTO	0.489
	10 Year	Precipitation	(Mgal)	0.175	0.17.0	0.109	0.111	0.051	2000	710,0	0.004		0,002	0.004	0.006	7,000	7+0.0	0.133	0.160	2500	0.813
 Input	Process Wastewater In	From Pond 1	(Mgal)	0.00	00,00	007.0	0.257	0.179	0.224	0.401	0.211	0.217	776'0	0.197	0.309	0 300	0000	0.269	0,278	2 643	C+0.2
	Start	Volume	(Mgal)	0:230	707.0	507.0	0.915	0.833	0.662	1000	0.605	0.520	22.0	0,434	0.335	0.350		0.34/	0,299		
		Month		January	Fehruary	, 10 mm	iviarcn	April	Mav	7	nne	Viul	, , , , , ,	August	September	October.	N. C. C. L.	NOVERIDEL	December	Total	

Project: Girard Winery Use Permit

Landscape	0.5 a
Vineyard =	2.5 a
Pasture =	0 2
Soil perc rate =	1 1

Month January February March April May June July August September October November	Days 31 28 31 30 31 30 31 30 31 31 30 31	Reference Evapotranspiration ¹ (inches) 1.0 1.6 3.0 4.6 6.0 7.0 8.0 7.0 5.2 3.4 1.4	ersa)) 3 0 3 0 6 1 5	Mal Capacity (Mgal) 0.000 0.000 0.474 0.848 1.373 1.543 2.594 2.619 2.457	Irrigatio (in) 0.000 0.000 0.460 0.409 0.307 0.307 0.307 0.307 0.358	Effluent to on Pond (Mgal) 0.000 0.450 0.400 0.300 0.300 0.400 0.300 0.300 0.350	Residual Capacity ⁷ (Mgal) 0.000 0.000 0.024 0.448 1.073 1.243 2.194 2.319 2.157 0.723
December	31	0.9	;	0.541	0.460	0.450	0.091
TOTAL	365.0	49.1		0.000 13.520	0.211 3.536	0.206 3.456	-0.205 10.064

- 1 Average monthly reference evapotranspriz
- 2 Pasture coefficient from Table 5-1, "Irrigati
- 3 Vineayrd coefficient from Table 5-12, "Irrig
- 4 Crop coefficient times the reference evapo
- 5 Precipitation for a 10-yr event, refer to the
- 6 Irrigation demand is the evapotrasnpiration
- 7 Residual capacity estimates irrigation/perci

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Project: Girard Winery Use Permit

Aeration Calculations

Design Flow Estimated Average Daily Flow

10,120 gal/day 0.010 Mgal/day = 38 m^3/day 38,294 liters/day

BOD MASS LOADING - Amount of Biochemical Oxygen Demand (BOD) Based on Amount of Organics in Wastewater

BOD into Pond **- 33** 7700 mg/L

(Table 4-12 & 4-14 of Small and Decentralized Wastewater Management Systems)

1000 mL/m^3 x 0.000001 kg/mg

BOD Mass Load

38 m^3/day 294.9 kg BOD/day

648.7 lb BOD/day

OXYGEN REQUIREMENTS - The amount of oxygen requiremed to breakdown the waste in the water

O2 Requirement

648.7 lb BOD/day

1.5 lbs 02/lb BOD

7700 mg BOD/L

973.1 lbs O2/day

HORSEPOWER REQUIREMENTS - The horsepower of aeration required to provide the necessary amount of oxygen

Oxygen Transfer Efficiency Horsepower Requirement

973.1 lbs O2/day

= 18 lbs O2/Hp*hr (3.4 assumes a VBT aerator, model 100) 1.8 lbs O2/Hp*hr +

22.5 Hp required

POWER TO VOLUME RATIO (Hp/10^3 ft^3) - This is used to estimate the amount of mixing which will occur in a pond due to aeration

Pond Volume

0.723 Mgai 722,797 gallons

Number if cells Ratio of first to second cell 96,631 ft^3 2 2

Volume in Pond 1

722,797 gallons 96,631 ft^3

Volume in Pond 2

803,995 gallons 107,486 ft^3

Horsepower in Pond 1; cell 1

20 Hp 20 Hp

Pond 1 Power to Volume Ratio

1000 ft^3 96,631 ft^3 1000 ft^3

0.21 Hp/1000 ft^3 5 Hp

Horsepower in Pond 1, cell 2 Pond 2 Power to Volume Ratio

5 Ho

0.05 Hp/1000 ft^3

107,486 ft^3 1000 ft^3 1000 ft^3 (Page 463 of Small and Decentralized Wostewater Monagement)

Complete Mix 0.75 - 1.5 Hp/1000 ft^3 Partial Mix 0.4 - 0.75 Hp/1000 ft^3

Facultative Hp/1000 ft^3 = 0.1 - 0.4

Pond 1

Retention Time (t)/ Estimated Effluent

Çn Effluent BOD Со 7700 mg/L

1 for single cell pond n

k 0.276 d^(-1) 71.4 days t = 372 mg/L Cn Effluent BOD 372 mg/L

Pond 2

Pond 1

Retention Time (t)/ Estimated Effluent

Cn Effluent BOD Co 372 mg/L

n 1 for baffled pond =

k = 0.276 d^(-1) 71.4 days 18 mg/L Cn = Effluent BOD 18 mg/L

SITE EVALUATION REPORT

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Please attach an 8.5" x 11" plot map showing the locations of all test pits triangulated from permanent landmarks or known property corners. The map must be drawn to scale and include a North arrow, surrounding geographic and topographic features, direction and % slope, distance to drainages, water bodies, potential areas for flooding, unstable landforms, existing or proposed roads, structures, utilities, domestic water supplies, wells, ponds, existing wastewater treatment systems and facilities.

Permit #: E13-00744		
APN: 020-150-017		
(County Use Only) Reviewed by:	Date:	***************************************

PLEASE PRINT OR TYPE ALL INFORMATION

Vintage Wine Estates dba Girard W	linery			×	New Construction Other:	☐ Addition	☐ Remodel ☐	Relocation	n	
Property Owner Mailing Address 205 Concourse Blvd				☐ Residential - # of Bedrooms: Design Flow:						
City	State	Zip		x Commercial – Type: Winery domestic						
Santa Rosa Site Address/Location 1077 Dunaweal Lane	CA	95403	***************************************		Sanitary Waste: !	500-1675 gpd	Process Waste	e: 0	gpd	
Calistoga, CA 94515					Other:					
					Sanitary Waste:	gpd	Process Was	te:	gpd	
Evaluation Conducted By:										
Company Name Always Engineering, Inc.		Evaluator's Name Ben Monroe, P.E.	RCE	7		Signature (CIVI)	Engineer, P.E.H/S/ Geolog	ist Soil Scie	ntist)	
Mailing Address: 131B Stony Circle, Sutie 1000						Telephone Nu (707) 542-879	mber / 5 x 17		vitarutuvita saaraan	
City Santa Rosa, Ca 95401		State	Zip			Date Evaluatio 11/14/2013	n Conducted			

Primary Area	Expansion Area					
Acceptable Soil Depth: 24-48 in. Test pit #'s: TP1-TP6	Acceptable Soil Depth: 24-48 in. Test pit #'s: TP1-TP6					
Soil Application Rate (gal. /sq. ft. /day): 0.75 to 1.0 gpd/sf	Soil Application Rate (gal. /sq. ft. /day):0.75 to 1,0 gpd/sf					
System Type(s) Recommended: PD, drip - pending gw	System Type(s) Recommended: PD, drip – pending gw					
Slope: 3-5 %. Distance to nearest water source: 1000 ft.	Slope: 3-5 %. Distance to nearest water source: 1000 ft.					
Hydrometer test performed? No	Hydrometer test performed? No					
Bulk Density test performed? No	Bulk Density test performed? No					
Percolation test performed? No	Percolation test performed? No					
Groundwater Monitoring Performed? Pending Rain	Groundwater Monitoring Performed? Pending Rain					

Site constraints/Recommendations:

- Existing well
- Groundwater monitoring to be performed to identify perched groundwater level due to presence of mottling at less than 24 inches deep.
- Interceptor drain and surface drainage to divert away from septic area recommended.
- Proposed drainage features and grading will need to avoid.
- Additional test pits near wastewater ponds showed signs of significant seasonal saturation and lesser depths of permeable soils. Pits on map but not logged due to time onsite.

Test Pit # 1

PLEASE PRINT OR TYPE ALL INFORMATION

Horizon					C	onsistenc	e			Mottling
Depth (Inches)	Boundary	%Rock	Texture	Structure	Side Wall	Ped	Wet	Pores	Roots	
34	D/G	15-20	SCL	SAB,3	FR	S	S	3,C	1,M	1,VF
48	D/G	35	SCL	SAB,3	VF	S	SS	3,M	1,M	1,F
60+		<10	SCL	SAB,2	D/L	М	М	1,VF	1,M	2,P
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Test Pit #2

Horizon	B	%Rock	Texture		C	onsistenc	e			
Depth (Inches)	Boundary			Structure	Side Wall	Ped	Wet	Pores	Roots	Mottling
24	D/G	15-20	SCL	SAB,3	FR	S	S	3,C	1,M	1,VF
56	D/G	35	SCL	SAB,3	VF	S.	SS	3,М	1,M	1,F
65+		<10	SCL	SAB,2	D/L	М	М	1,VF	1,M	2,P
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Test Pit # 3

Horizon	Boundary	%Rock	Texture	Structure	C	onsistenc	e			Mottling
Depth (Inches)					Side Wall	Ped	Wet	Pores	Roots	
28	D/G	15-20	SCL	SAB,3	FR	S	S	3,C	1,M	1,VF
60	D/G	15-20	SL/LS	SAB,3	F	М	SS	3,M/F	1,M	1,F
70+		<10	SCL	SAB,2	D/L	M	М	1,VF	1,M	2,P
+									***************************************	

Test Pit # 4

PLEASE PRINT OR TYPE ALL INFORMATION

Horizon	Boundary	0/17		_	C	onsistenc	e			Mottling
Depth (Inches)		%Rock	Texture	Structure	Side Wall	Ped	Wet	Pores	Roots	
24	D/G	15-20	SCL	SAB,3	FR	S	S	3,C	1,M	1,VF
49	D/G	25	SCL	SAB,3	FR	F	S	2,M	1,M	2,F
60+		<10	SCL	SAB,2	D/L	L	М	1,VF	1,M	2,P

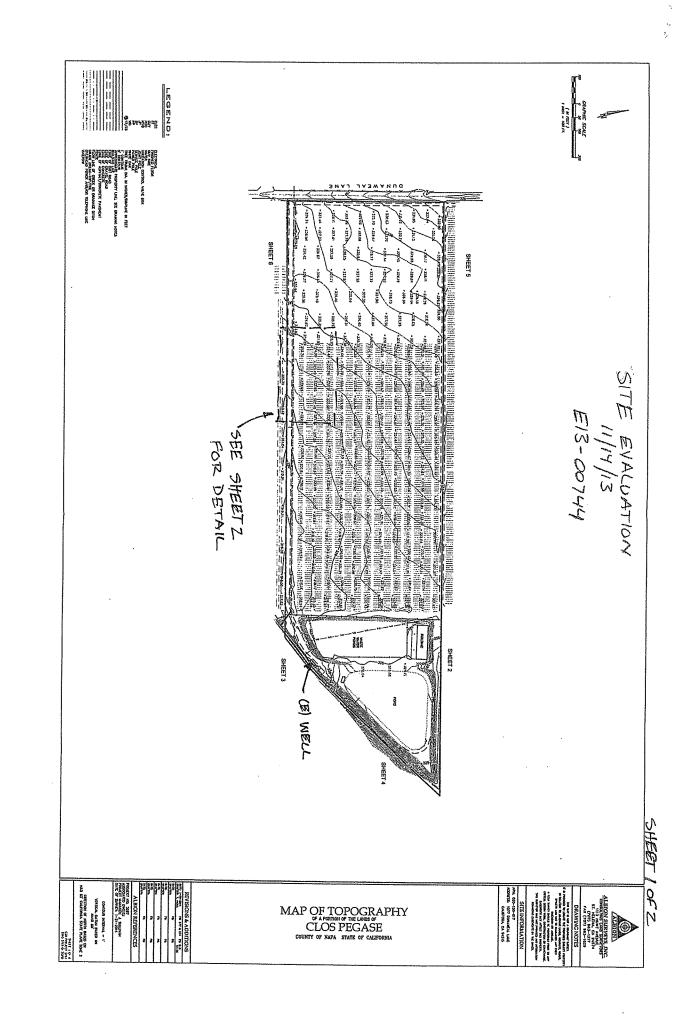
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### Test Pit #5

Horizon	Boundary	0/17	Texture		(	onsistenc	е			1
Depth (Inches)		%Rock		Structure	Side Wall	Ped	Wet	Pores	Roots	Mottling
24	D/G	15-20	SCL	SAB,3	FR	S	S	3,C	1,M	1,VF
49	D/G	25	SCL	SAB,3	F	M/FR	SS	2,F	1,F	1,F
54+		>50%								
+			***************************************							
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# Test Pit # 6

Horizon	Boundame	2/2			C	onsistenc	e			
Depth (inches)	Boundary	%Rock	Texture	Structure	Side Wall	Ped	Wet	Pores	Roots	Mottling
36	D/G	15-20	SCL	SAB,3	FR	S	S	3,C	1,M	1,VF
55	D/G	25	SL	G/B,2	L	L	SS	2,C	1,M	1,D
70+		>50%								
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